

# The KNOO Project At The University of Manchester

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# What is KNOO?



KNOO is a four-year initiative set-up to maintain and develop know-how relevant to nuclear power generation. The project consists in a close collaboration between several universities in UK and key industrial and governmental stakeholders. KNOO is founded through the “**Towards a Sustainable Energy Economy Program**” of Research Councils UK.

The University  
of Manchester



The  
University  
Of  
Sheffield.  
THE UNIVERSITY OF SHEFFIELD  
UNIVERSITY OF SHEFFIELD



Imperial College  
London



# KNOO in numbers

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- ⇒ Collaboration between seven universities among all UK
- ⇒ Budget of £6.1 million (€7.5 million): KNOO is the single **largest** commitment to fission reactor research in UK in the last thirty years.
- ⇒ More than 50 investigators involved
- ⇒ More than 70 PhD projects financed
- ⇒ Structured in four different Works Package covering all the aspects of nuclear engineering.

# Work Packages

KNOO is divided into four Work Packages:

- ⇒ **WP1: Fuel Thermal-hydraulics and reactor Systems;**
- ⇒ **WP2: Materials performances and Monitoring Reactors Conditions;**
- ⇒ **WP3: An integrate approach to waste immobilization and management;**
- ⇒ **WP4: Safety and performances for a new generation of Reactor Design.**

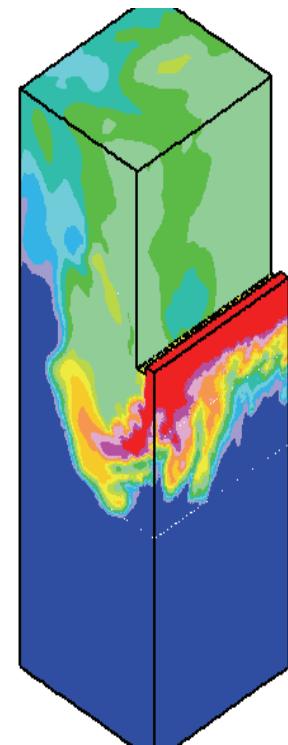
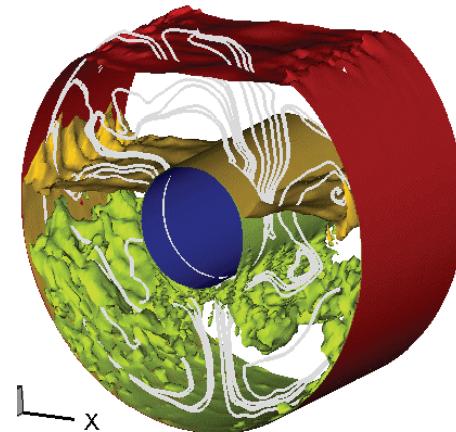
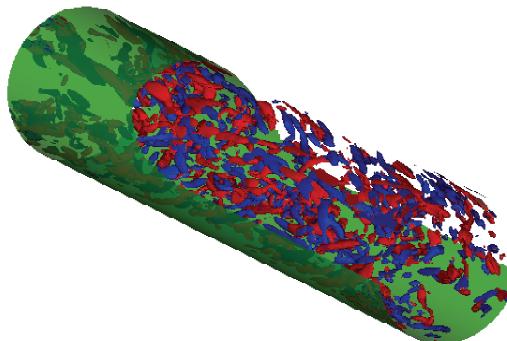
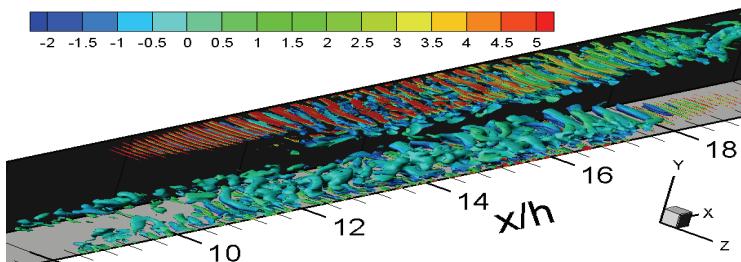
<http://www.knoo.org/>

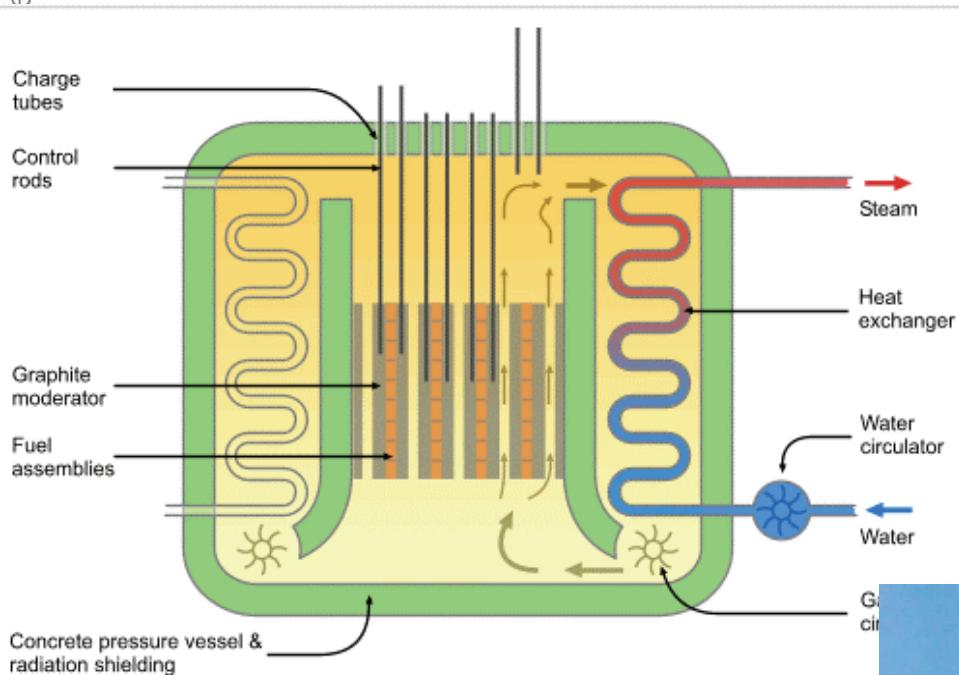
Activities of the MACE CFD Group in KNOO can be divided into:

1. Creation of databases (Refined LES) for RANS validation
  - KNOO Test cases (Heat Transfer)  
<http://cfd.mace.manchester.ac.uk/Main/KnooTestCases>
2. Best Practise Guidelines (BPG) for CFD in nuclear applications.
  - <http://cfd.mace.manchester.ac.uk/Main/KnooWorkshop>
3. Generation IV design.
4. Performance improvements of actual reactor configurations
5. TWiki portal of the Project:
  - <http://cfd.mace.manchester.ac.uk/Main/KnooProject>

## Refined LES of Natural Convection and induced re-laminarized flow.

- ⇒ Heated vertical pipe flow
- ⇒ Buoyancy opposed wall jet
- ⇒ Cohaxial heated cylinder
- ⇒ Tilted cavity





### Working bulk temperatures:

- Channel inlet: 334°C
- Channel outlet: 635°C
- Peak Temp: 661°C

### Working pressures inside pressure vessel:

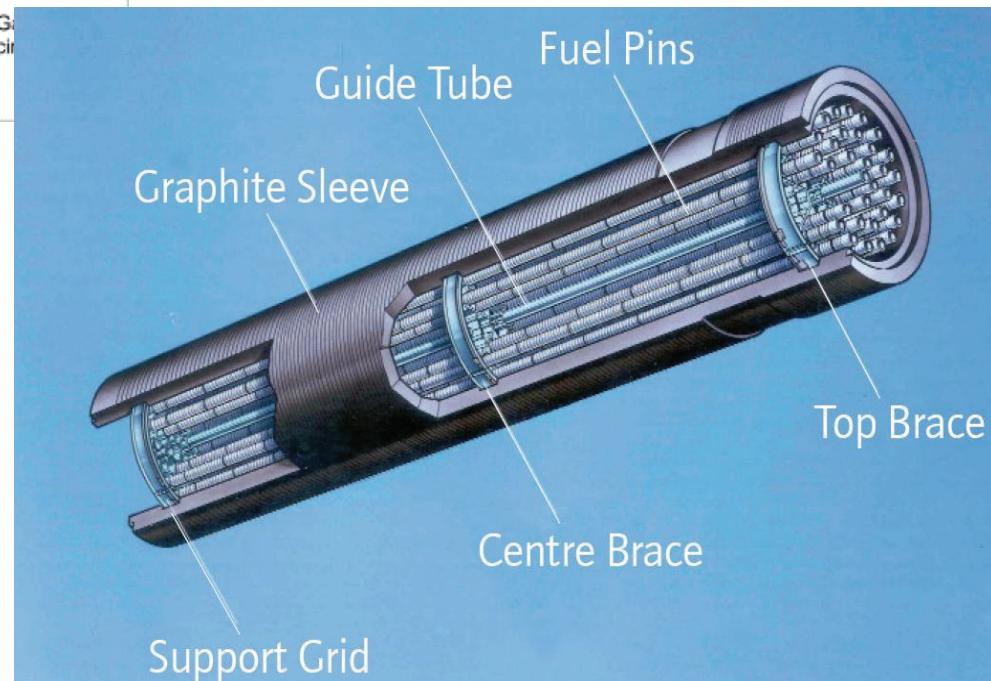
- Bottom slab: 45.2 bar
- Top slab and walls: 42.5 bar

### General:

- Working fluid: CO<sub>2</sub>
- Re=1e+6 ; based on D<sub>h</sub>
- Flow direction: Upward

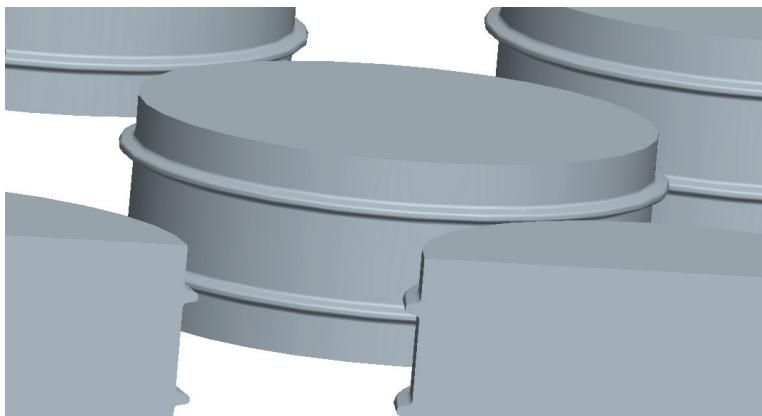
### Mass flow rates:

- Fuel channels: 3910 kg/s
- Net circular flow: 4270 kg/s
- Peak channel flow: 14.1 kg/s

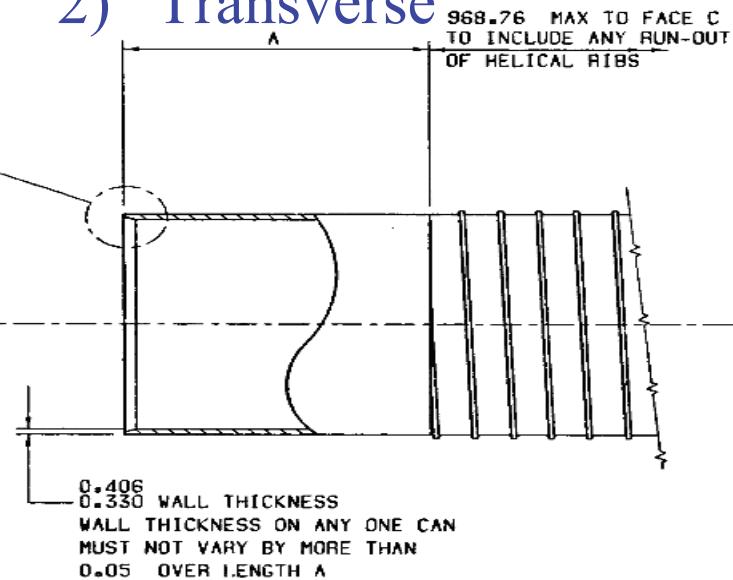


Three different types of configurations for fuel pins:

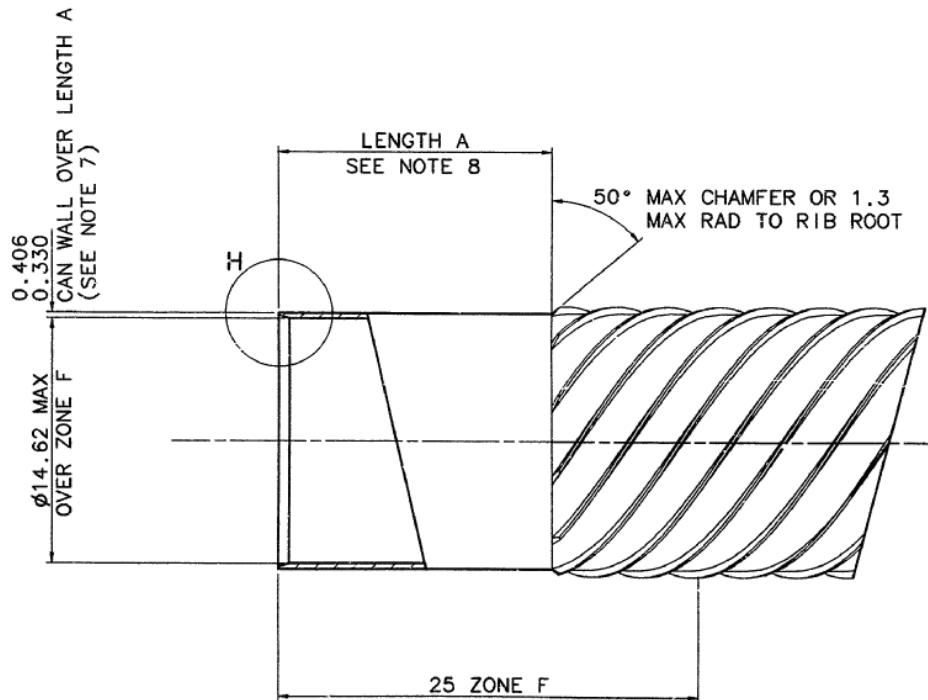
1) “Parallel”

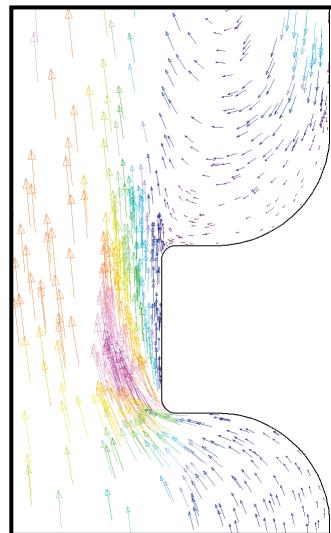
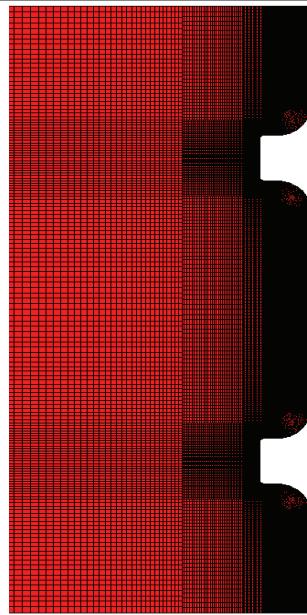
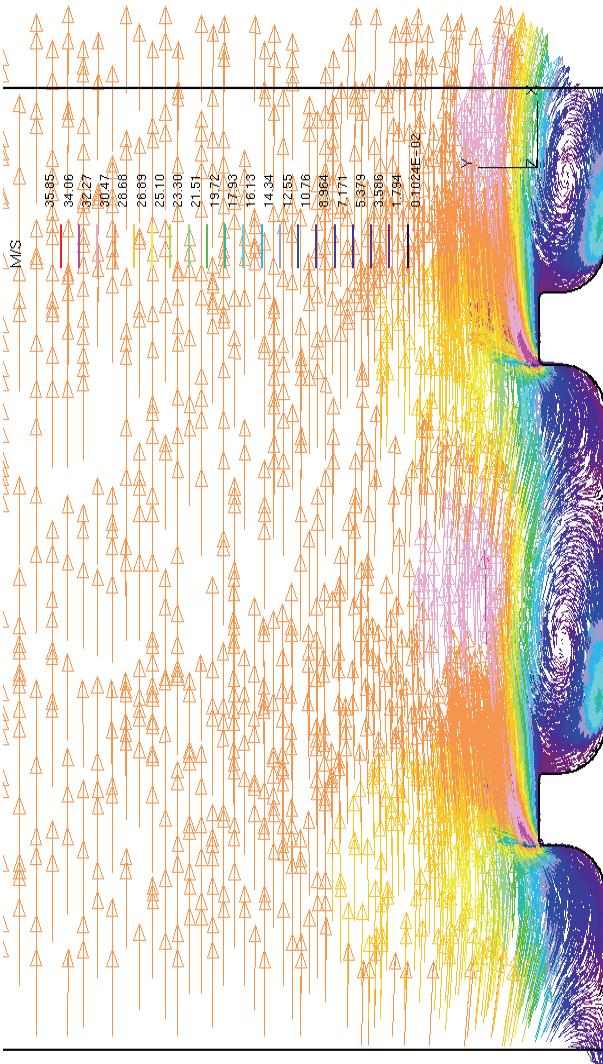


2) “Transverse”

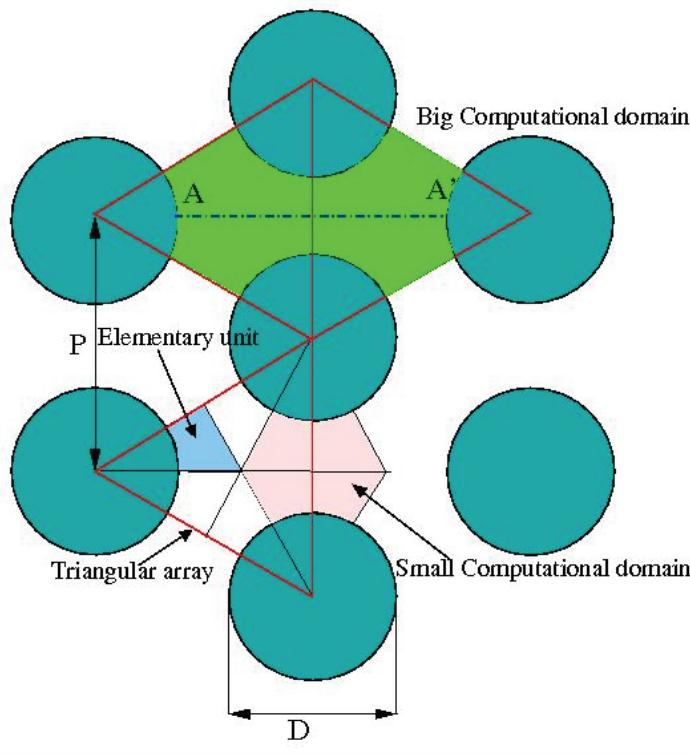


3) “Multi-start” : 12 different helixes with different starting points

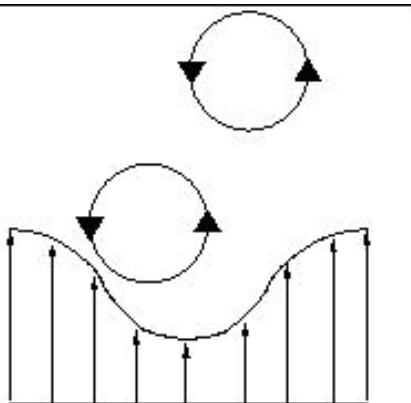


Preliminary Results “Transverse Configuration”  
(A. Keshmiri)2D Approach with a Low-Reynolds k- $\varepsilon$  model

# Rod Bundle arranged in a triangular array



- Experimental work:
  - I. **Secondary flow**: Vonka "Measurement of secondary vortices in Rod Bundle" Nuclear Engineering and Design, Volume 106, Issue 2, 2 February 1988, Pages 191-207
  - II. **Flow pulsations**: Krauss, Meyer "Experimental investigation of turbulent transport of momentum and energy in a heated rod bundle", Nuclear Engineering and Design, Volume 180, Issue 3, April 1998, Pages 185-206
- CFD work (URANS):
  1. E. Merzari, H. Ninokata, E. Baglietto "Numerical simulation of flows in tight-lattice fuel bundles" Nuclear Engineering and Design, Volume 238, Issue 7, July 2008, Pages 1703-1719 .
  2. D. Chang, S. Tavoularis "Simulations of turbulence, heat transfer and mixing across narrow gaps between rod-bundle sub-channels" Nuclear Engineering and Design, Volume 238, Issue 1, January 2008, Pages 109-123



From II

$$St = \frac{fD}{U_{B,gap}} = 0.93 \quad \text{for} \quad \frac{P}{D} = 1.06$$

Two different geometrical configuration

1. **P/D = 1.06**

- I. LES @ Re = 6000 Mesh size ~ 2 Millions cells with Heat transfer.
  - $0.75 < \Delta r + < 1.06$
  - $6 < r\Delta\theta + < 10$
  - $16 < \Delta x + < 22.5$
- II. Hybrid @ Re = 6000 Mesh size ~ 0.35 Million cells with Heat transfer
  - $0.8 < \Delta r + < 1.3$
  - $15 < r\Delta\theta + < 20$
  - $40 < \Delta x + < 60$
- III. Hybrid @ Re = 39000 Mesh size ~ 0.9 Million cells no Heat transfer
  - $0.8 < \Delta r + < 1.2$
  - $20 < r\Delta\theta + < 25$
  - $50 < \Delta x + < 70$

2. **P/D = 1.15**

- I. LES @ Re = 6000 Mesh size ~ 1.4 Million cells no Heat transfer
  - $0.8 < \Delta r + < 1.1$
  - $6.5 < r\Delta\theta + < 10$
  - $16 < \Delta x + < 22.5$

All the domains have a stream-wise length equal to 12 times  
the hydraulic diameter

The Hybrid RANS-LES method is following a usual LES decomposition in large scale and sub-grid part:

$$u_j = \underline{u_j} + u'_j$$

The anisotropic part of the residual stress tensor and residual heat flux can be decomposed following a Schumann decomposition:

$$\left\{ \begin{array}{l} \text{Locally Isotropic} \\ \tau_{ij}^r = -2\nu_r \mathcal{F}_b (\overline{S_{ij}} - \langle \overline{S_{ij}} \rangle) - 2\nu_a (1 - \mathcal{F}_b) \langle \overline{S_{ij}} \rangle \\ \sigma_j = -\mathcal{F}_b \kappa_r \frac{\partial}{\partial x_j} (\overline{T} - \langle \overline{T} \rangle) - (1 - \mathcal{F}_b) \kappa_a \frac{\partial \langle \overline{T} \rangle}{\partial x_j} \end{array} \right.$$

$$\nu_r = (C_s \Delta)^2 \sqrt{2s'_{ij} s'_{ij}}$$

$$\nu_a = C_\mu \varphi k T$$

$$\text{Sub- grid viscosity} \quad T = \max \left( \frac{k}{\varepsilon}, C_T \sqrt{\frac{\nu}{\varepsilon}} \right)$$

RANS viscosity computed from the mean velocity field ( $\varphi = \overline{v^2}/k$ )

For the eddy conductivity a simply turbulent Prandtl number analogy is used

$$\left\{ \begin{array}{l} \kappa_r = \frac{\nu_r}{Pr_t} \\ \kappa_a = \frac{\nu_a}{Pr_t} \end{array} \right.$$

$$\mathcal{F}_b = \tanh\left(C_l \frac{L_t}{\Delta}\right)^n$$

The merging between the two velocity fields is done through a blending function to obtain a smooth transition

$$L_t = \varphi k^{3/2} / \varepsilon$$

Turbulent RANS length scale computed with a relaxation model based on  $\overline{v^2} - f$

$$\Delta = 2Vol^{1/3}$$

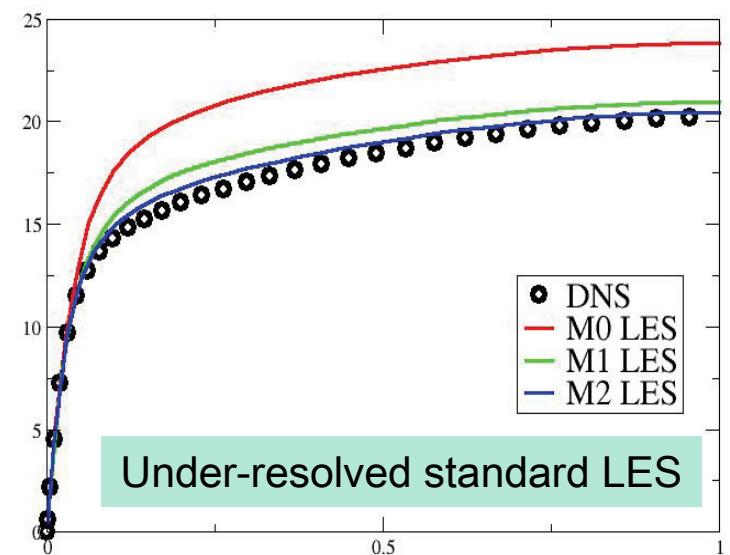
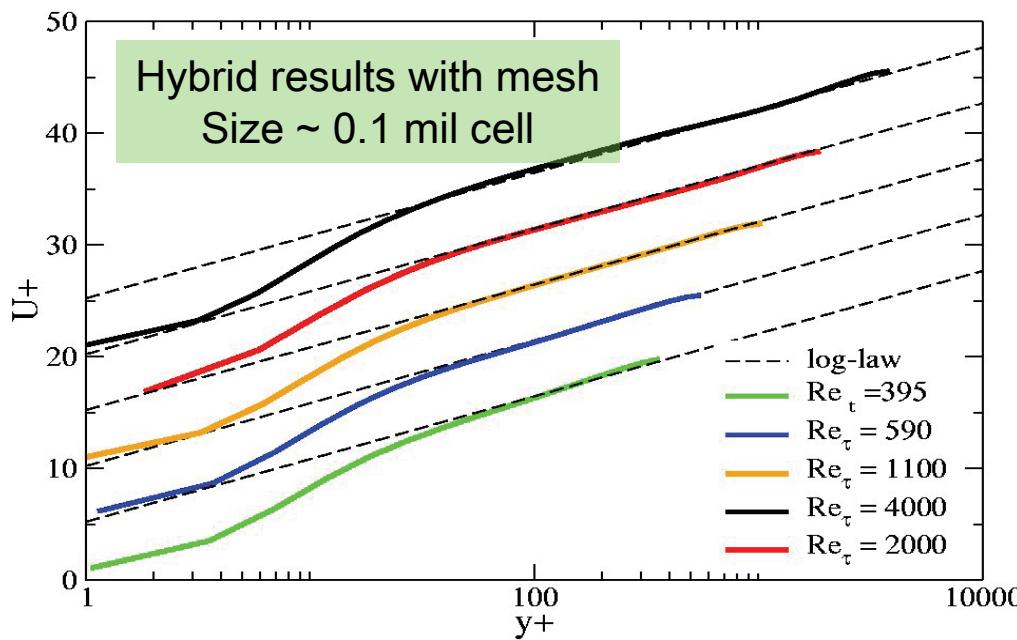
Filter width

$$C_l = 1.5$$

Empirical constants computed in order to match the stress profile for channel flow @

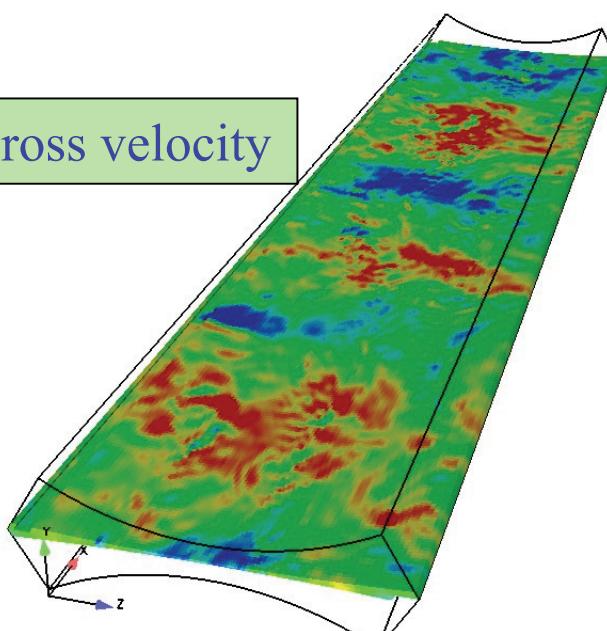
$$n = 1$$

$$Re = 395$$

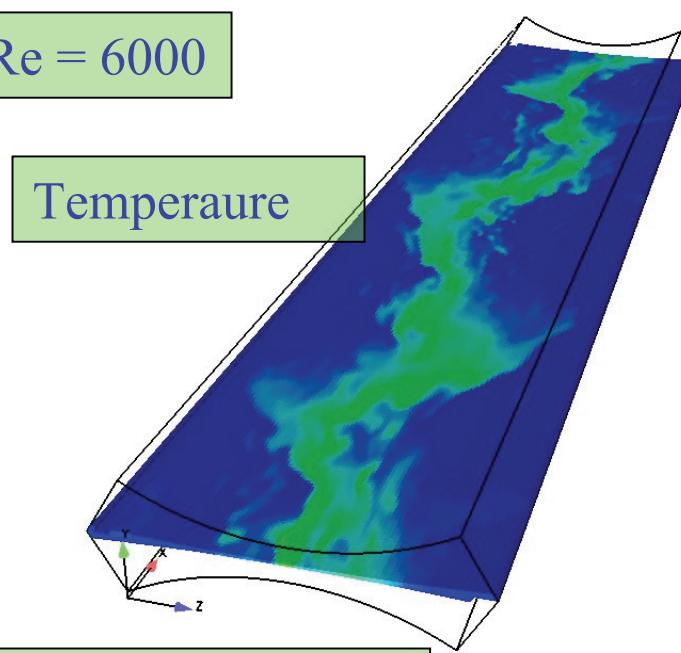
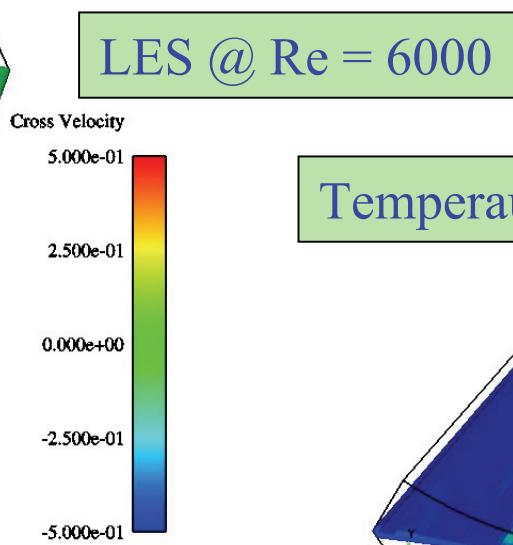


# Results: Flow Pulsation in the mid-plane

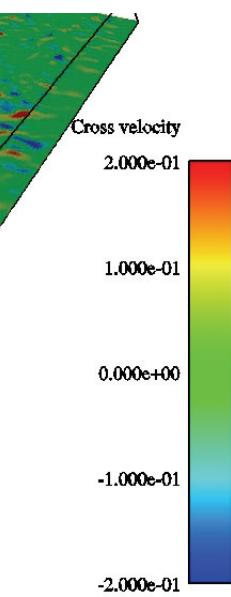
That's interesting



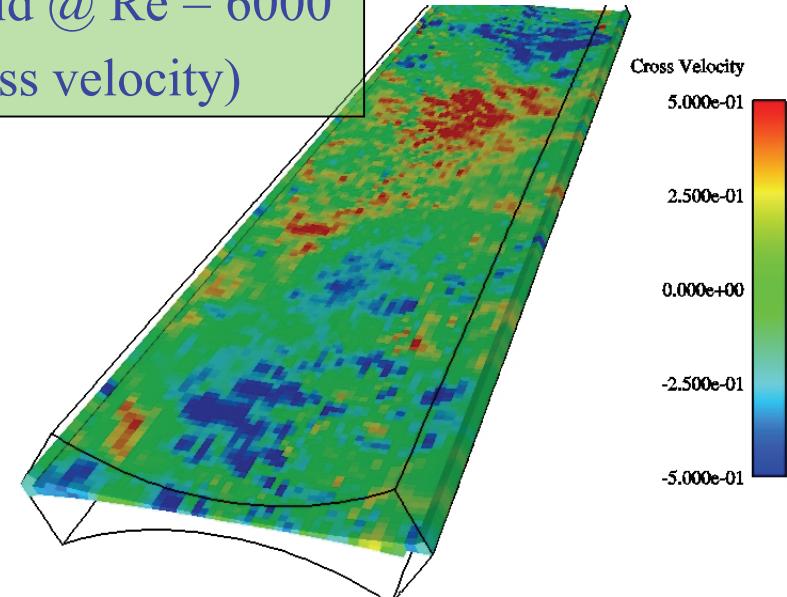
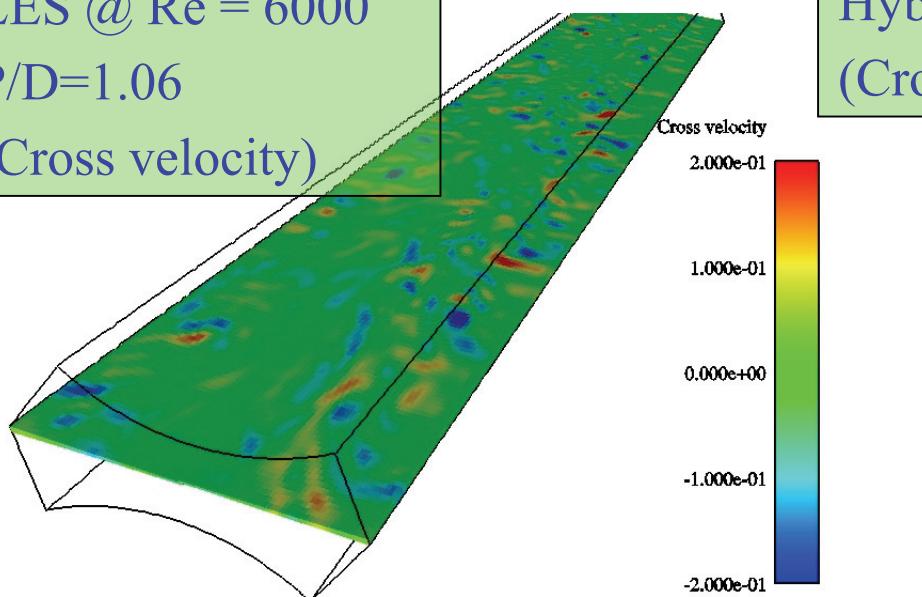
LES @ Re = 6000  
P/D=1.06  
(Cross velocity)



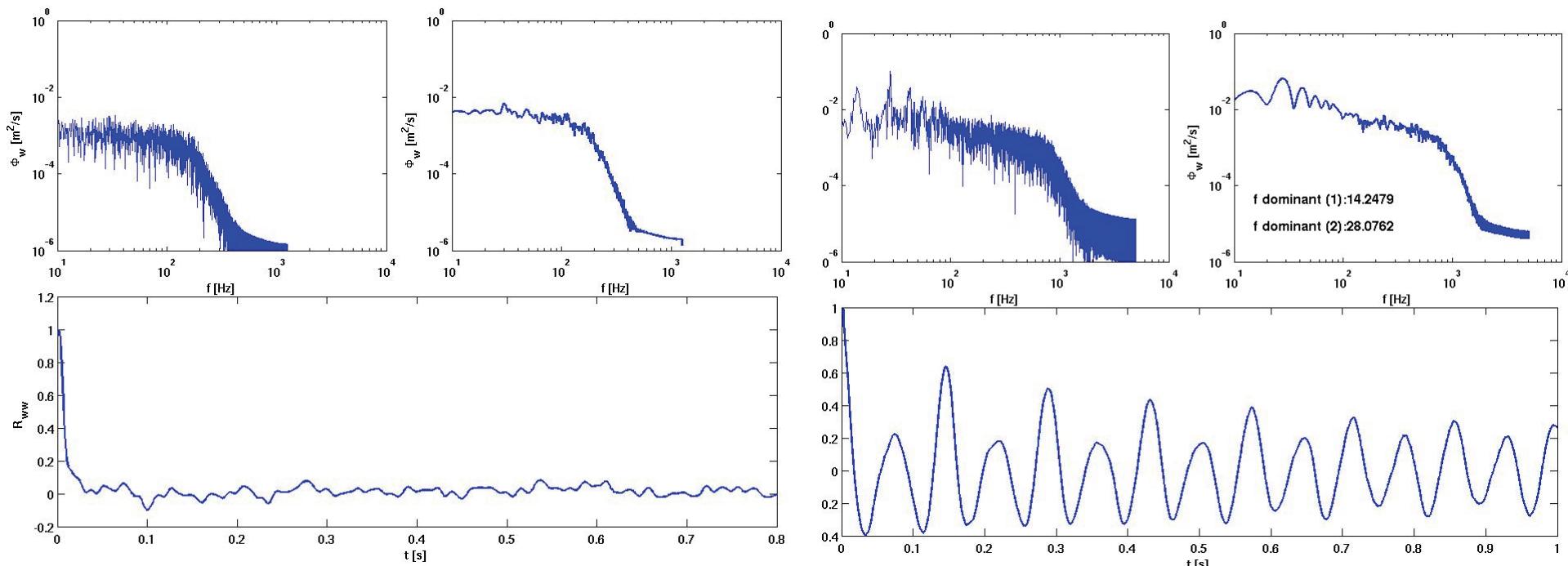
Temperaure



Hybid @ Re = 6000  
(Cross velocity)



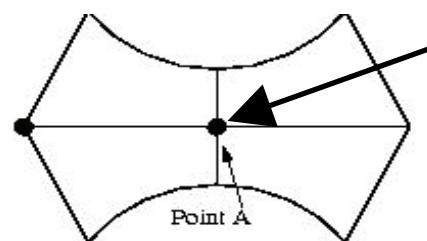
## Power spectra azimuthal velocity

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P/D=1.15

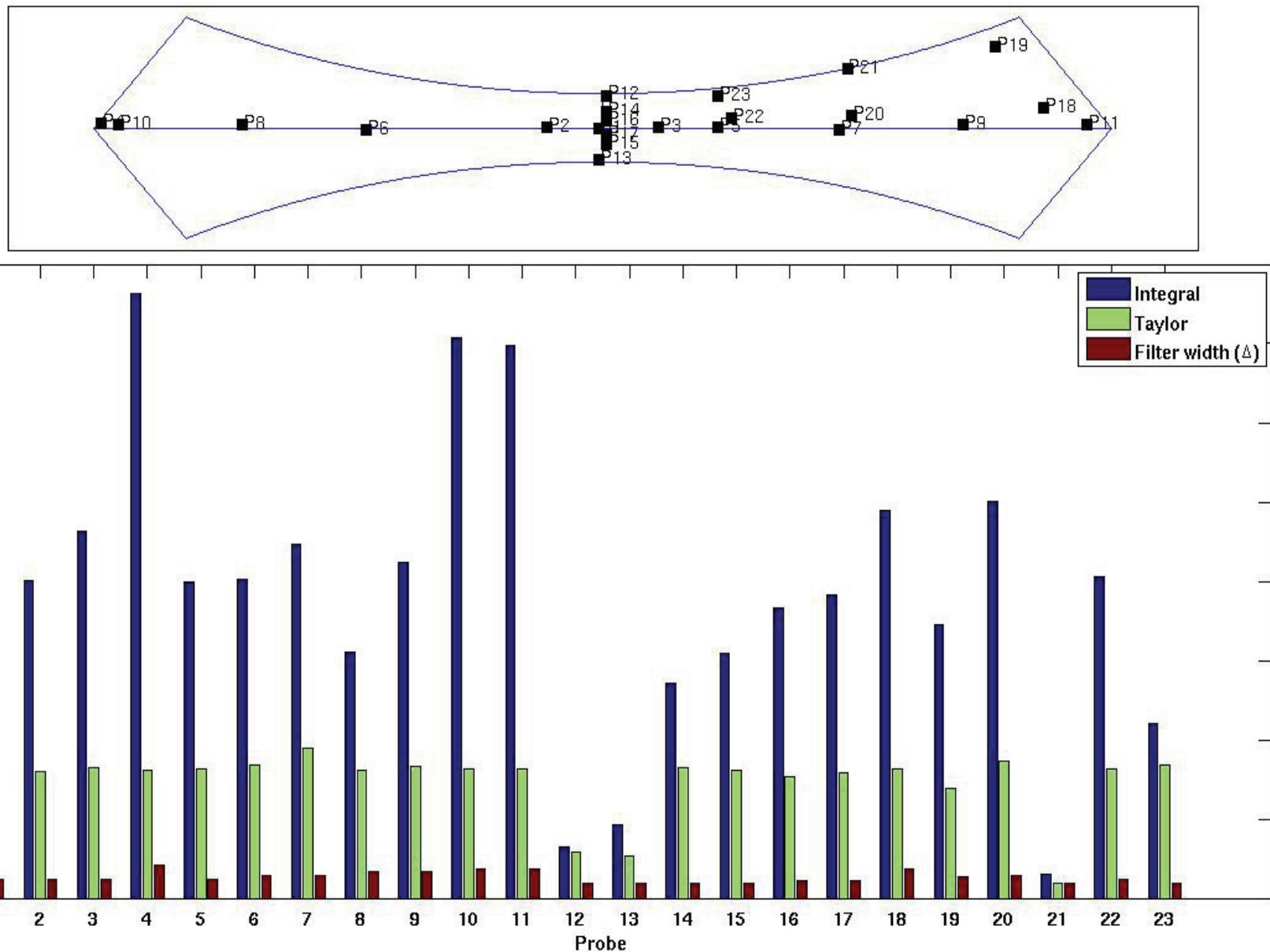
Point A

P/D=1.06

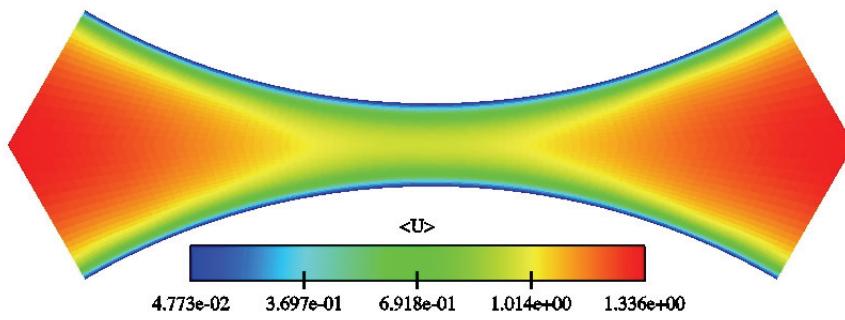


	LES6K	LESWPD	HYB6K	HYB39K	EXP
$St = fD / U_{B,\text{gap}}$	0.98-1.96	/	0.91-1.85	0.92-1.94	0.93

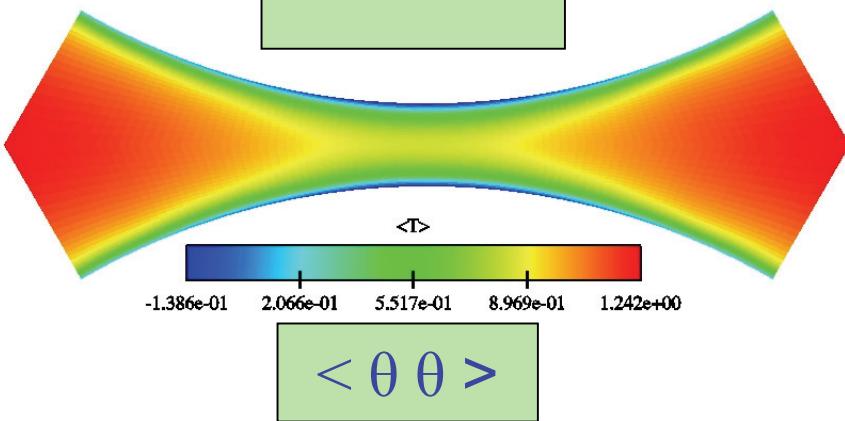
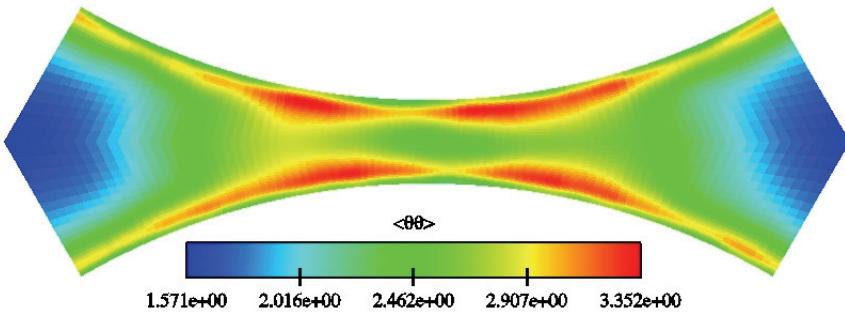
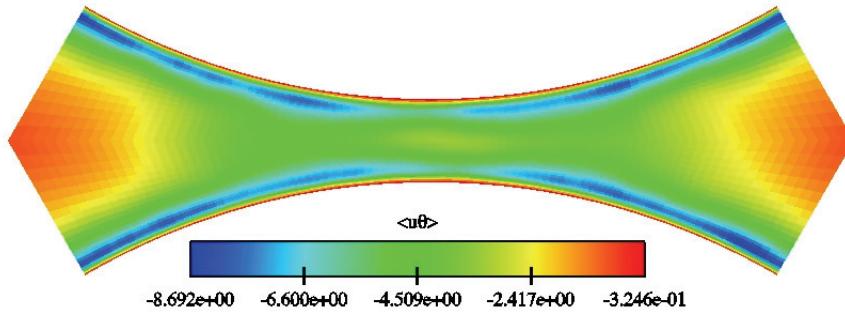
# Length scales

The University  
of Manchester

## Results: Average Field (LES P/D = 1.06 Re = 6000)

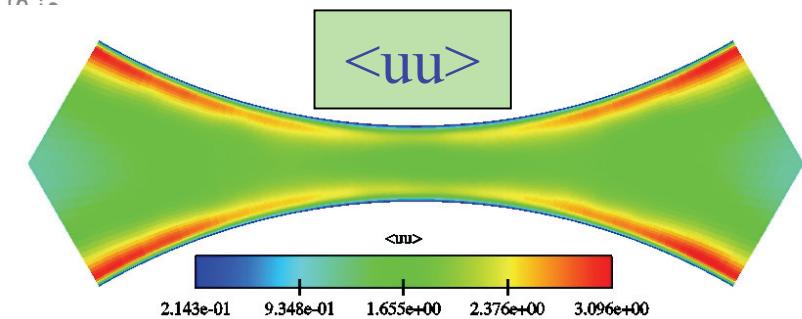
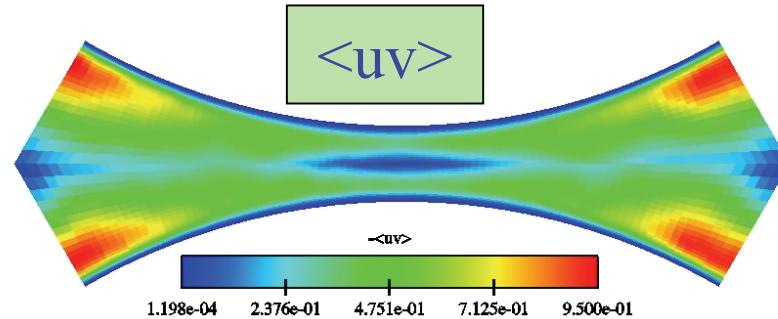
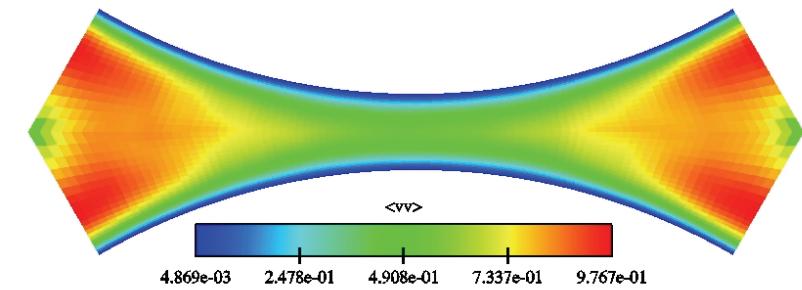
 $\langle U \rangle / U_B$ 

$$\frac{T_{w,m} - T}{(T_{w,m} - T_b)}$$

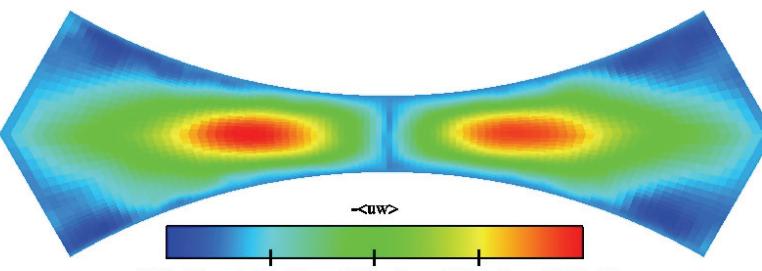
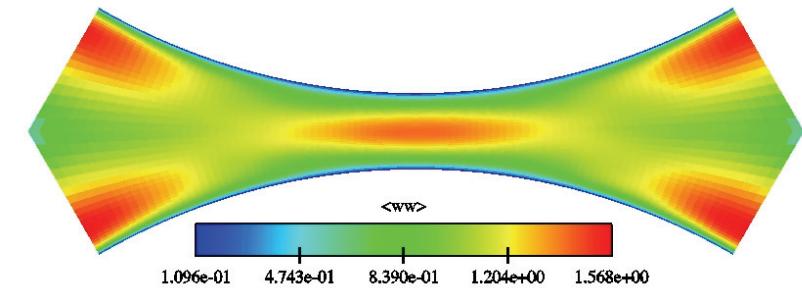
 $\langle u\theta \rangle$ 

	LES6K	LESWPD	HYB6K	HYB39K	EXP
$\tau_w / 0.5\rho U_B^2$	0.0086	0.0025	0.0106	0.0104	0.0057
$U_{B,gap} / U_B$	0.75	0.89	0.77	0.83	0.78

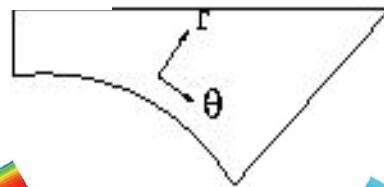
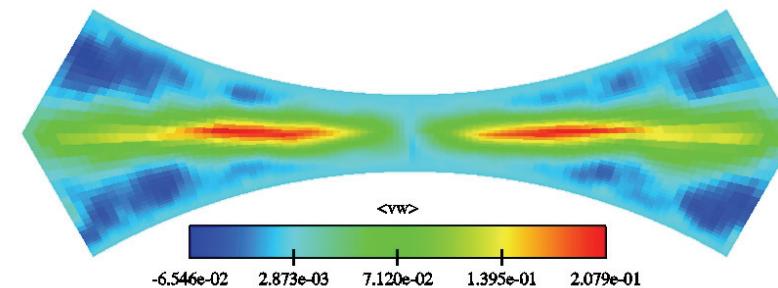
## Results: Reynolds Stress LES P/D=1.06

city  
iter $\langle uu \rangle$  $\langle uu \rangle$   
2.143e-01 9.348e-01 1.655e+00 2.376e+00 3.096e+00 $\langle uv \rangle$  $\langle uv \rangle$   
1.198e-04 2.376e-01 4.751e-01 7.125e-01 9.500e-01 $\langle vv \rangle$  $\langle vv \rangle$ 

4.869e-03 2.478e-01 4.908e-01 7.337e-01 9.767e-01

 $\langle uw \rangle$  $-\langle uw \rangle$   
-2.513e-01 1.403e-01 5.318e-01 9.234e-01 1.315e+00 $\langle ww \rangle$  $\langle ww \rangle$ 

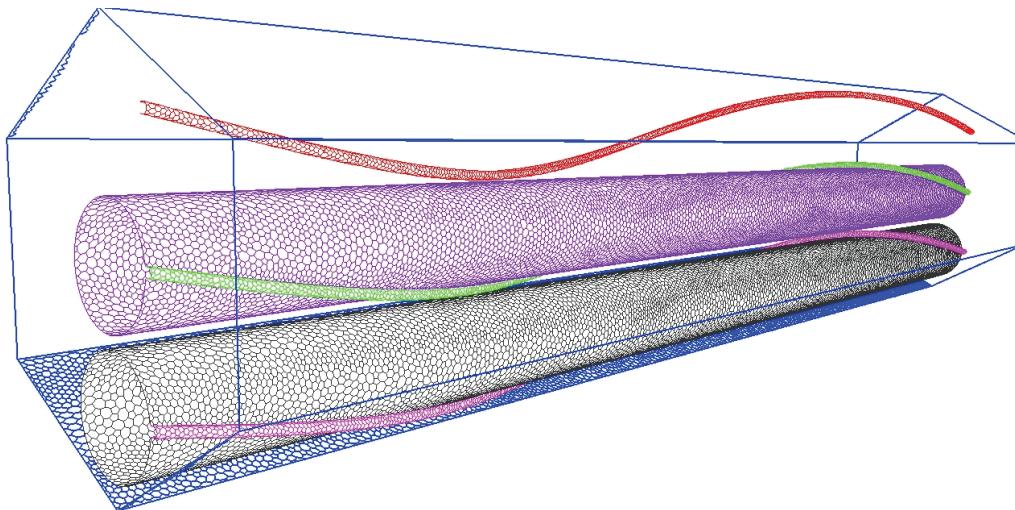
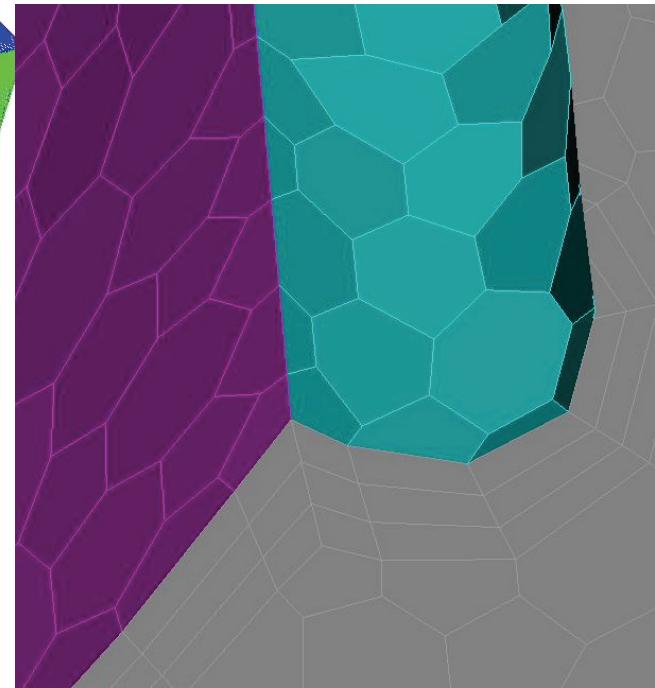
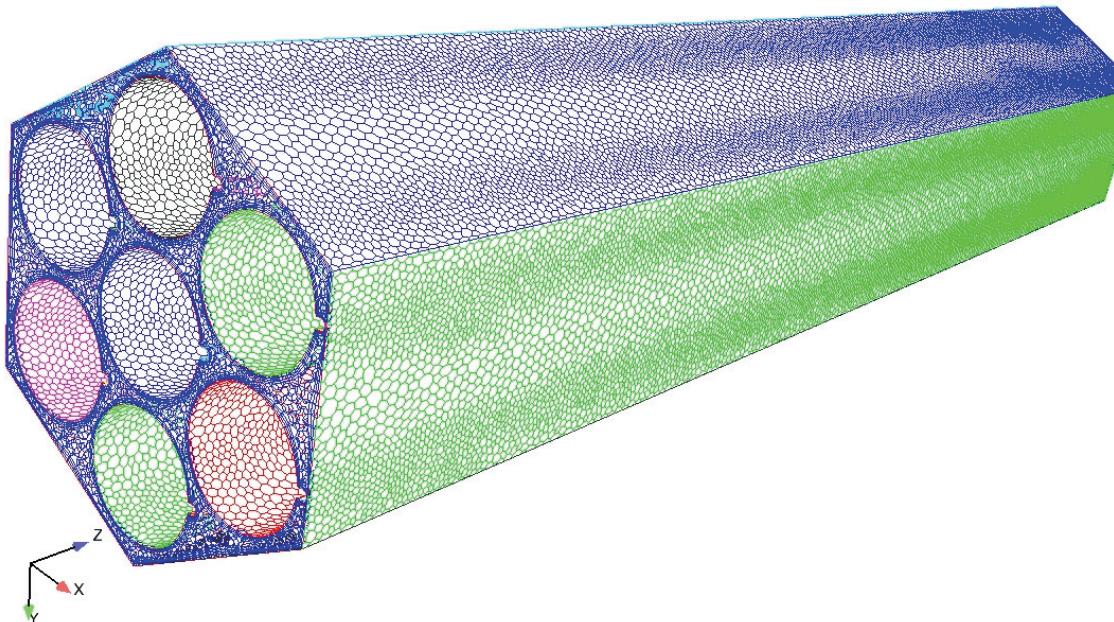
1.096e-01 4.743e-01 8.390e-01 1.204e+00 1.568e+00

 $\langle vw \rangle$  $\langle vw \rangle$ 

-6.546e-02 2.873e-03 7.120e-02 1.395e-01 2.079e-01

# SFR assembly (with C. Penniguel)

Proposal of EdF for the GEN IV reactors



Same geometry presented before with the addition of a wire wrapped around the fuel pin.

# Conclusions.

## ⇒ LES

- Flow Fluctuations detected,
- Presence of a second dominant frequency has to be verified with bigger domain.

## ⇒ Hybrid

- Flow pulsations detected and dominant frequency in according with LES
- Improvement of the blending function for RANS/LES coupling using an elliptic blending (following the work of F. Billard on the  $\alpha$  parameter)

## ⇒ KNOO – Heat transfer test cases: expansion of the TWiki portal.

## ⇒ Evaluating possible advantage/disadvantages of polyhedral cells

## ⇒ AGRs: complete 3D study to evaluate possible improvements of the geometrical configuration. (A. Keshmiri)

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