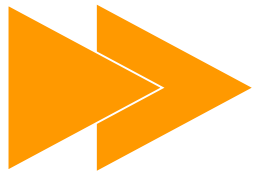


CFD simulations of the temperature behaviour of bitumen mud with *Code_Saturne V4.0*



Overview

Context

Experimental

Geometry and mesh

Boundary conditions and Numerical parameters

Physical properties

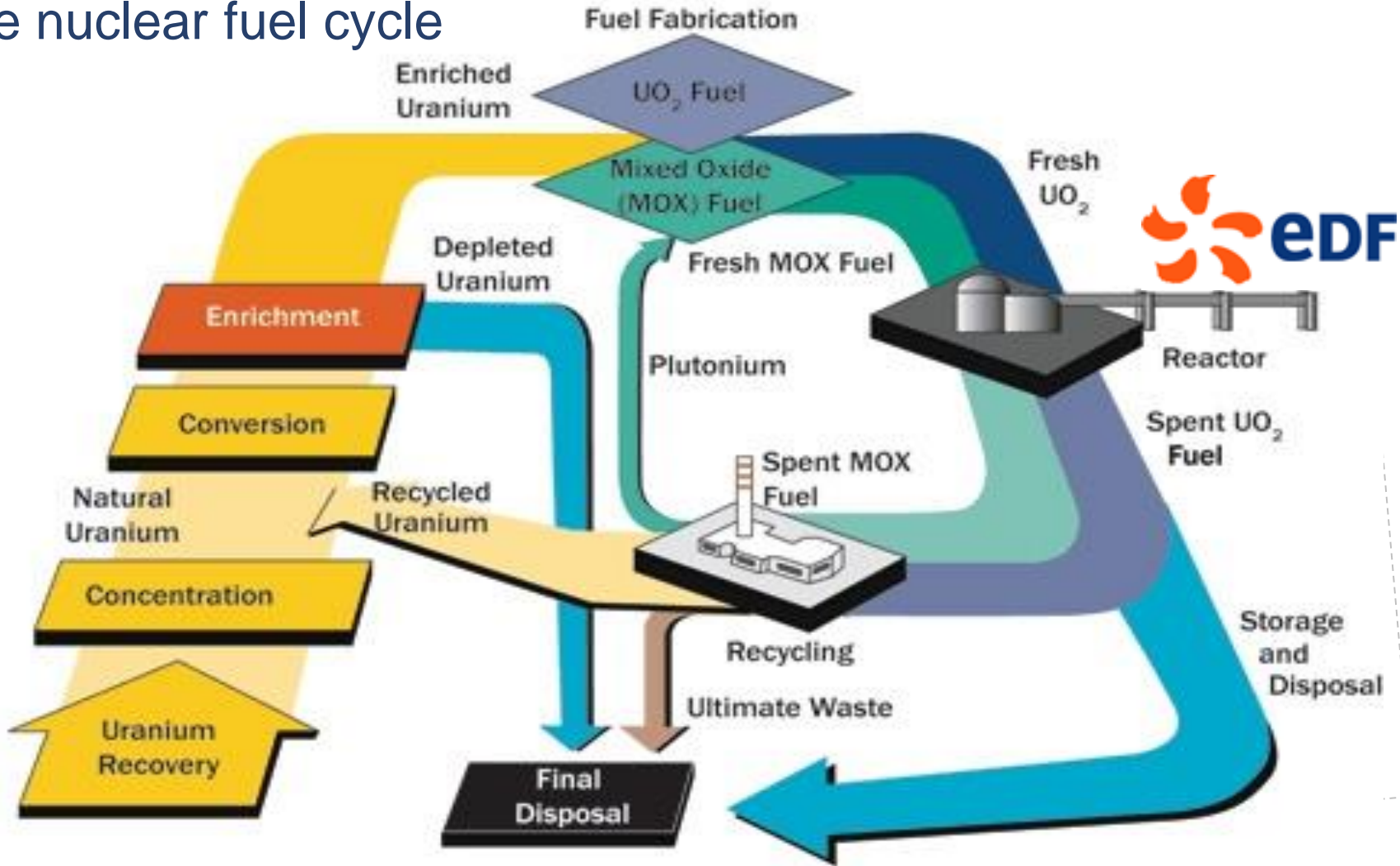
CFD results *Code_Saturne* vs. experimental

CFD results: barrel scale 1



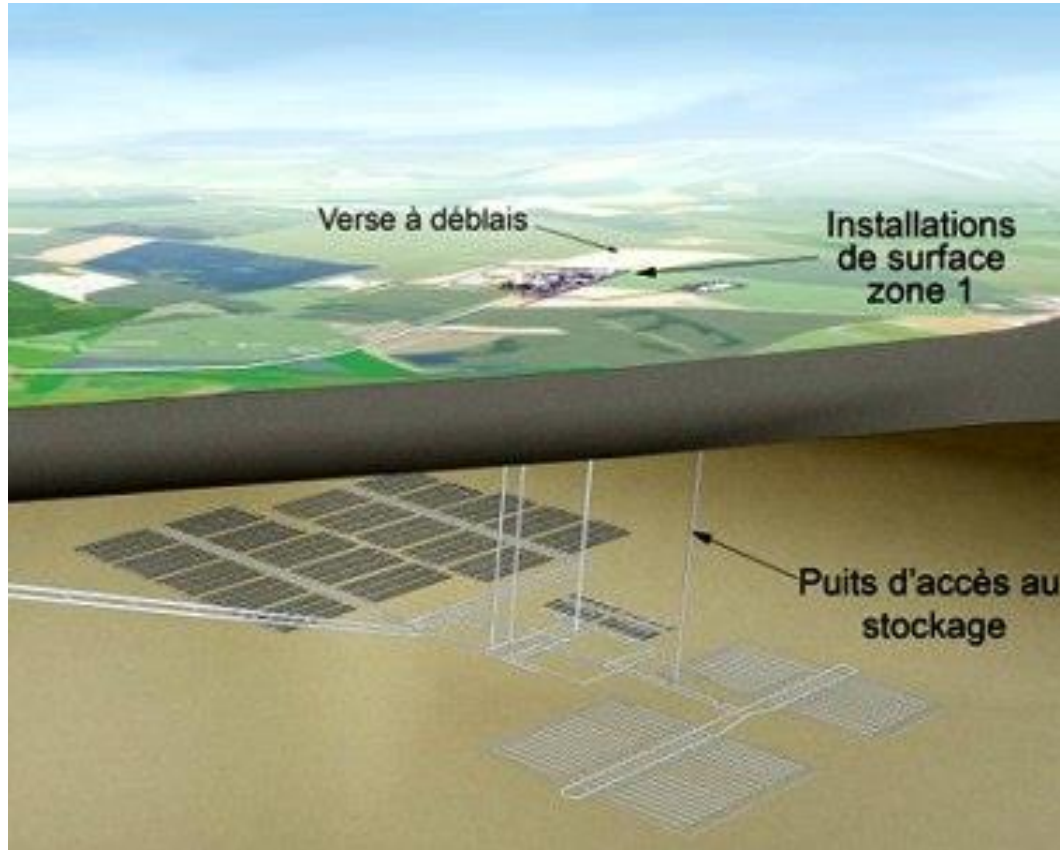
Context

The nuclear fuel cycle





Context





Context

Radioactive wastes in the form of dewatered sludge are incorporated in the bitumen. Bitumen is a derivative of crude oil.

Control of various risks is through simulation and experimentation.

The goal is to contribute to the validation of containment nature of the mixture formed by the bitumen and dehydrated radioactive sludge



Experimental

Bitumen: medium-scales trial (2kg)

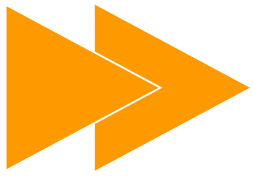
Before studying the behavior of bitumen in a drum, we try to reproduce the behavior of bitumen in a small pot of 2kg.



Exploitation of measurements from trials made by the CEA

Cylindrical pot

- similar to the shape
- preventing lateral heat losses
- radius sufficient for the establishment of the convection loops
- allow to observe the movement of the temperature front
- establishment of thermocouples



Experimental Sensor measure



Changes in temperature over time within the coated subjected to an external heat flux is recorded with probes

Probes radius:

$R_C = 0$ (centrer)

$R_I = 36.2$ (internal)

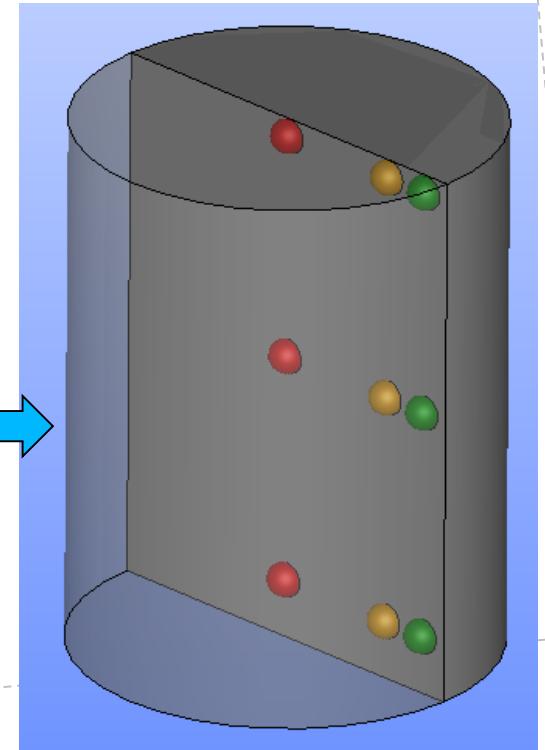
$R_E = 49.5$ (external)

Probes height:

$H_H = 148$ (top)

$H_M = 83$ (middle)

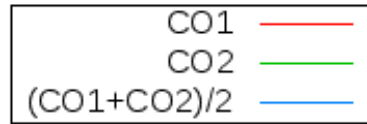
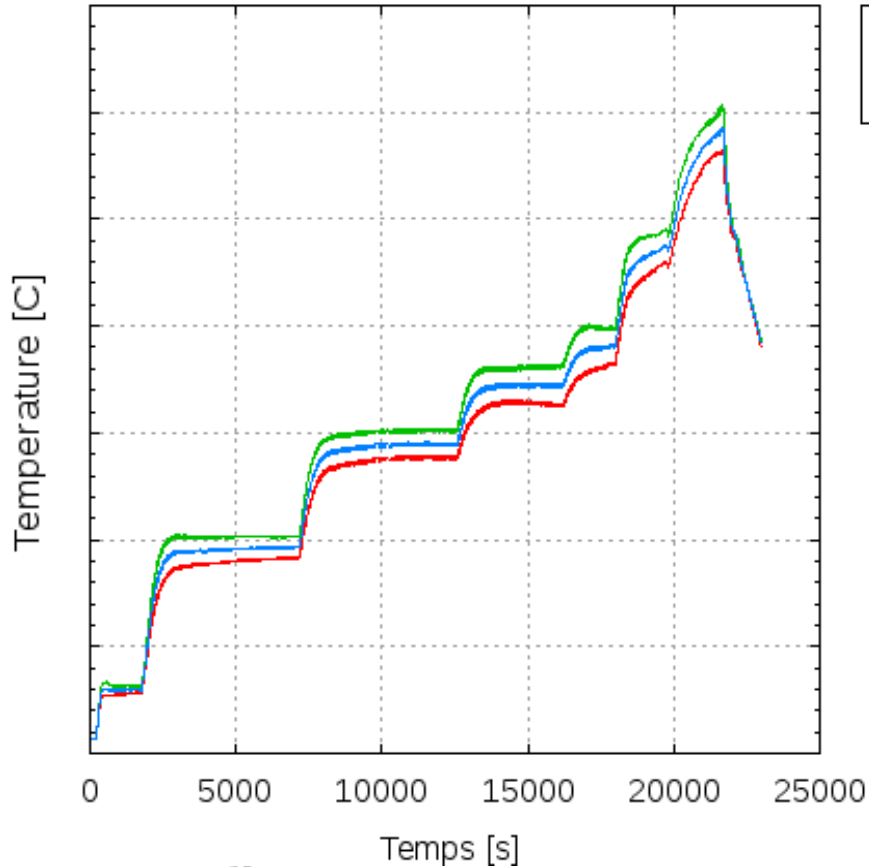
$H_B = 17$ (low)





Experimental Temperature applied on the walls

A heating crown and a temperature control system is used for heating the vertical walls.



Heating
program

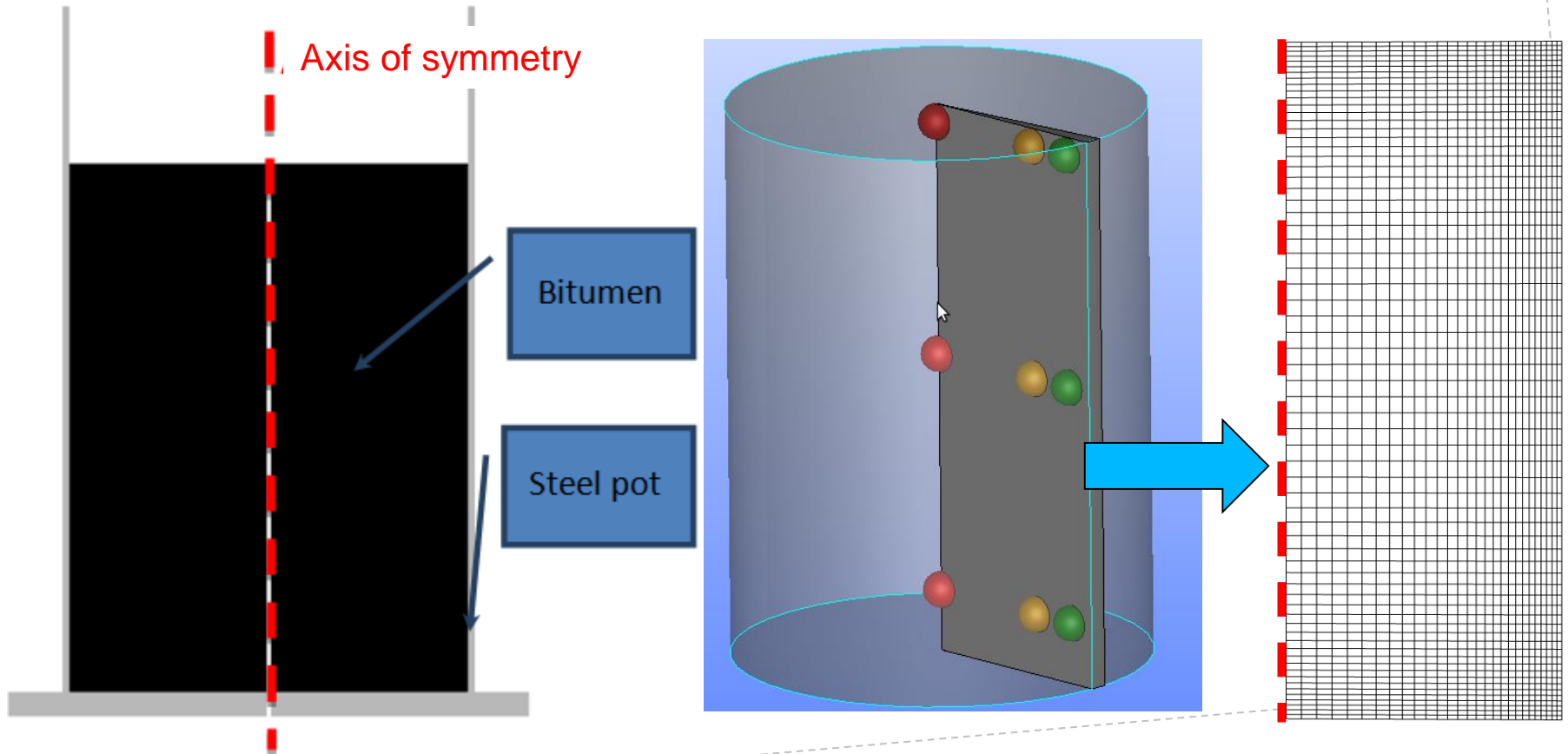
T measure CO1
T measure CO2

On wall for *Code_Saturne*
 $T = (CO1+CO2)/2$

Geometry and mesh

Axisymmetrical bidimensional simulation

Dimension	[m]
Height	0.153
Radius	0.05725





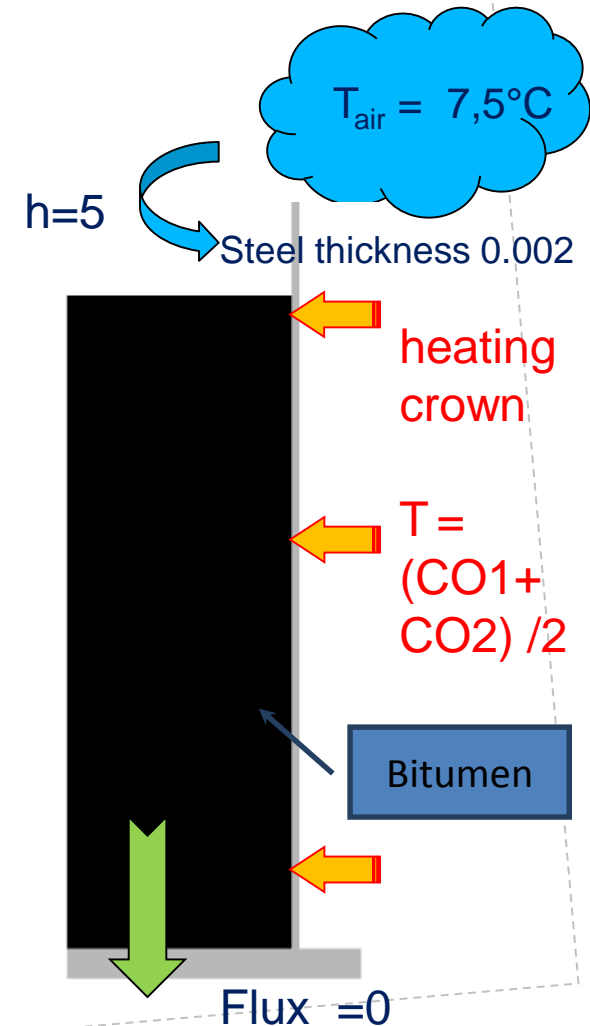
Boundary conditions and Numerical parameters

Axisymmetric 2D model created with version 4.0 of *Code_Saturne* takes into account the following parameters :

- physical properties of the bitumen
- convective exchange surface
- positioning of the heating bracelet
- room temperature
- thermal properties of pot
- source term (chemical kinetics)

A first boundary condition $h=5$ has been tested, then flux =0, the bottom of the barrel based on aerated concrete block insulation.

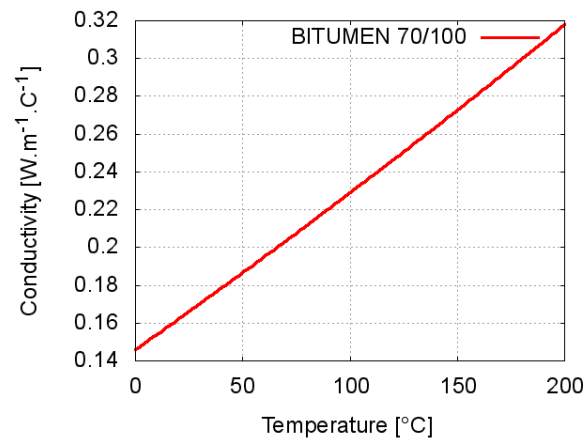
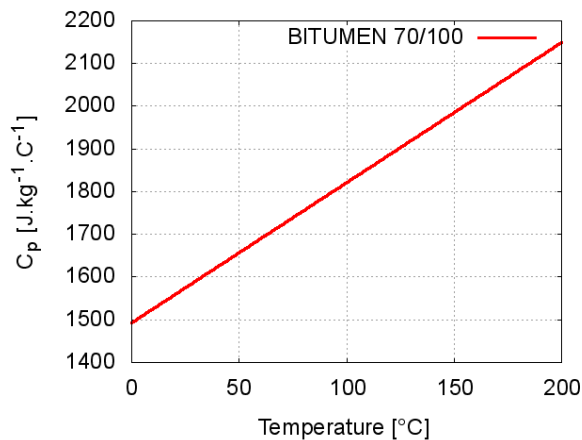
Although even lose heat by conduction with this concrete block, it is difficult to assess the loss.



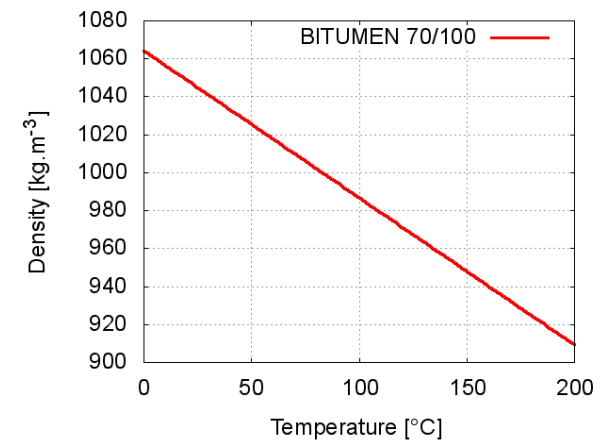
Physical properties

For the first calculations, the physical properties of the bitumen 70/100 was used

Specific heat C_p [$J.kg^{-1}.C^{-1}$]
 $3.29 * T + 1492$



Density ρ [$kg.m^{-3}$]
 $1064.2 - 0.775 * T$



Thermal conductivity λ [$W.m^{-1}.C^{-1}$]
 $3 * 10^{-7} * T^2 + 8 * 10^{-4} * T + 0.1459$

Physical properties

For the first calculations, the physical properties of the bitumen 70/100 was used

Viscosity [Pa.s]
Loi de Carreau-Yasuda

$$\mu(\dot{\gamma}) = \frac{\sigma}{\dot{\gamma}} + \mu_0 a_T [1 + (\tau a_T \dot{\gamma})^a]^{\frac{n-1}{a}}$$

$$\sigma = 0.02 \text{ Pa}$$

$$\mu_0 = 2300 \text{ Pa.s}$$

$$\tau = 2.5 \cdot 10^{-3} \text{ s}$$

$$n = 0.37$$

$$a = 0.55$$

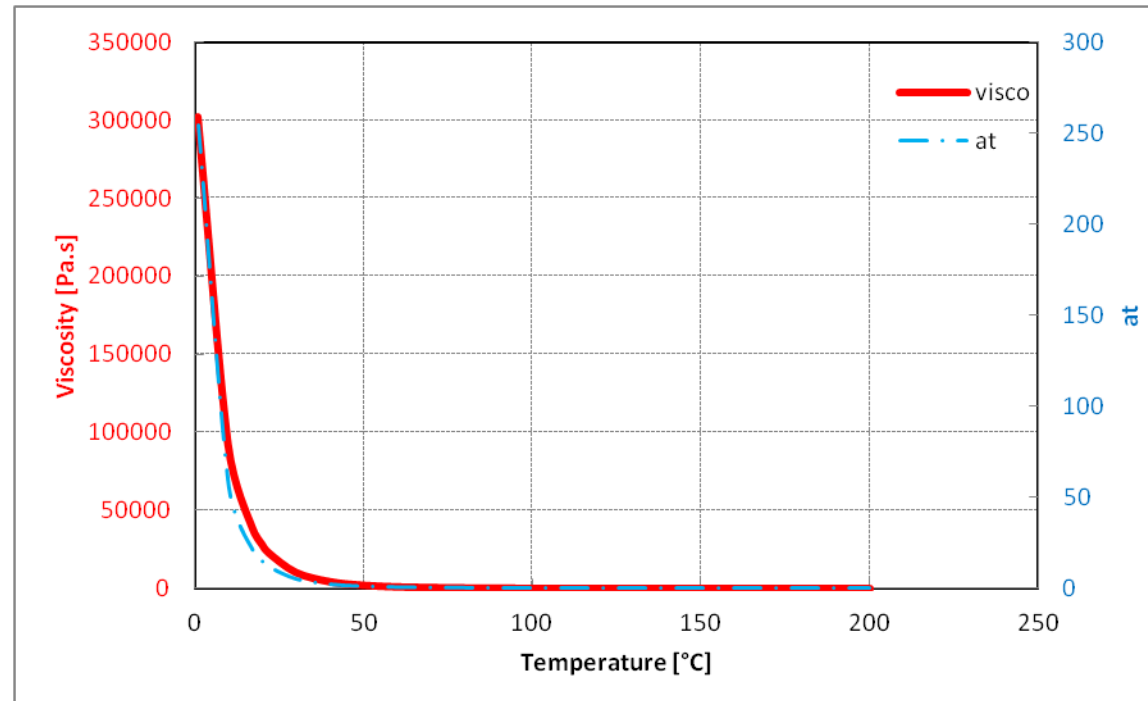
$$C_1^0 = 8.16$$

$$C_2^0 = 121.2$$

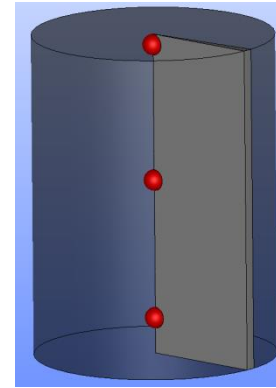
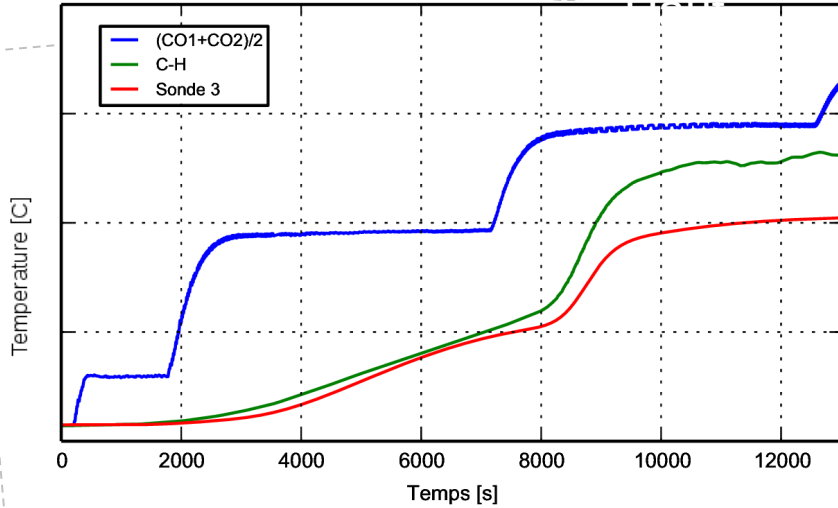
$$T_{ref} = 50^\circ\text{C}$$

Coefficient of friction

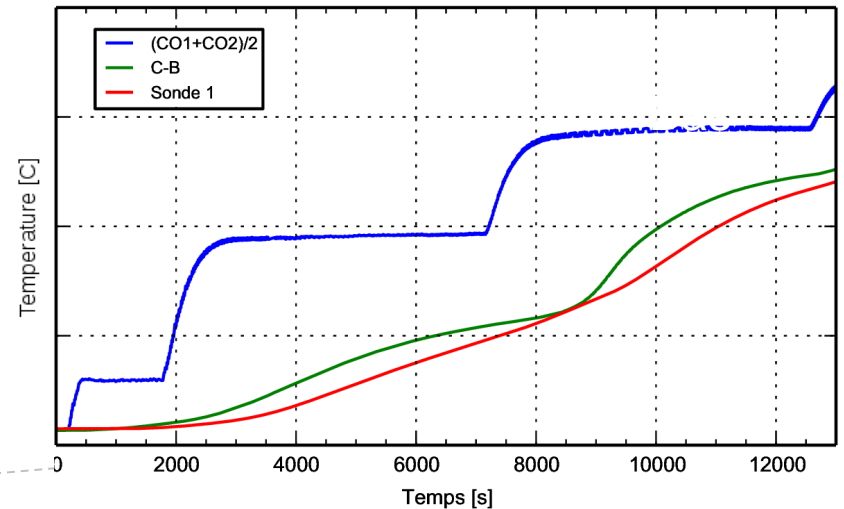
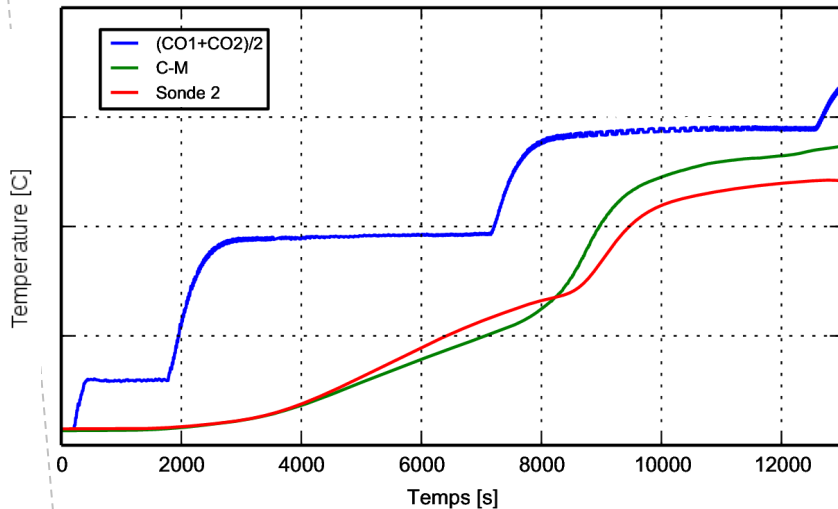
$$a_T = e^{\left[\frac{-C_1^0 (T - T_{ref})}{C_2^0 + (T - T_{ref})} \right]}$$

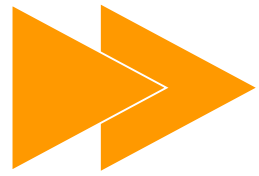


CFD results: *Code_Saturne* vs. experimental data

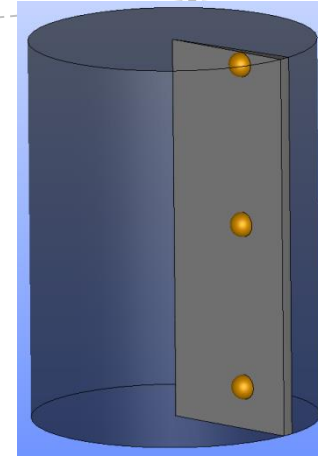
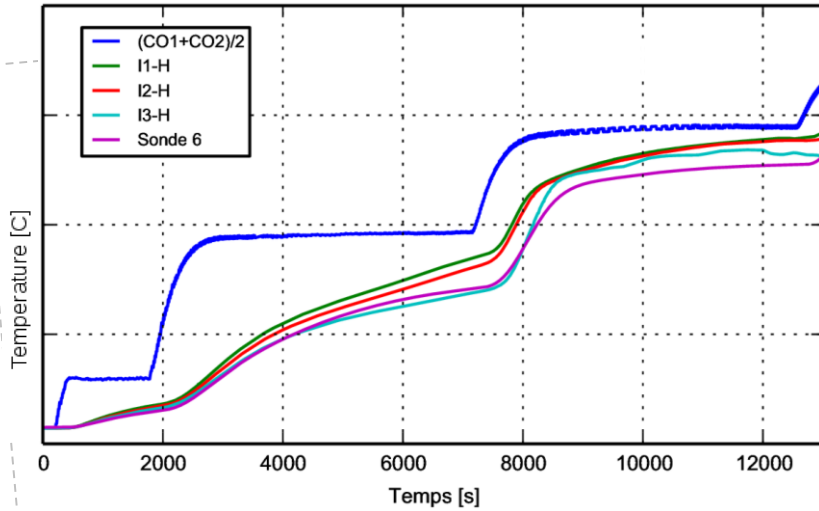


Changing the temperature at the centre

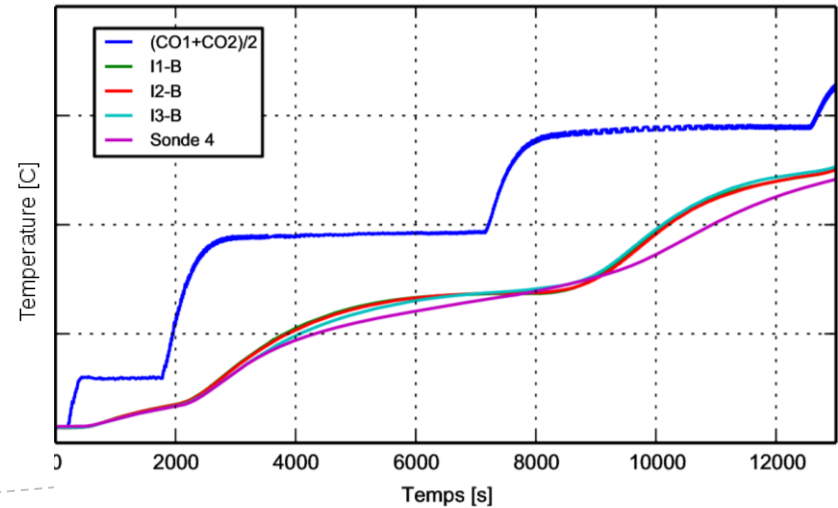
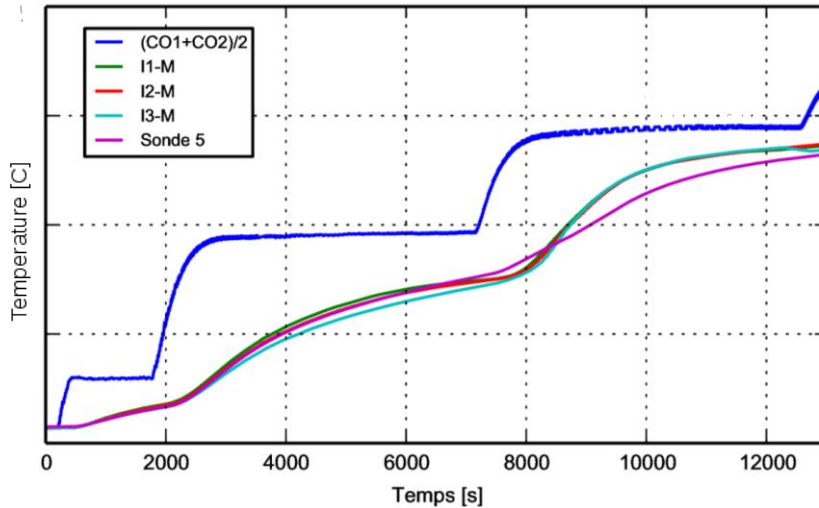




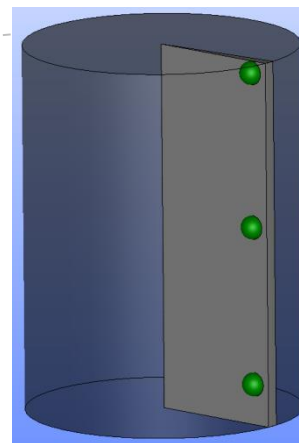
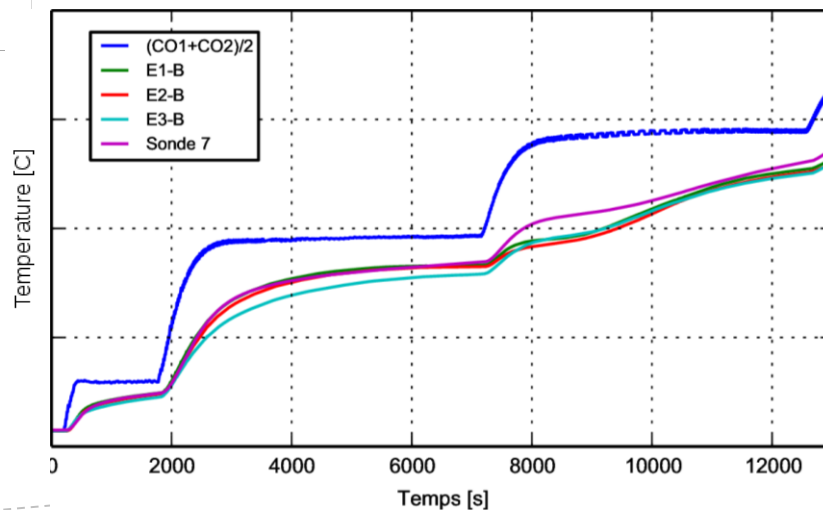
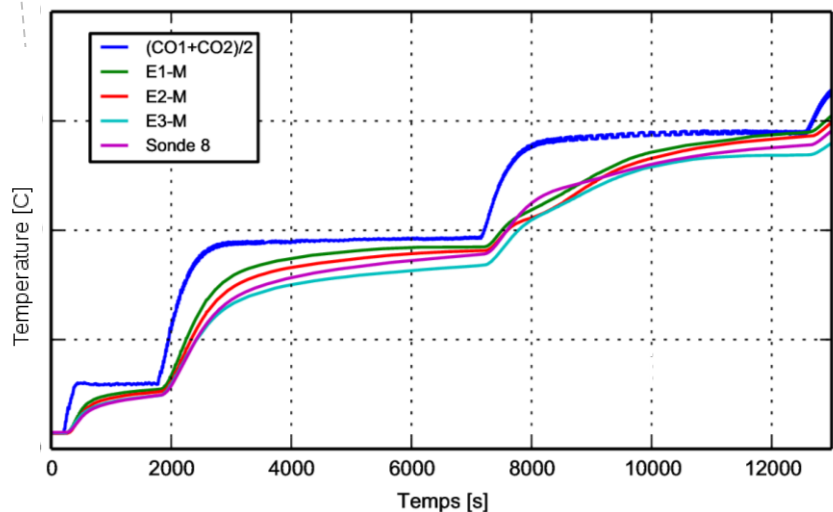
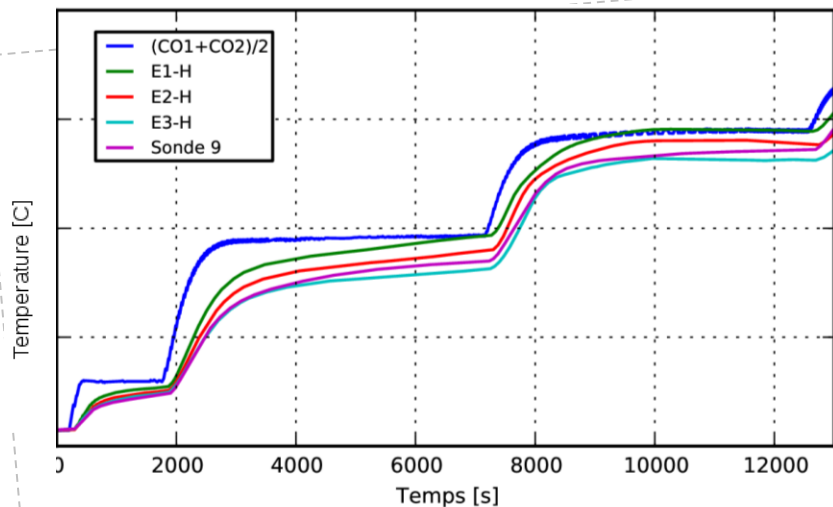
CFD results: *Code_Saturne* vs experimental data



temperature changes in intermediate ring



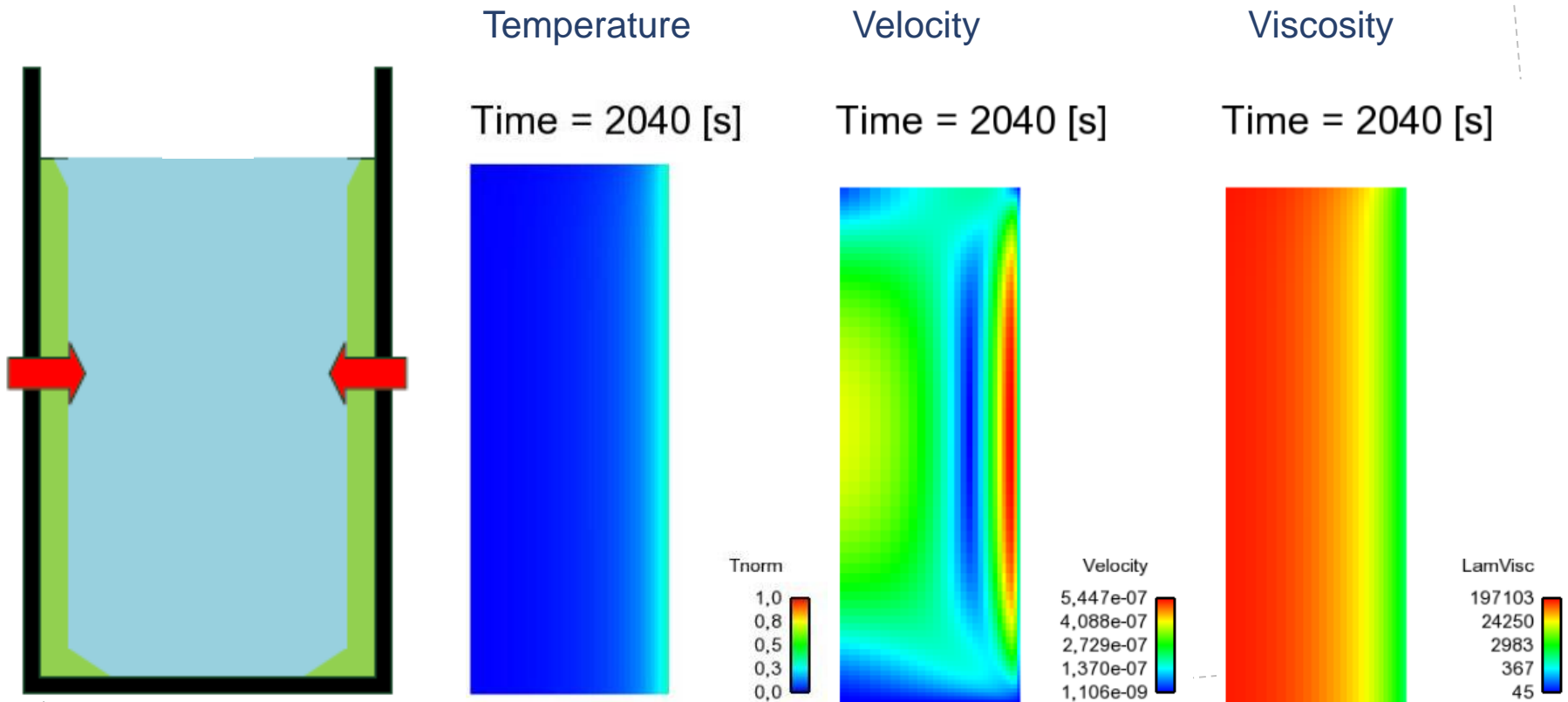
CFD results: *Code_Saturne* vs experimental data



Evolution of the external ring temperature

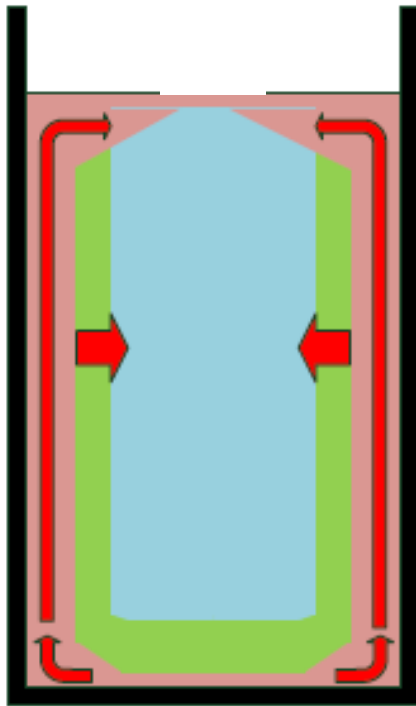
Analysis of the CFD results

At low temperatures below the glass transition, the heat transfer takes place **only by conduction**.



Analysis of the CFD results

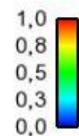
Volumes subjected to temperature higher than the temperature of the glass transition. The fluid flows upwardly and cover the surface.



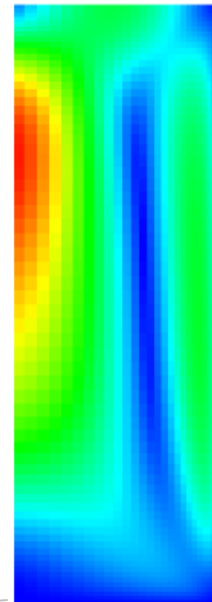
Temperature
Time = 9540 [s]



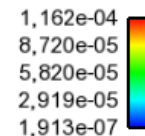
Tnorm



Velocity
Time = 9540 [s]



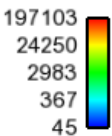
Velocity

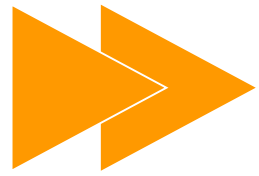


Viscosity
Time = 9540 [s]



LamVisc

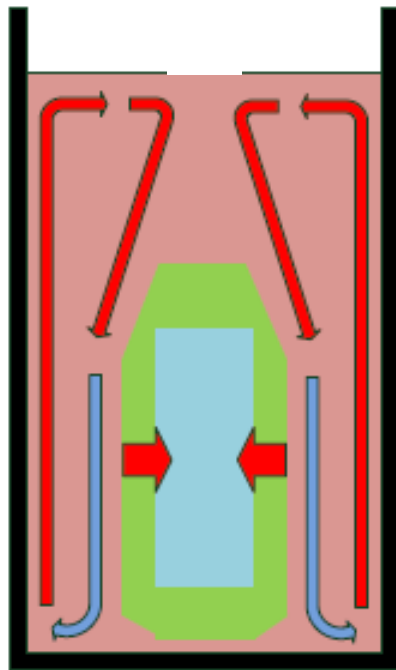




CFD results : Analysis of the results

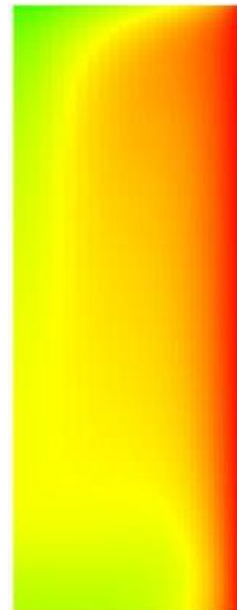
The volumes with low viscosity is sufficient to allow thermal cycle of convection, near vertical walls.

Exchanges in the heart of the matrix are always made by conduction.



Temperature

Time = 13000 [s]

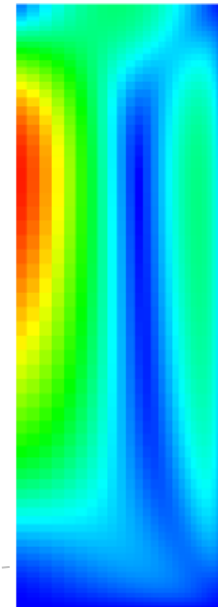


Tnorm

1,0
0,8
0,5
0,3
0,0

Velocity

Time = 13000 [s]



Velocity

2,004e-04
1,504e-04
1,003e-04
5,032e-05
2,991e-07

Viscosity

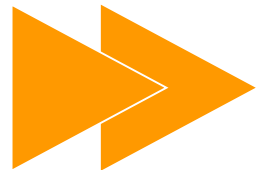
Time = 13000 [s]



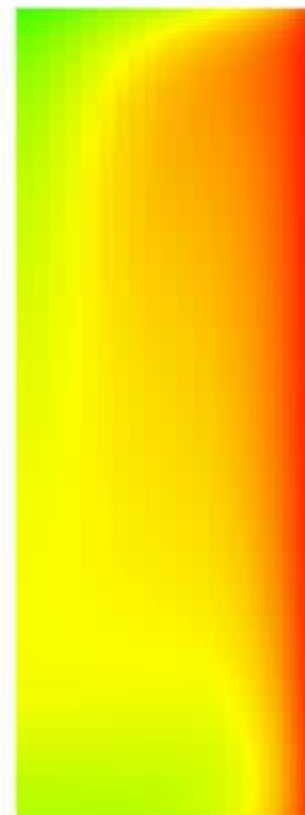
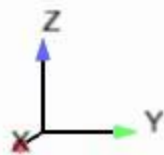
LamVisc

197103
24250
2983
367
45

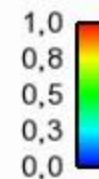
CFD results: video of the temperature field



Time = 13000 [s]

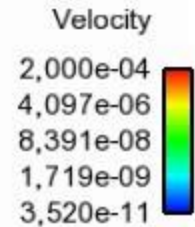
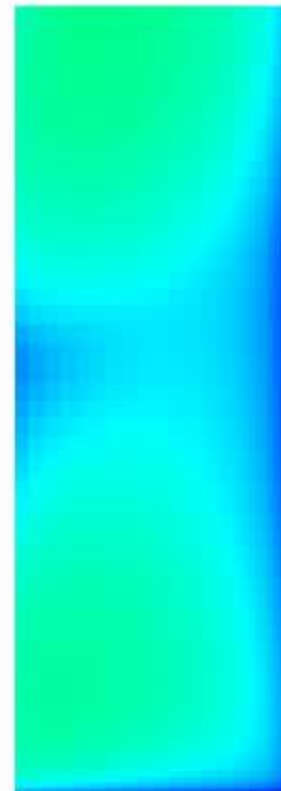
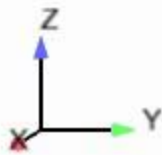


Tnorm



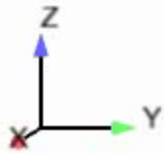
CFD results: video of the velocity field

Time = 60 [s]

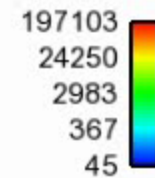


CFD results: video of the viscosity field

Time = 60 [s]



LamVisc





Consideration of a gradual release of chemical energy

Beyond a threshold temperature T_{onset} an exothermic chemical reaction provides heat to the bitumen volume. The thermal power P supplied by the chemical reaction is taken into account with a source of thermal power

Simplified kinetic equation $A \rightarrow B$

The rate of disappearance of species A $v = - \frac{d[A]}{dt}$ and $v = k[A]$

Transport equation of species A $\frac{\partial A}{\partial t} + \vec{u} \cdot \overrightarrow{\text{grad}}A = D_m \Delta A - kA$
 D_m mass diffusivity

k coefficient of the reaction rate (Arrhenius law) $k = A e^{\frac{-E_a}{RT}}$

A frequency factor

E_a activation energy Arrhenius

R gas constant

Consideration of a gradual release of chemical energy

For a higher temperature T_{onset} , three types of law for the thermal power P

Law 1 : thermal power polynomial P function of time after an experimental curve

$$P = f(t)$$

Law 2 : thermal power P according to a Arrhenius law with the energy of activation E_a

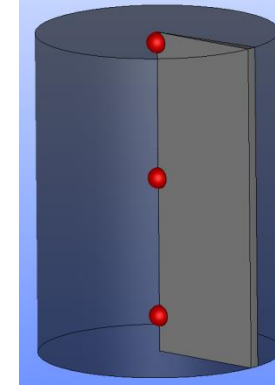
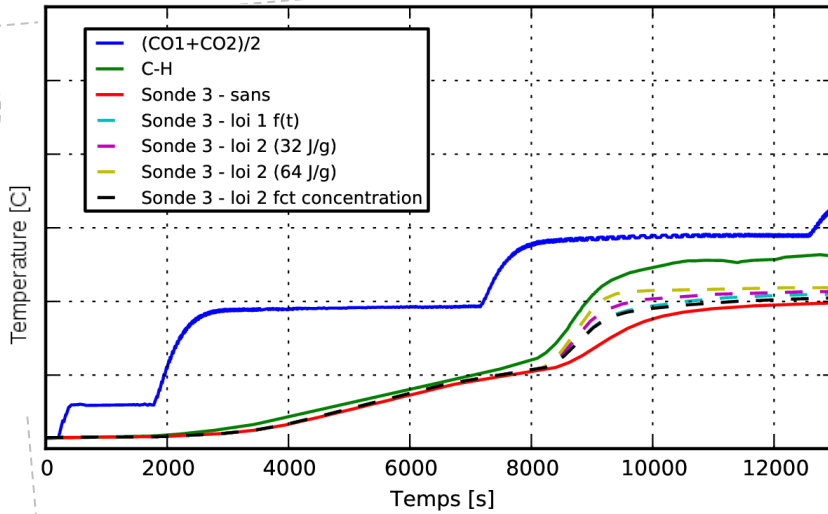
$$P = A e^{\frac{-E_a}{RT}} V \rho (-\Delta H_r)$$

V volume, ρ density, $\Delta H_r < 0$ for exothermic chemical reaction

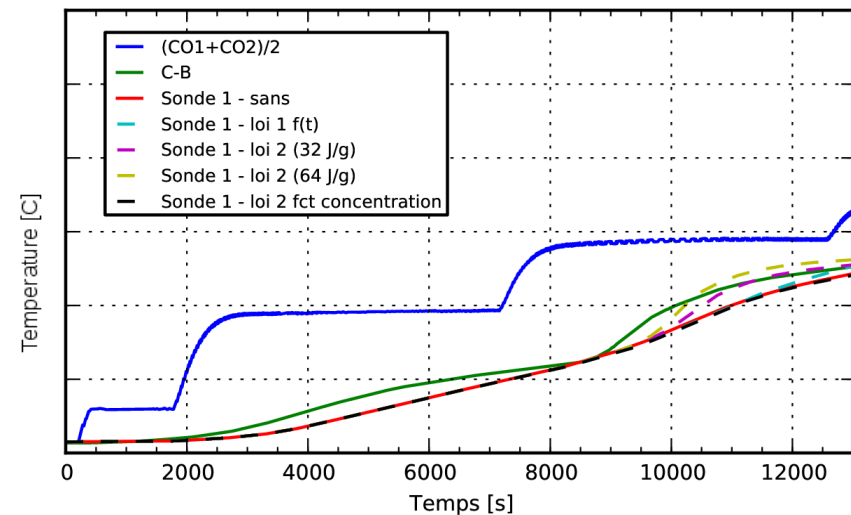
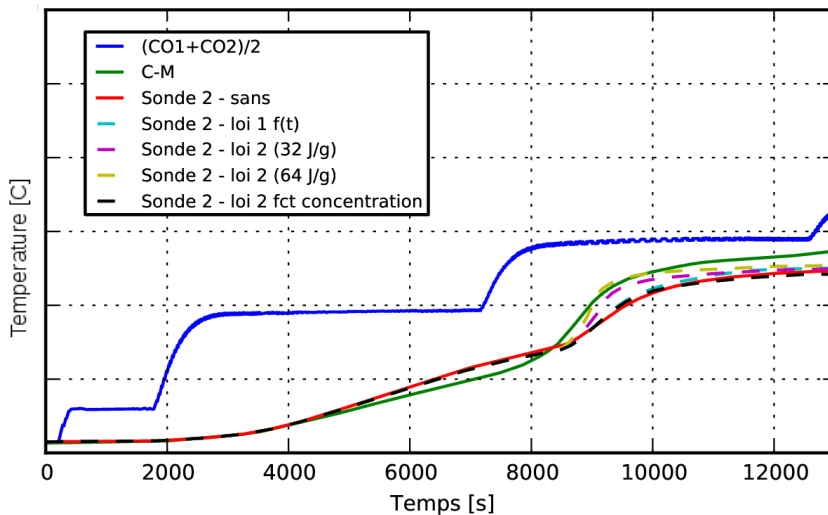
Law 3 : law 2 function concentration of species A

$$P = A \times e^{\frac{-E_a}{RT}} \times V \times \rho \times (-\Delta H_r) \times [A]$$

CFD results: *Code_Saturne* with thermal sources vs experimental data

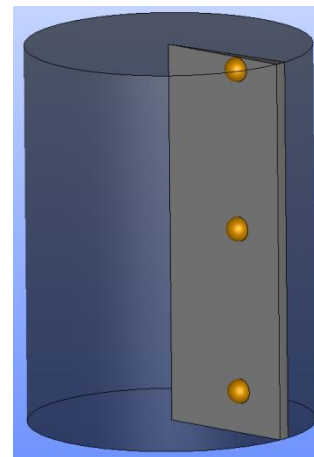
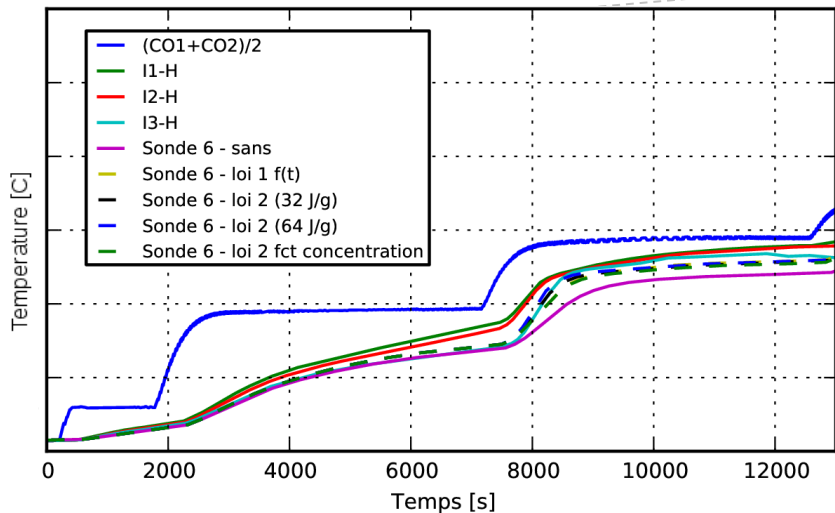


Changing the temperature at the center

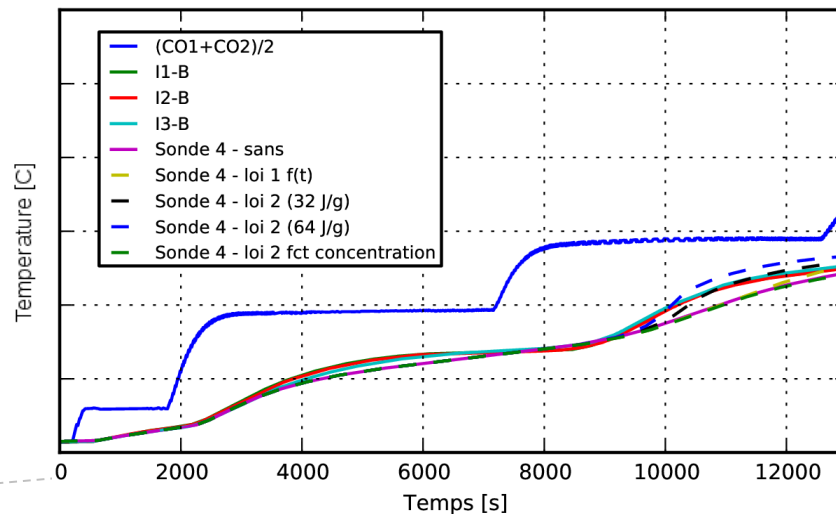
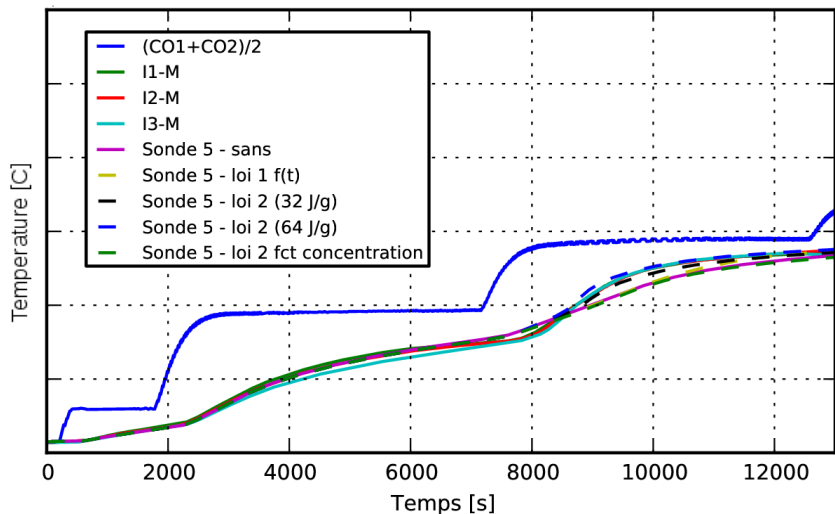




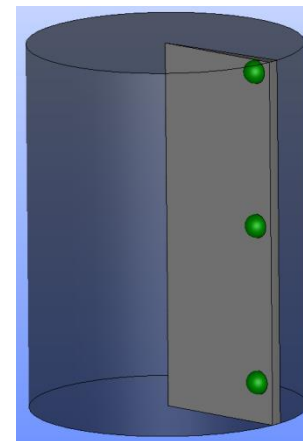
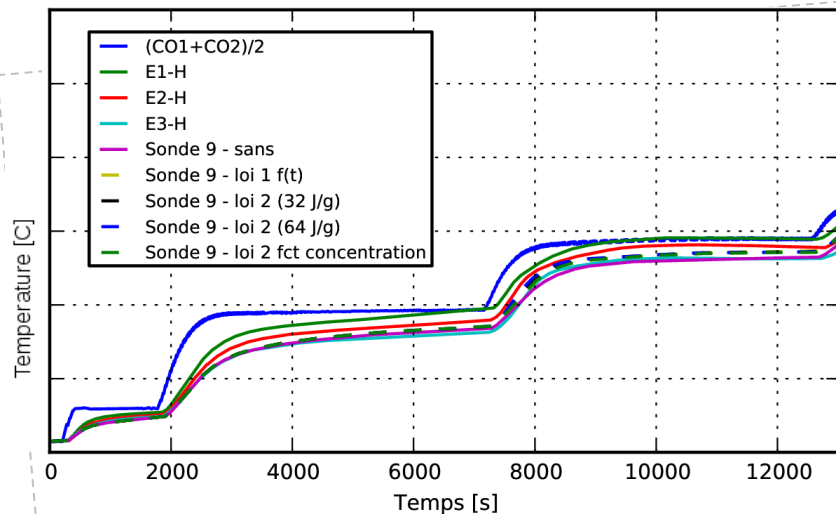
CFD results: *Code_Saturne* with thermal sources vs experimental data



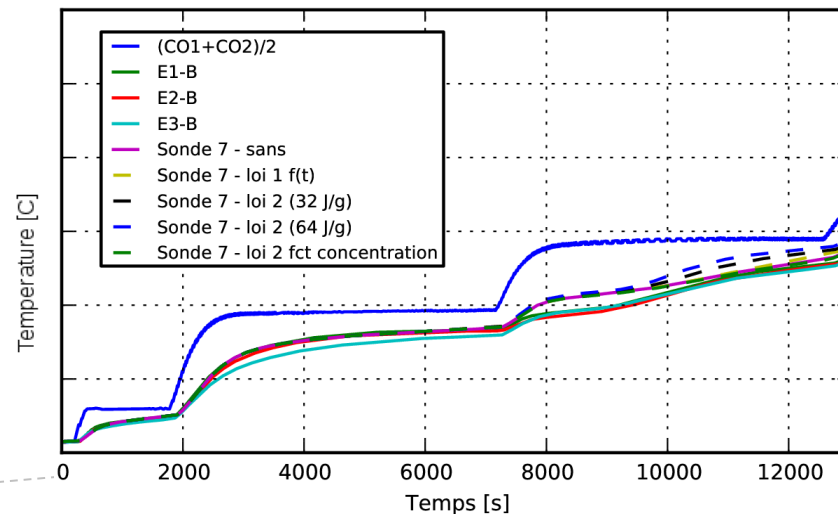
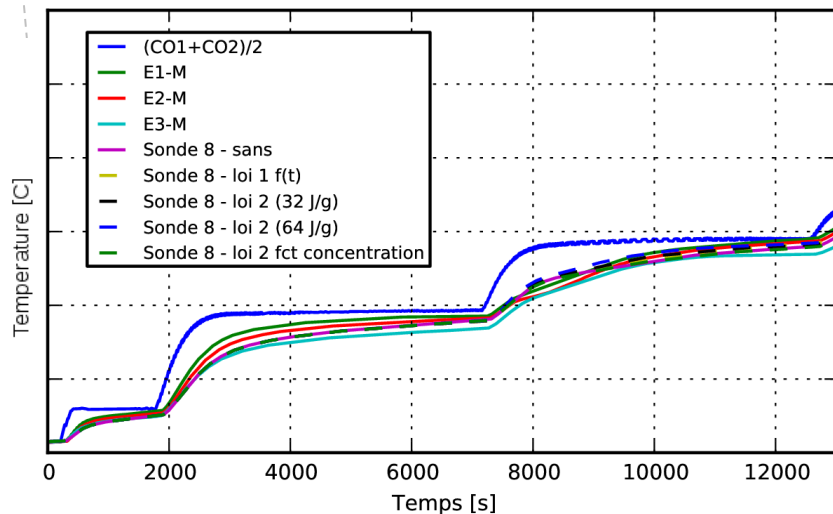
Temperature changes in intermediate ring



CFD results: *Code_Saturne* with thermal sources vs experimental data



Evolution of the external ring temperature



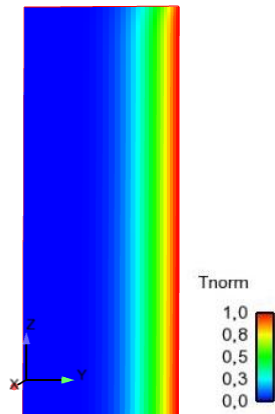
CFD results: *Code_Saturne* vs experimental data

Temperature

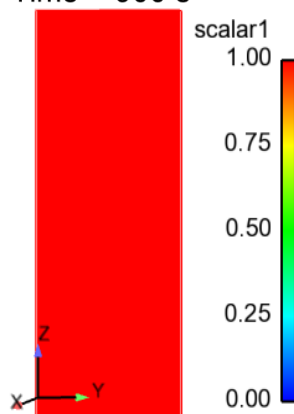
Concentration of the species [A]

Viscosity

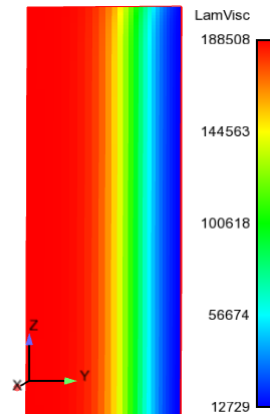
Time = 900 s



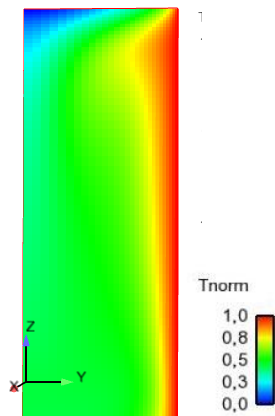
Time = 900 s



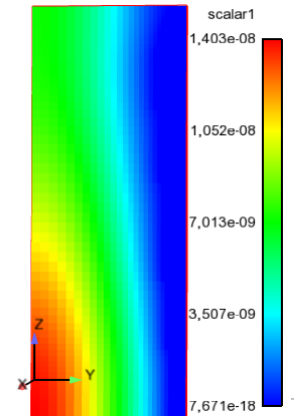
Time = 900 s



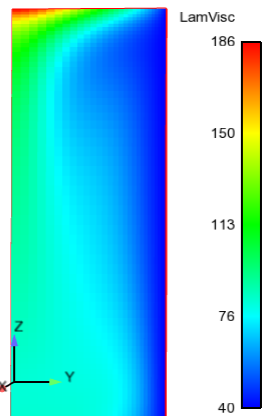
Time = 13500 s

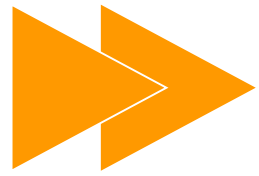


Time = 13500 s



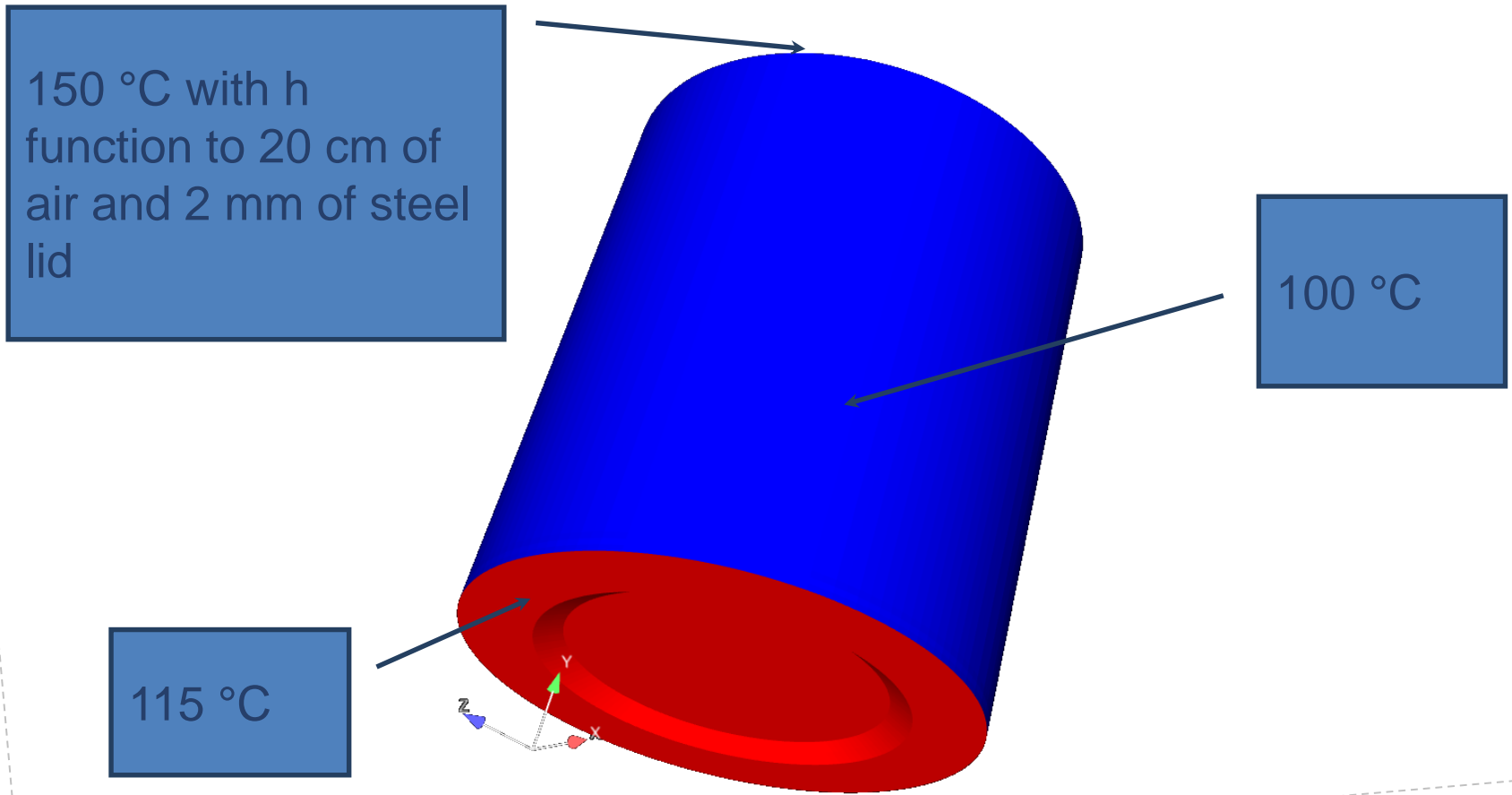
Time = 13500 s

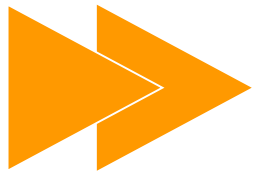




CFD results: barrel at scale 1

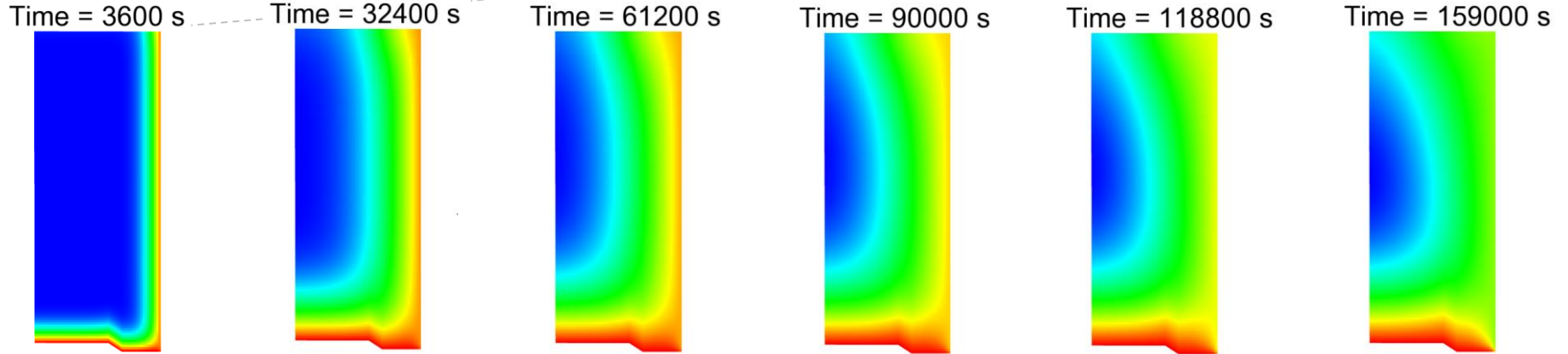
Constant boundary conditions over time



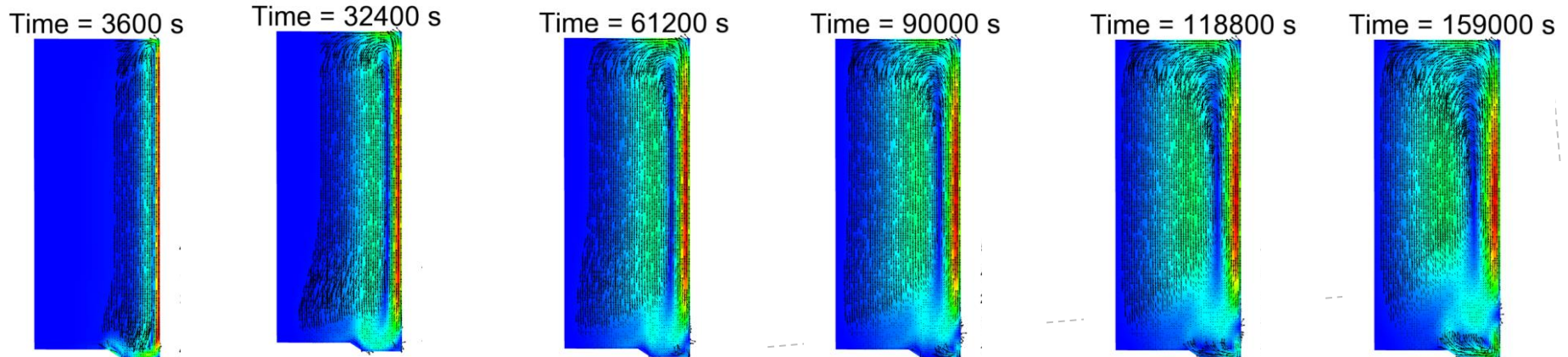


CFD results

Temperature



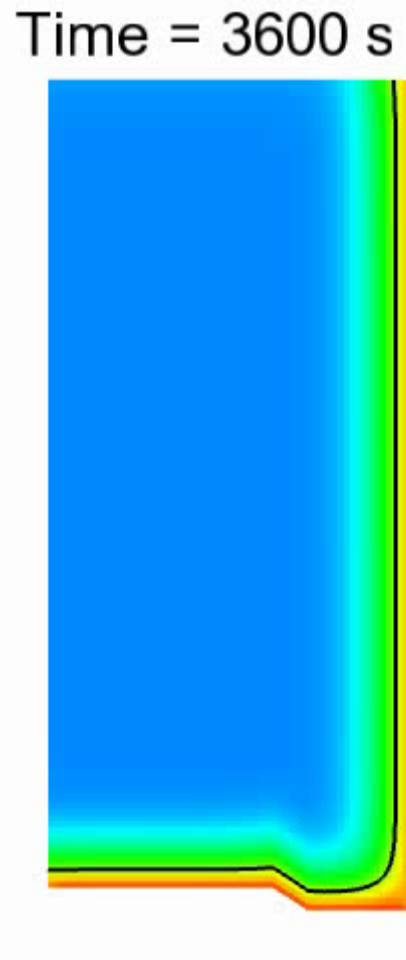
Velocity



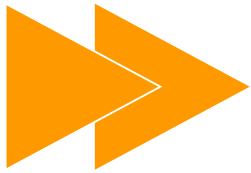


CFD results : video

Constant boundary conditions over time



Temperature

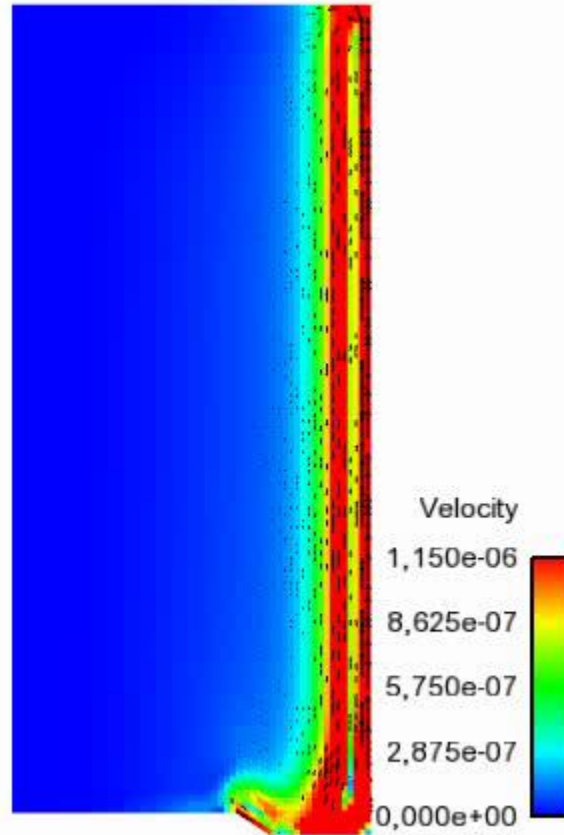


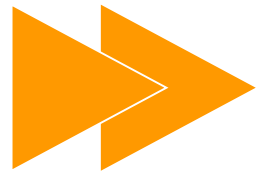
CFD results : video

Constant boundary conditions over time

Time = 3600 s

Velocity

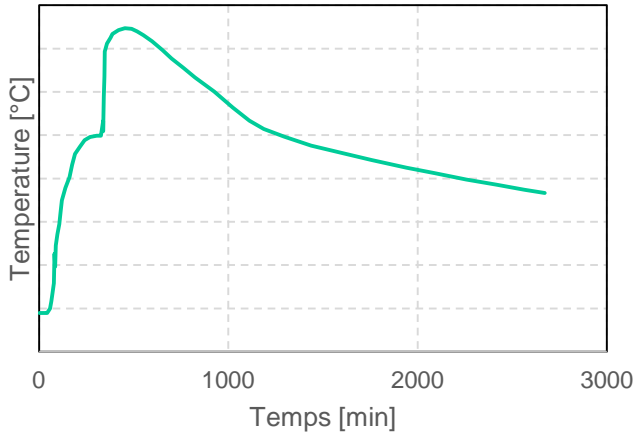




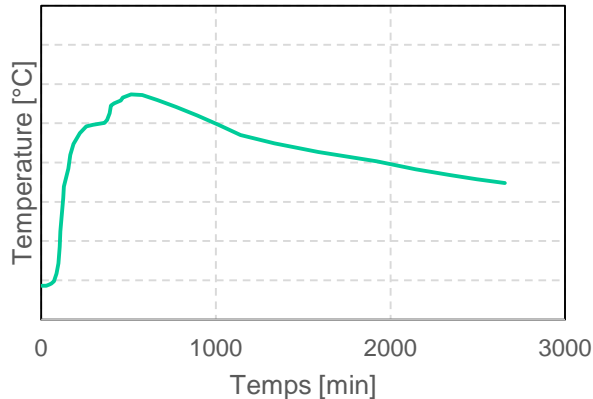
CFD results: barrel scale 1

Variable boundary conditions over time

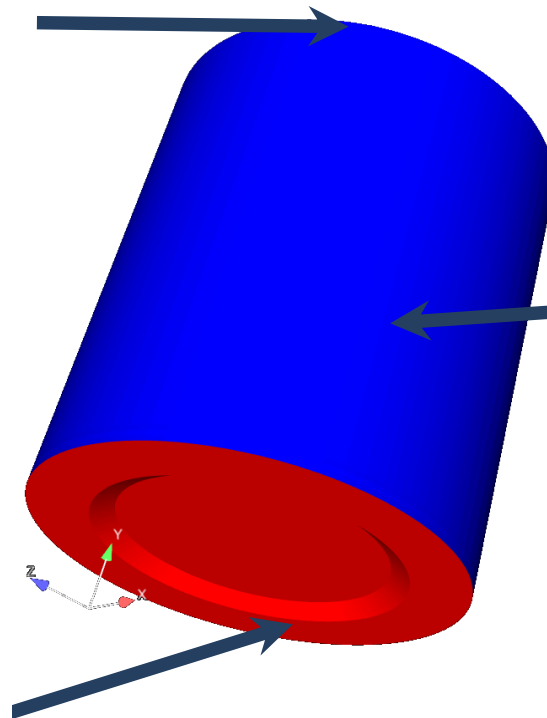
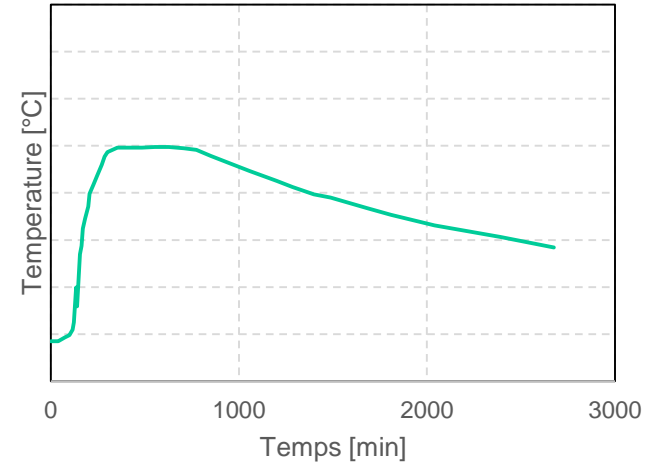
top

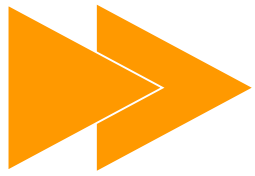


bottom



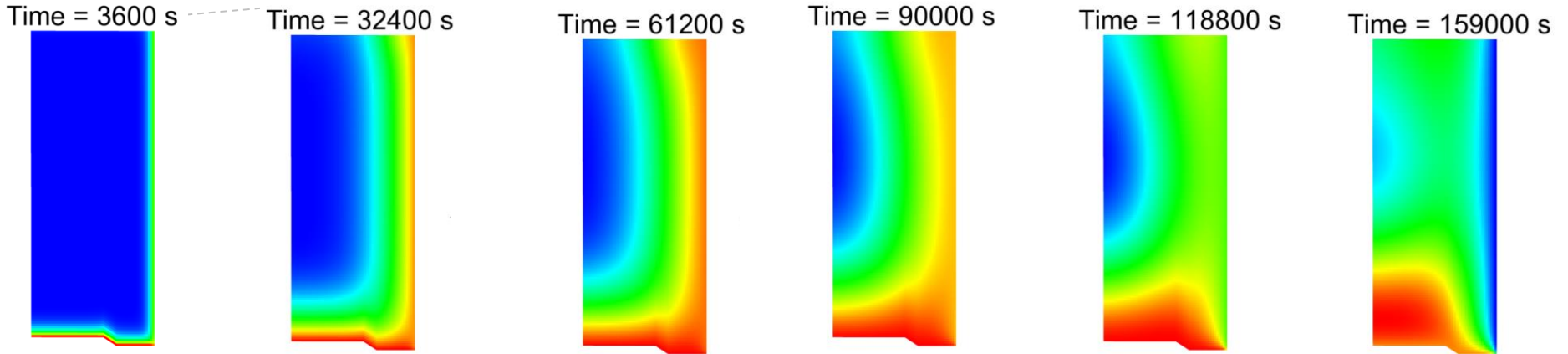
wall



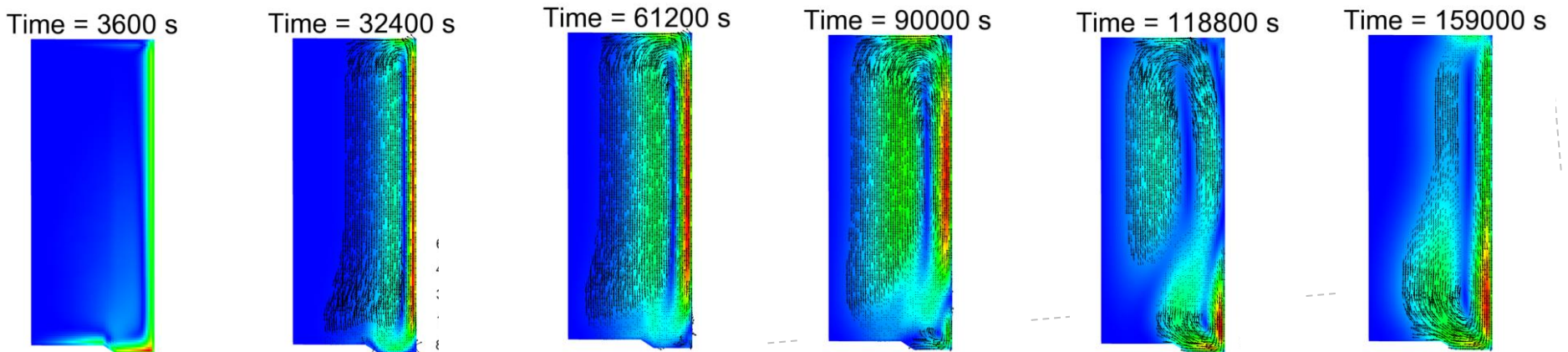


CFD results

Temperature



Velocity



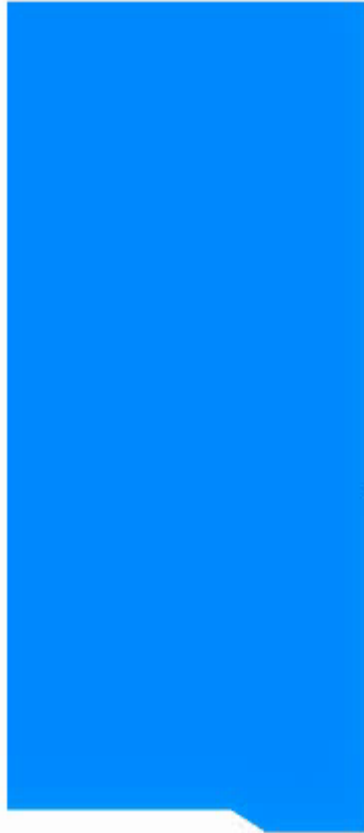


CFD results: video

Variable boundary conditions over time

Time = 3600 s

Temperature



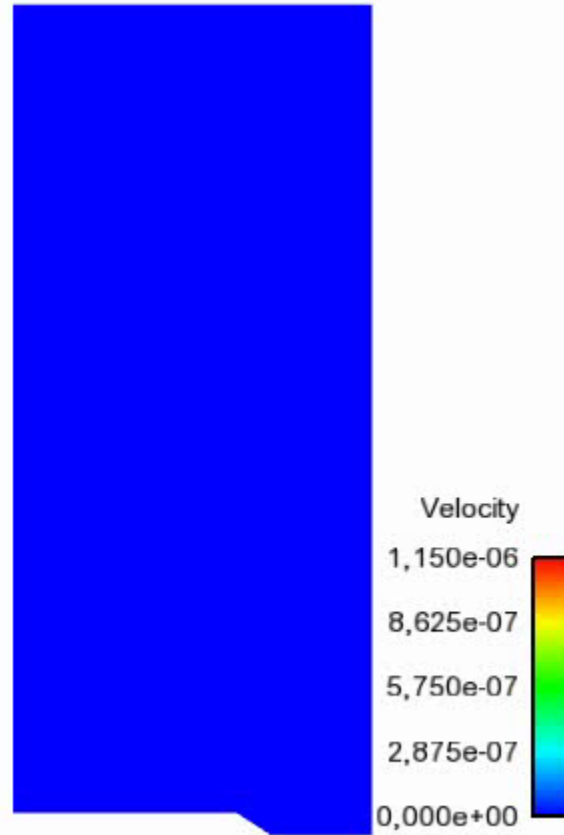


CFD results: video

Variable boundary conditions over time

Time = 3600 s

Velocity





CONCLUSION

1) Summary of the case made validations

- Experimental data on several types of bitumen in a 2kg pot
- test case with the physical properties of the bitumen 70/100
- test cases with a first approach to physical properties of bitumen with radioactive sludge

2) Summary of the models produced

- model with a 2kg pot with 70/100 bitumen
- model with a 2kg pot with properties bitumen used for storage
- model with a 2kg pot including an exothermic reaction for bitumen (3 type of law)
- model with a barrel at scale 1



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3) The first fluid calculations were presented to CNE in January



END

**THANK YOU FOUR
ATTENTION**



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