

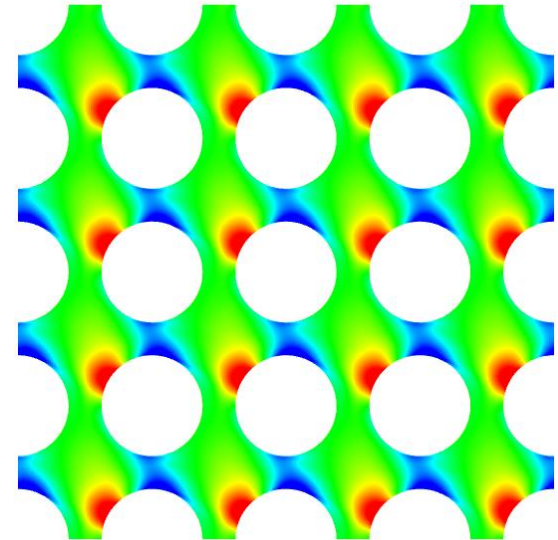
RANS computations of a quasi-axial flow in an in-line tube bundle

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CHANGER L'ÉNERGIE ENSEMBLE

Outlook

- Context
- Objectives and strategy
- Configuration
- Results
- Conclusion and perspectives

Context

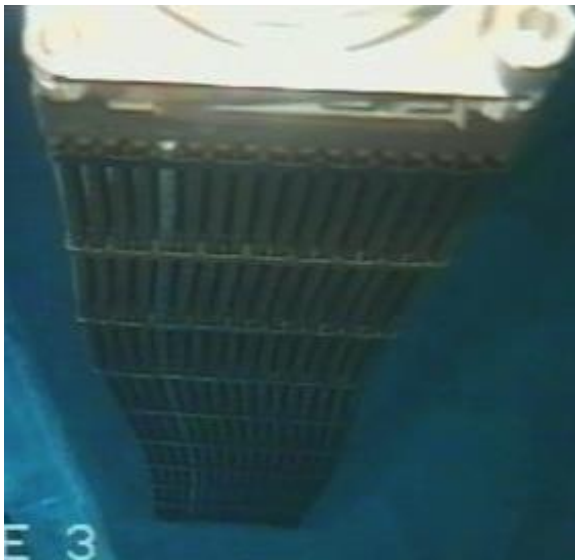
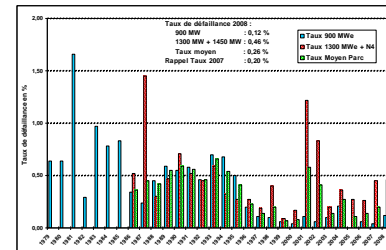
Context / Fuel assemblies issues

❑ Reliability and performance of Fuel assemblies in the core

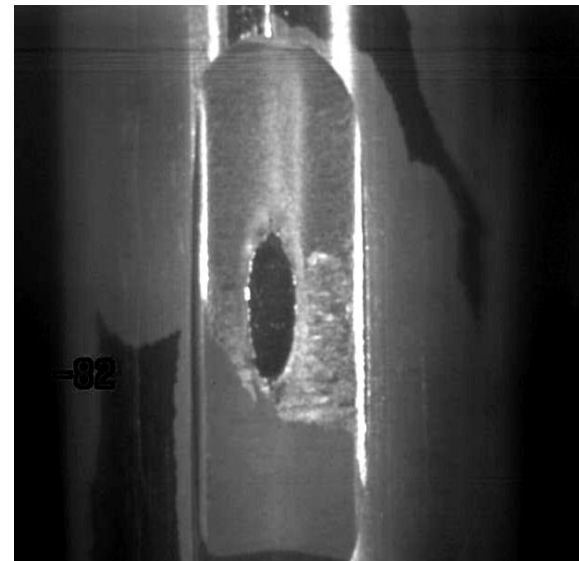
- 25 days of non-availability due to problems concerning the fuel assemblies (2008)



2 major issues



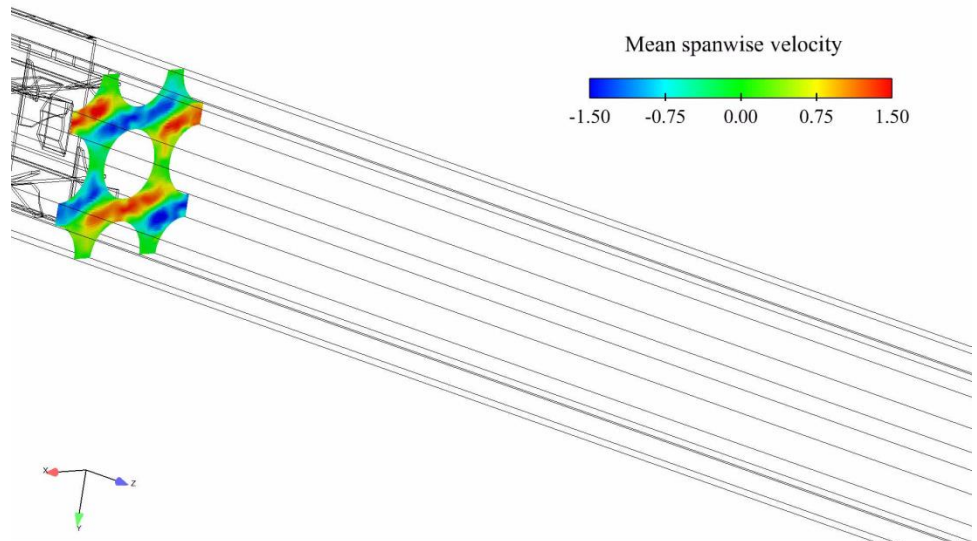
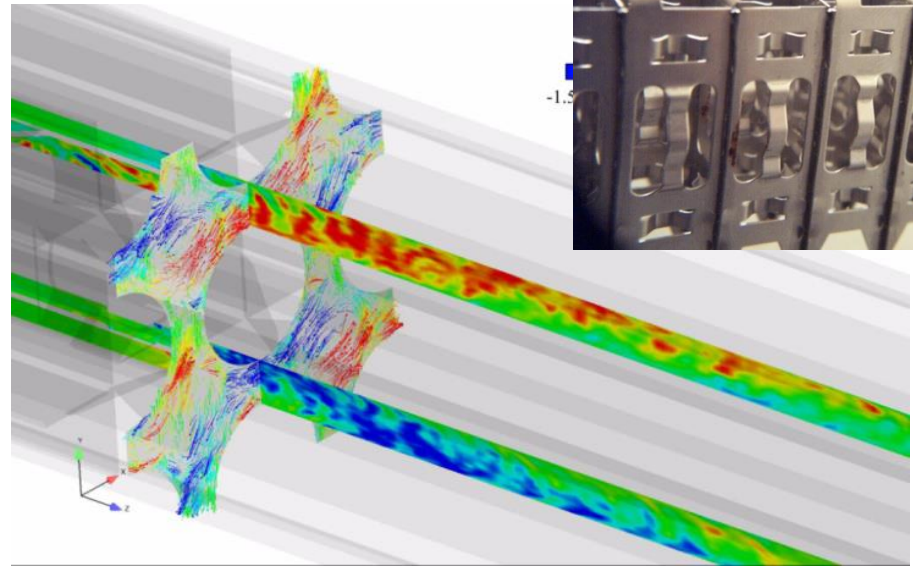
Deformations (RANS)



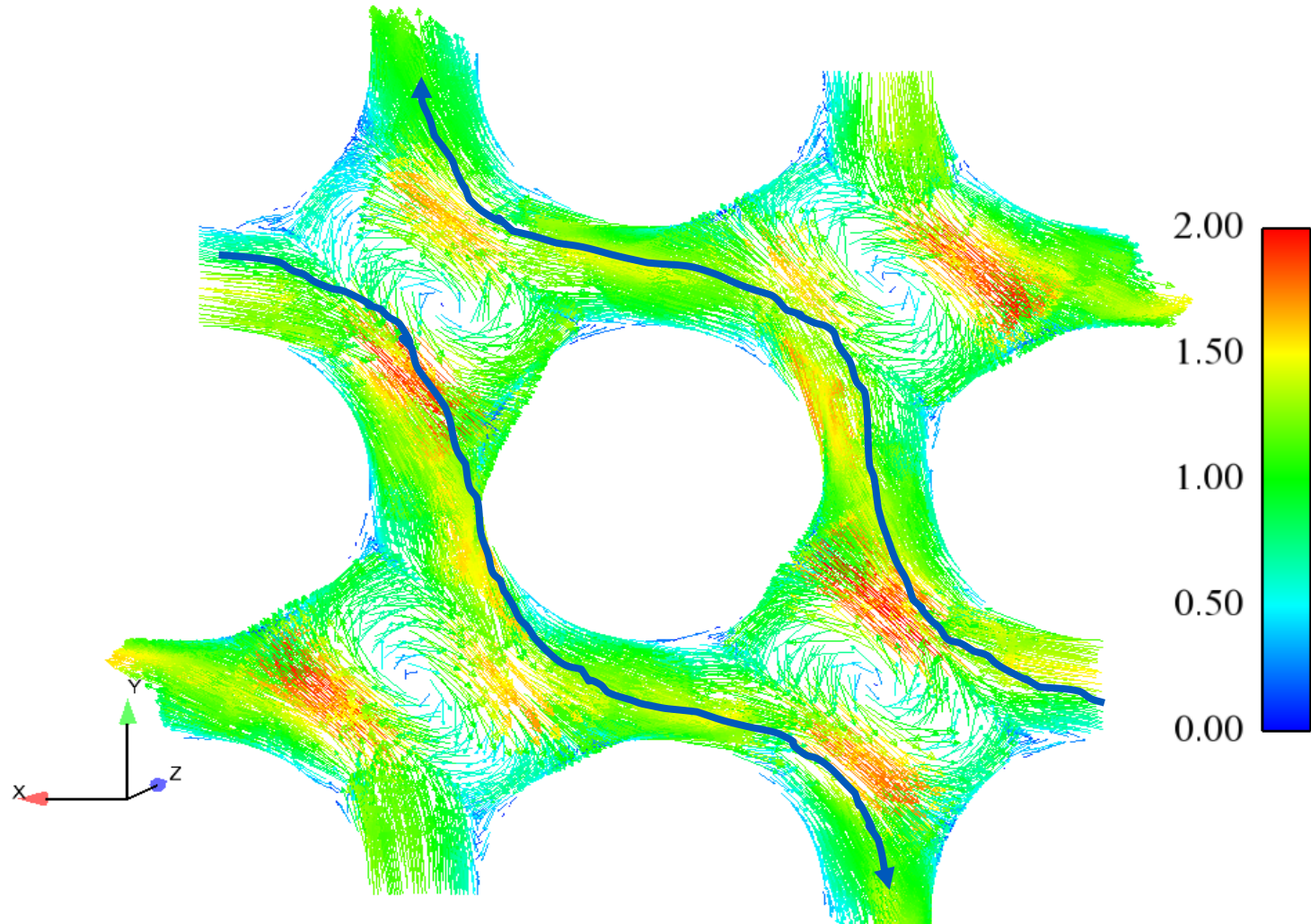
Fretting, vibrations (LES)

Context / strong cross-flow

- ❑ Transverse velocity component downstream a typical mixing grid (previous LES computations on a 2x2 fuel assembly with periodic boundary conditions)
- ❑ Very high local values, up to 50% of the stream-wise bulk velocity in the narrower region
- ❑ Thus, inclined flows in the bare bundle
- ❑ Almost, nothing in the littérature for quasi axial-flows in bare bundles (in particular for pressure drop coefficients, exp. Difficult/impossible to carry out)



Context / strong cross-flow



Objectives and strategy

Objectives / Strategy

- ❑ General objective: understanding the dynamics of the quasi-axial flow through square tube bundles
- ❑ Need of pressure drop coefficient to be used in coarser approaches (such as the ones used in THYC or CATHARE to simulation the whole core of a vessel)
- ❑ Actual objective: Prediction of pressure drop coefficients for quasi-axial flows in a typical PWR fuel assembly tube bundle.
- ❑ Long term strategy:
 - Validation of RANS for pure axial flow coefficients at different Reynolds numbers against available experimental data
 - Validation of a Reynolds Averaged Navier-Stokes (RANS) approach for few quasi-axial flows computed with Large Eddy Simulation (LES) at a given Reynolds number (no exp. available to the authors' knowledge)
 - Performing parametric RANS studies in order to extract correlations

Objectives / Strategy

□ Strategy for RANS approaches :

- **Mesh** sensitivity study
- Study of the sensitivity to **the dimension of the bundle (tubes number)**
- Sensitivity to the **turbulence model**

=> Leads to **one** choice at the end to perform parametric studies

Configuration

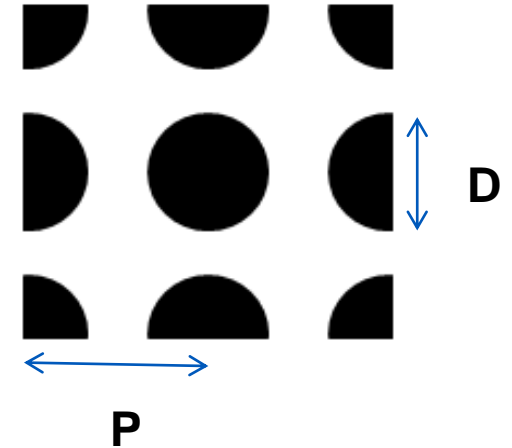
Configuration / Typical computation

- RANS modeling
- Tri-periodic boundary conditions
- One imposes the pressure loss in the three directions

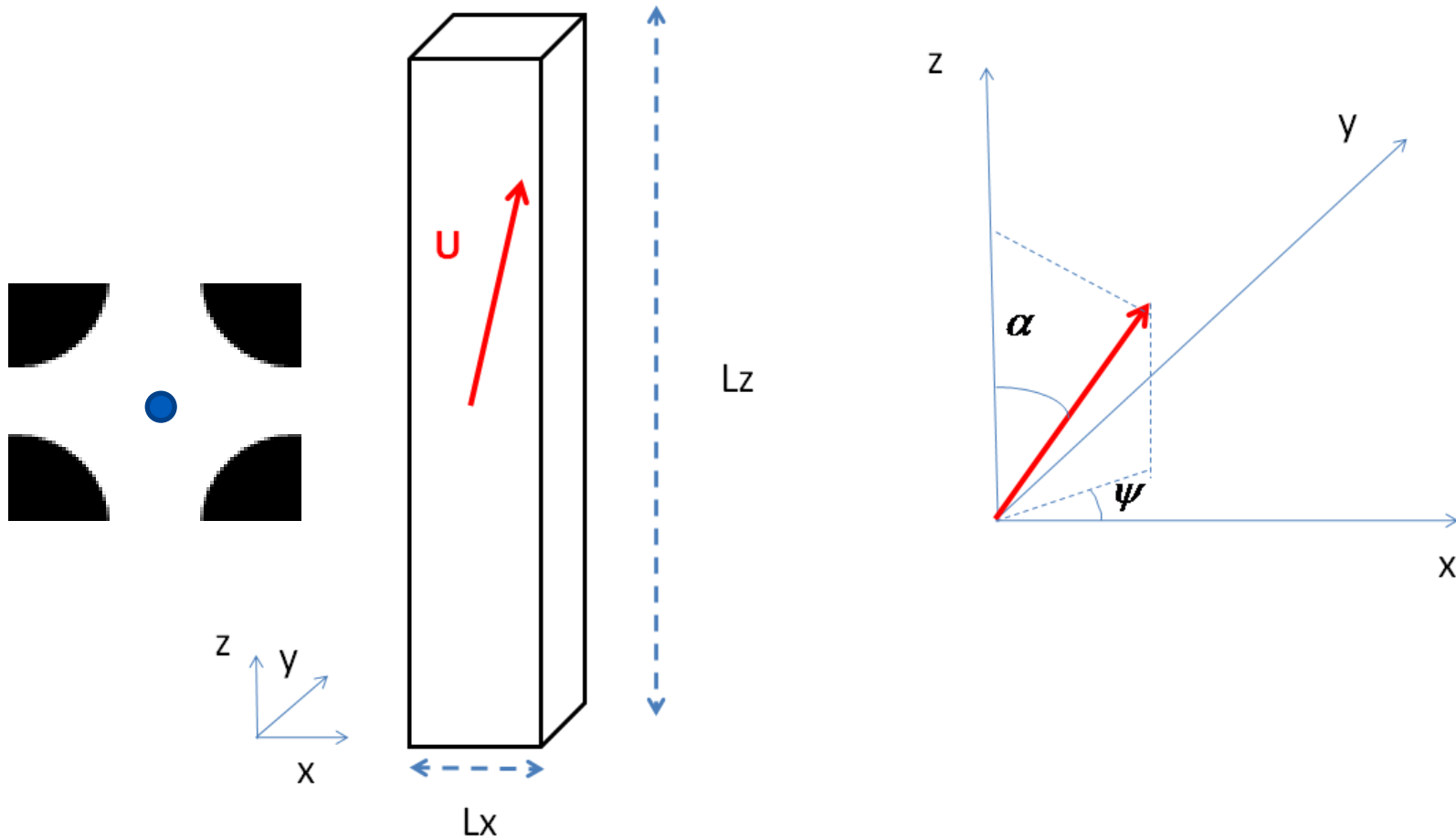
$$\frac{\partial \bar{u}_i}{\partial t} + \frac{\partial (\bar{u}_i \bar{u}_j)}{\partial x_j} = -\frac{1}{\rho_0} \frac{\partial \bar{p}}{\partial x_i} + \nu \frac{\partial^2 \bar{u}_i}{\partial x_j \partial x_j} - \frac{\partial \overline{u'_i u'_j}}{\partial x_j} + S_i$$

$$\frac{\partial \bar{u}_j}{\partial x_j} = 0$$

- The axial Reynolds number is always close to 50000 and a pitch to diameter ratio **P/D=1.326**
- 2D meshes (only one cell in the z direction) with hexadral conforming cells
- Mesh created with Salomé



Configuration / Quasi-axial flows in tube bundles



$$\text{Re}_H = \frac{UD_H}{\nu}, \quad \xi_i = \frac{2S_i D_H}{\rho U_i^2}$$

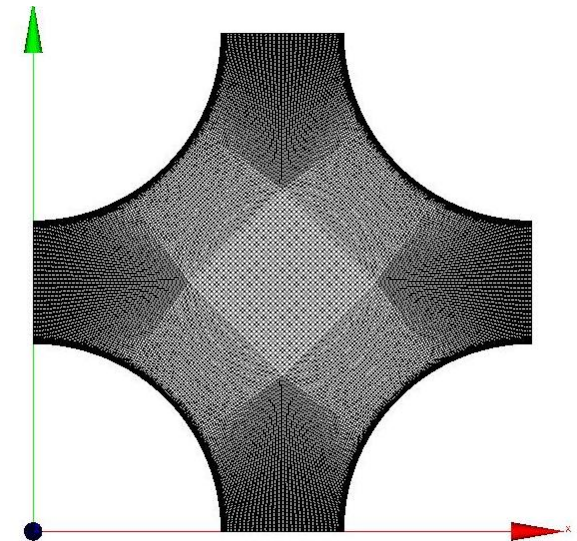
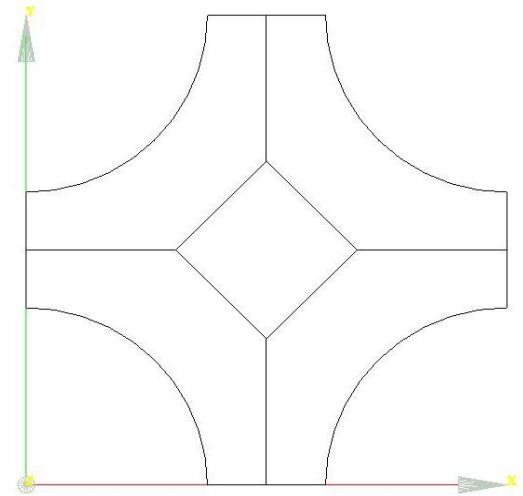
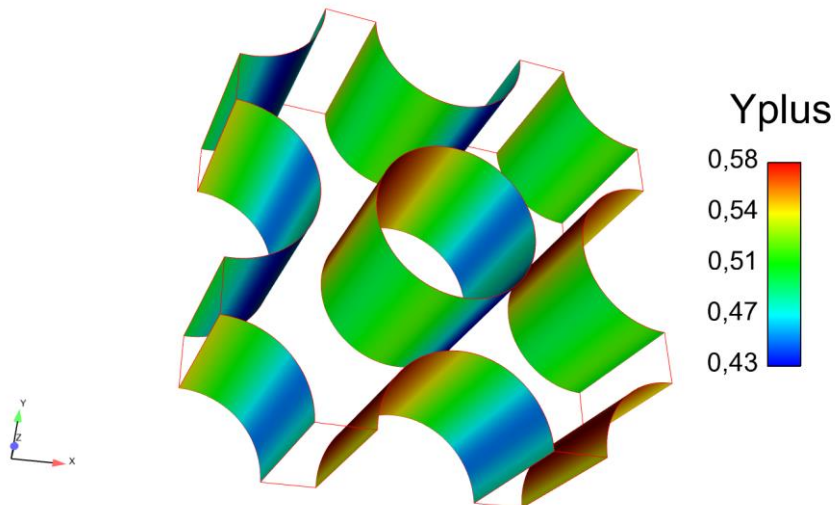
Mesh generation

□ Strategy :

- Creation of the geometry with the **GEOM** module
- Meshing with the **SMESH** module
- Use of the **dump study** function to create a Python file

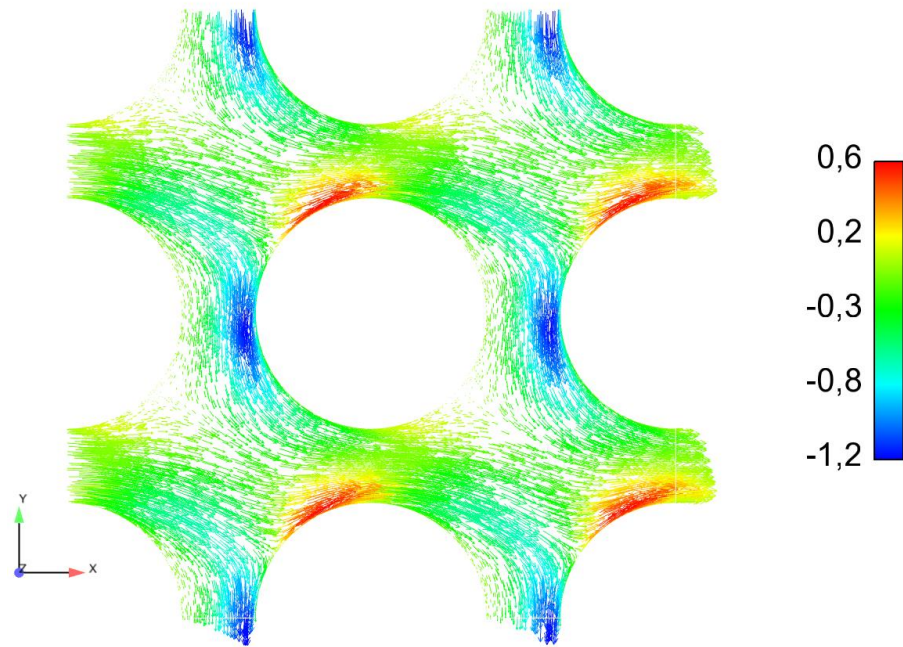
□ Advantages :

- The mesh and the geometry are **fully customizable** and easy to re-create

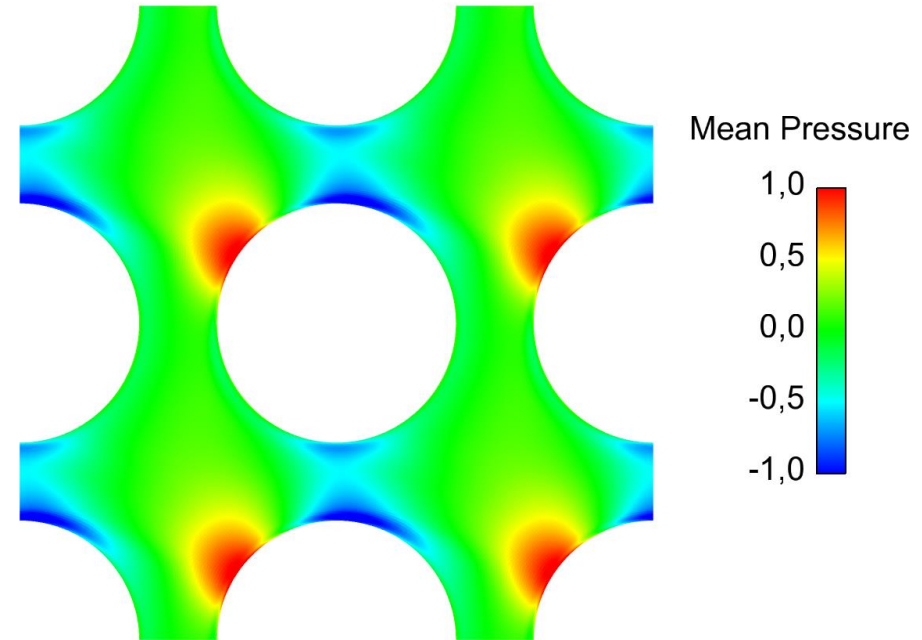


Results

Results / Major issue (asymmetry)



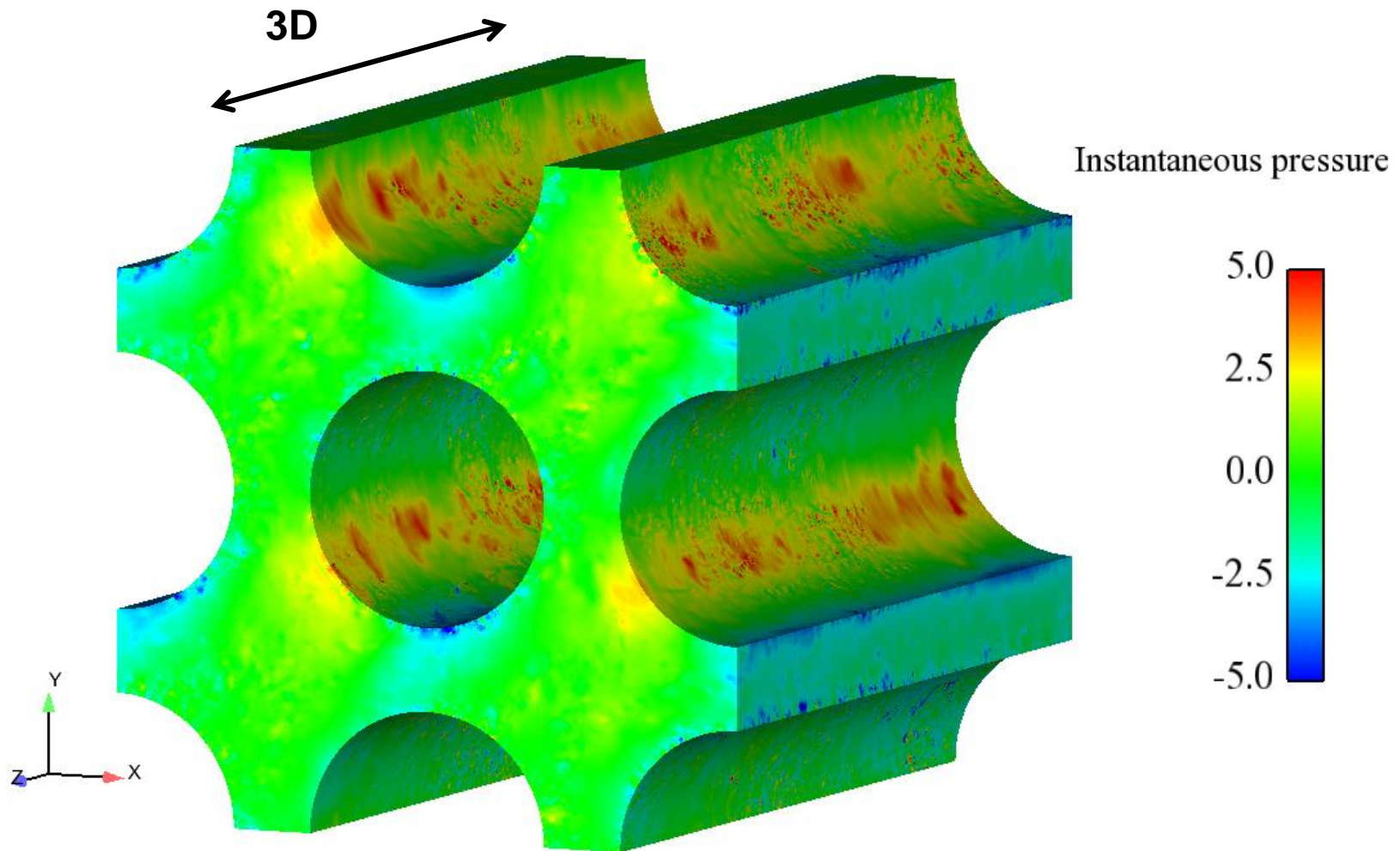
Mean transverse velocity vector coloured by the mean transverse velocity in y direction, 2×2 , $S_u=0,5$, $S_v=0$, $S_w=1$



Mean pressure, 2×2 , $S_u=0,5$, $S_v=0$, $S_w=1$

- Considering the symmetry of the configuration, one should *a priori* have $\psi=0$ and $\alpha=?$
- One obtains here $\psi=23^\circ$ and $\alpha=2^\circ$
- This asymmetry is observed in the very first LES computations

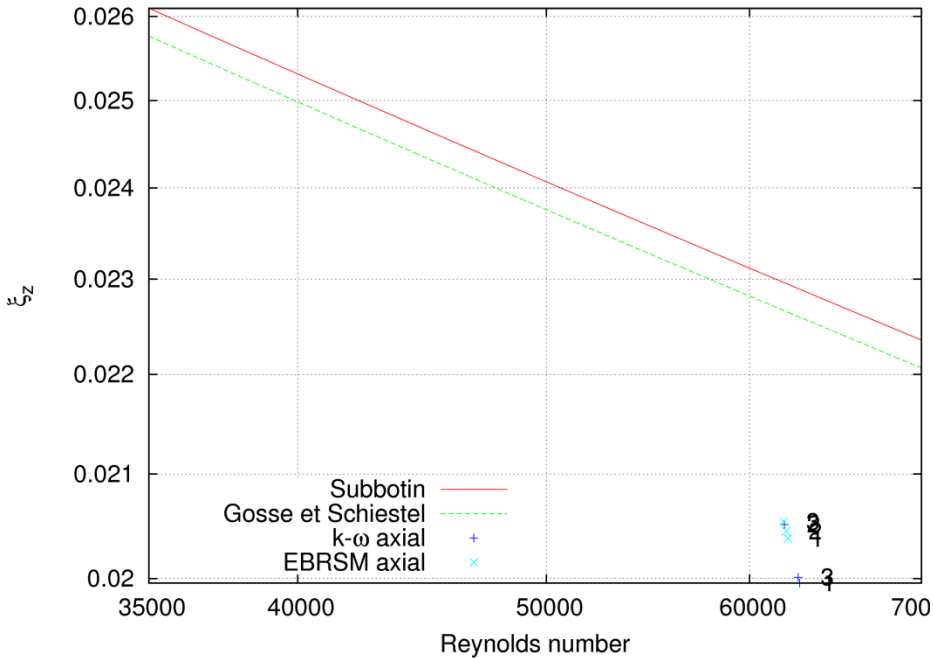
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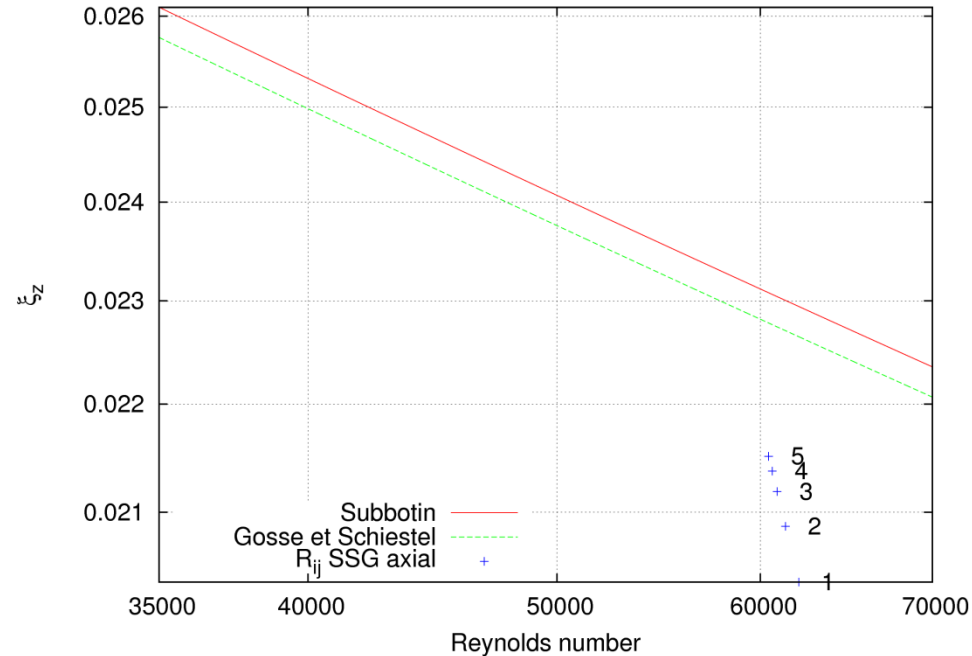
Instantaneous pressure field with LES (100 M cells), 2×2 , $S_u=1$, $S_v=0$, $S_w=1$

Results / Mesh Sensivity

- ❑ 2x2 tube bundle, P/D=1.326
- ❑ Different mesh raffinements
- ❑ Sw=1, Sv=0, Re~62,000
- ❑ Axial pressure loss coefficient



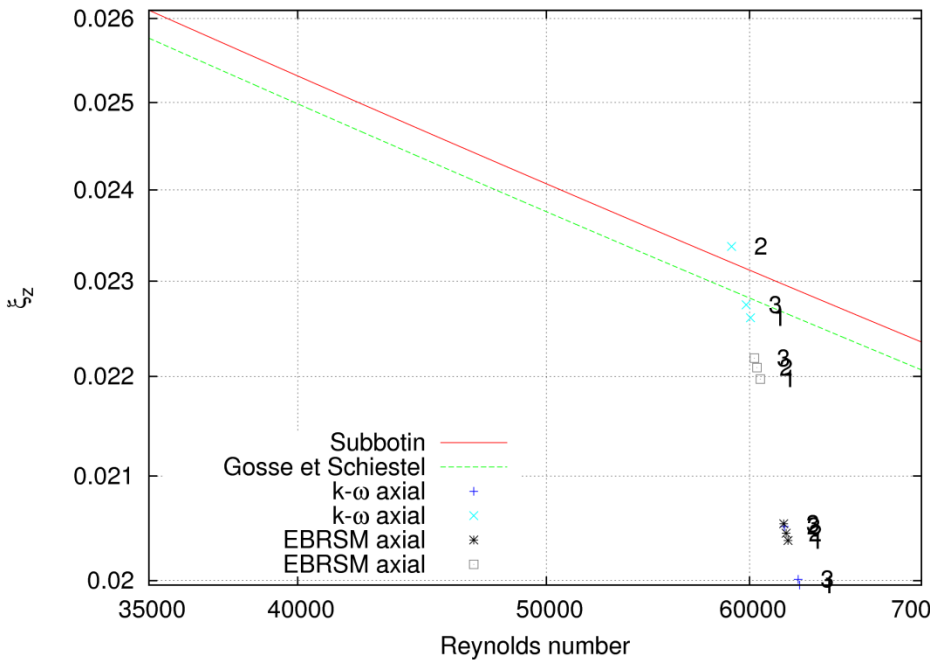
Low Reynolds Number models



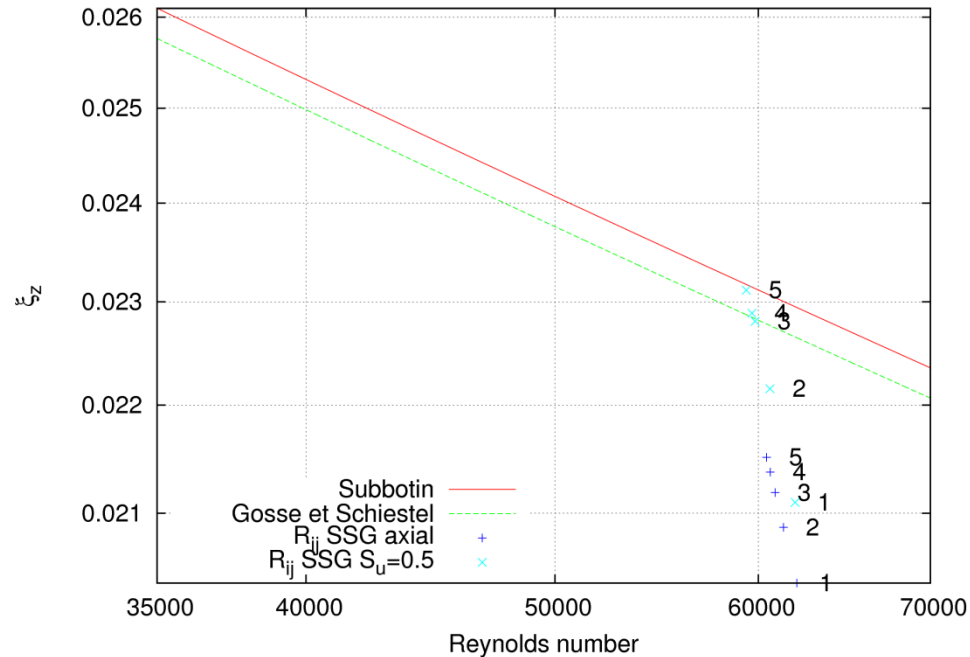
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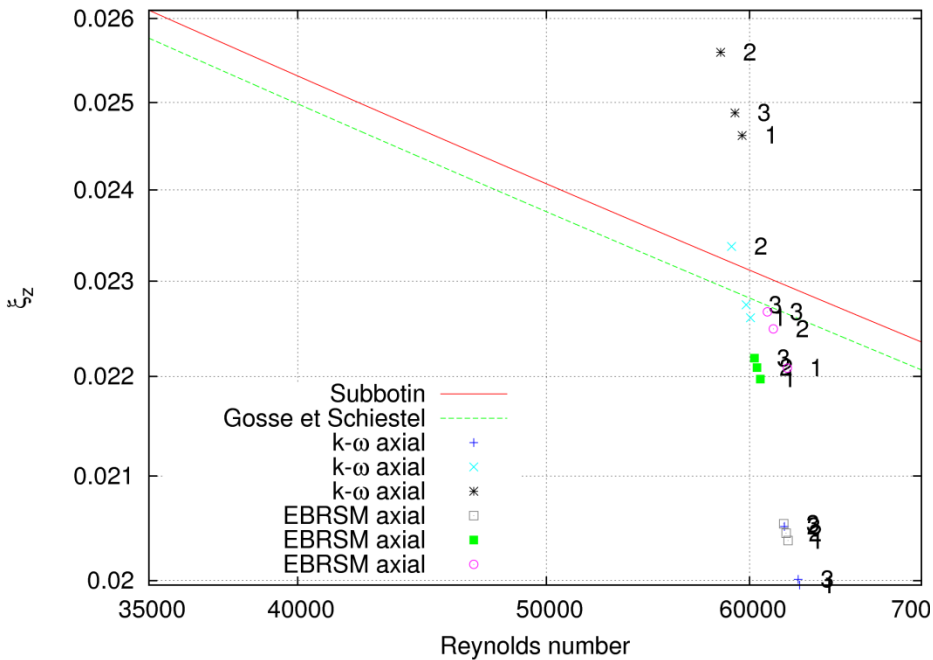
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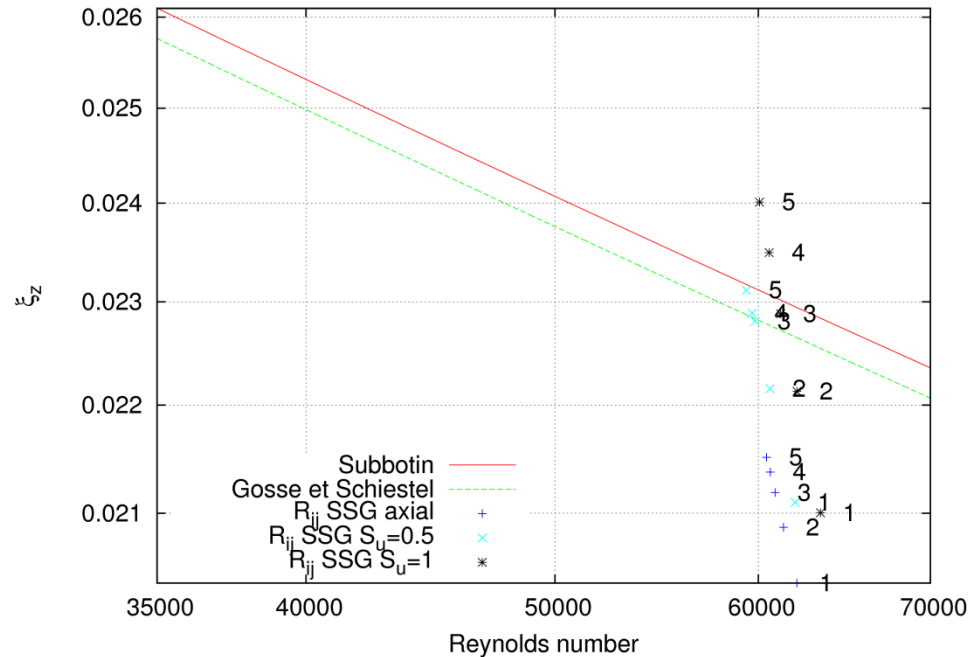
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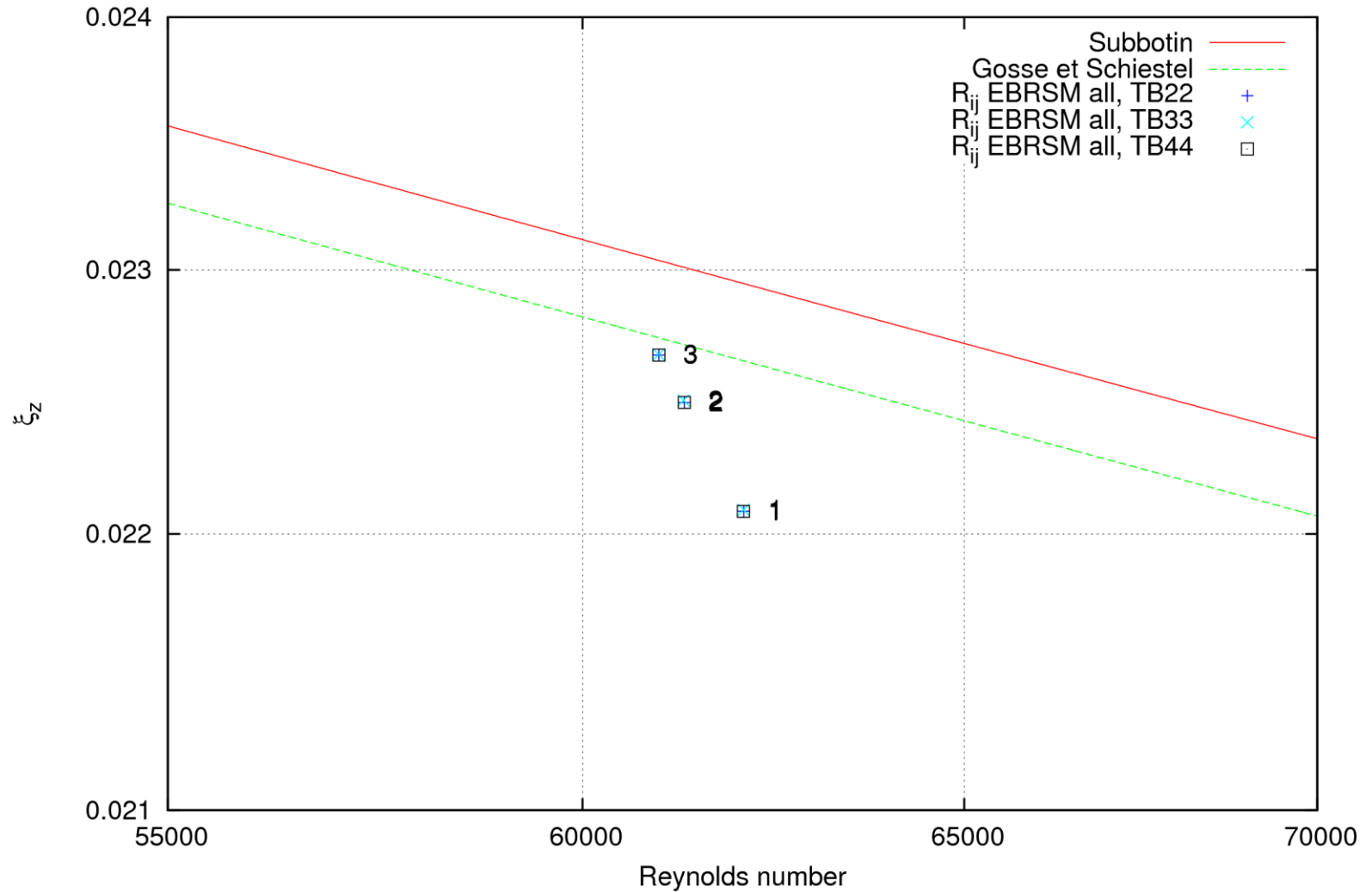
Low Reynolds Number models



High Reynolds Number models

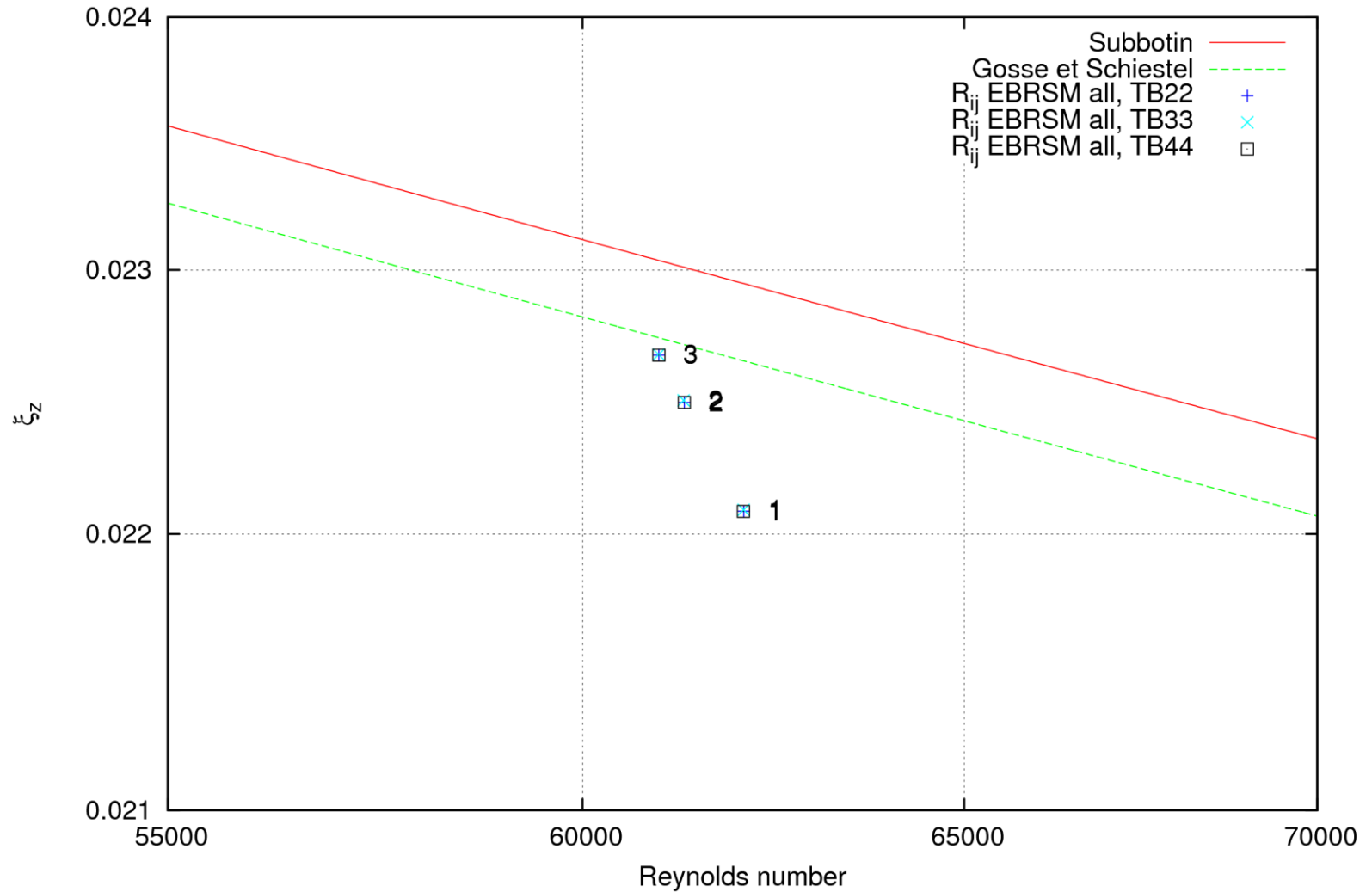
Results / Sensivity to the bundle size

Influence of the dimension of the bundle on the axial pressure loss, $Su=1$



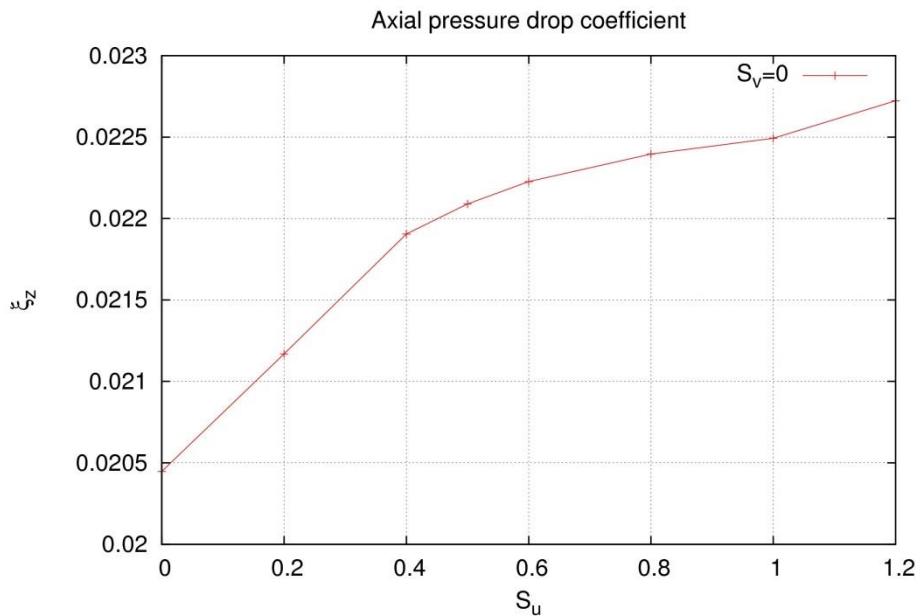
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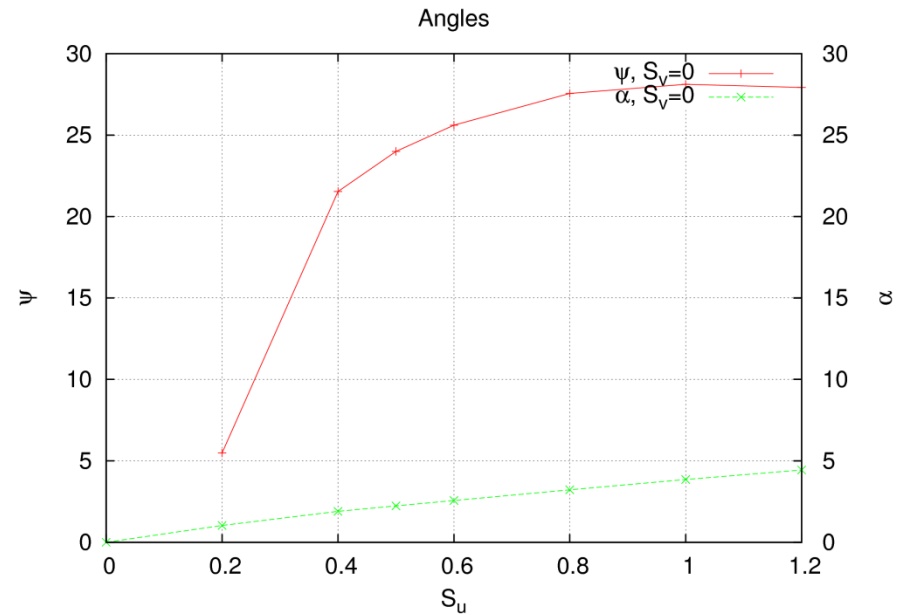


Results / Variation of the S_u source term

- ❑ 2x2 tube bundle, P/D=1.326
- ❑ Sw=1, Sv=0, Re~62,000
- ❑ Axial pressure loss coefficient and angles of the configuration



Axial pressure loss coefficient

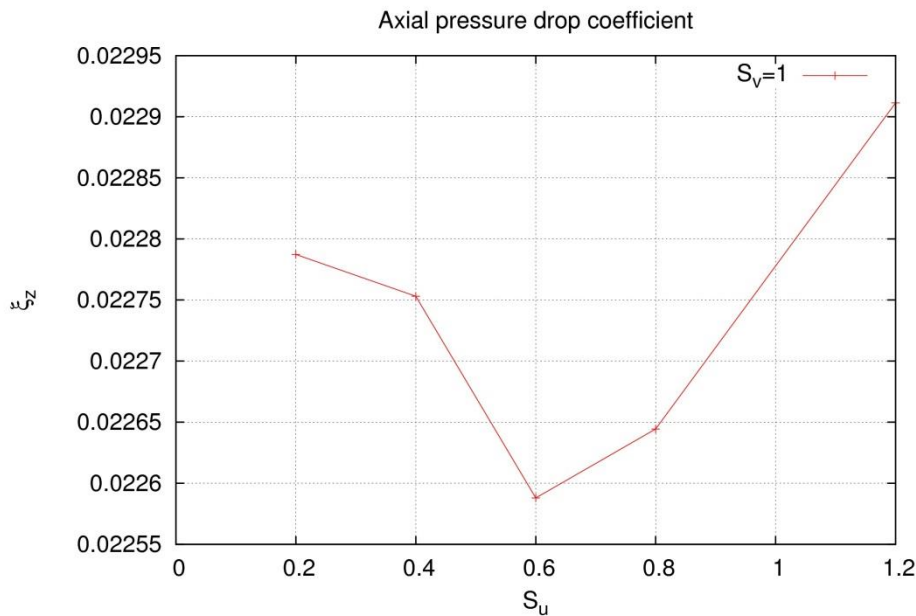


Angles of the configuration

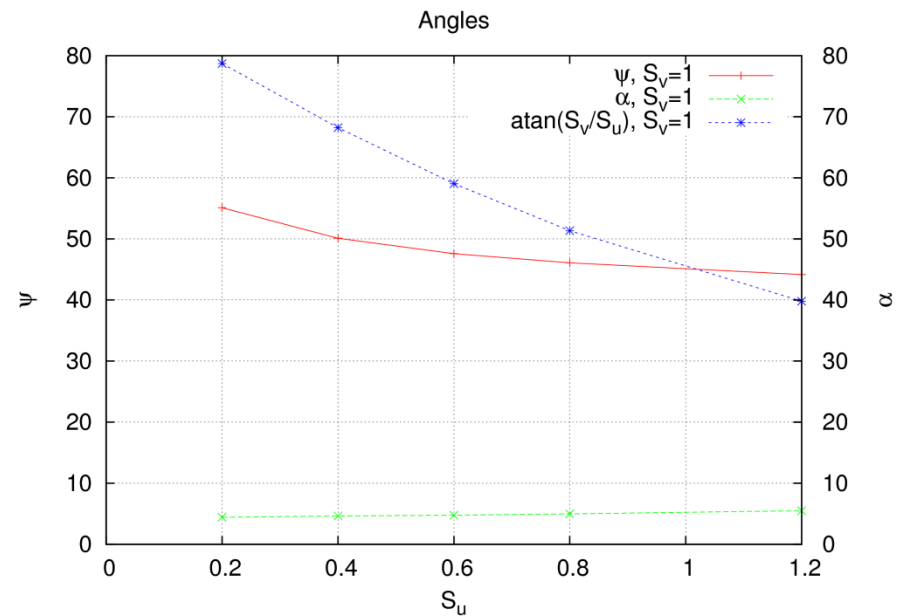
➤ The authors start to think that this configuration is physically impossible!

Results / Variation of the S_u source term

- ❑ 2x2 tube bundle, P/D=1.326
- ❑ Sw=1, Sv=1, Re~62,000
- ❑ Axial pressure loss coefficient and angles of the configuration



Axial pressure loss coefficient



Angles of the configuration

Conclusions

Conclusions / Our results

- ❑ Sensitivity studies for RANS computations :
 - No effect of the tubes number
 - Only low Reynolds Number approaches seems to converge
 - Good convergence of the EBRSM model

- ❑ « Unexpected » asymmetry of the flow with a strong axial flow

- ❑ Relatively good agreement with experimental correlations

- ❑ Access to data that we couldn't get with experimental approaches.

Conclusions / More computations to come ...

- ❑ **Very fine LES** now running
- ❑ A lot of questions remain unsolved, other configurations to test
- ❑ Increase of the Reynolds Number for RANS simulation (reactor Reynolds number~500000)
- ❑ **Final goal :**
 - **Correlations between head losses in the three directions, Reynolds number and α angle**

Thanks for your attention