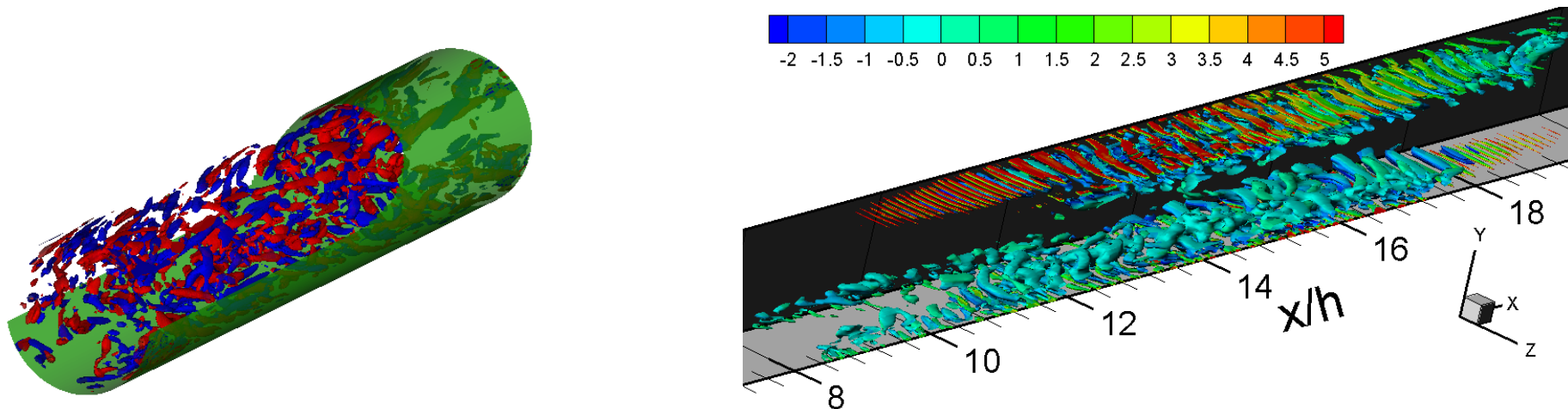


Computational Investigation of Buoyancy Influenced Flows and Benchmarking exercise



Presenter: Yacine Addad (PDRA)

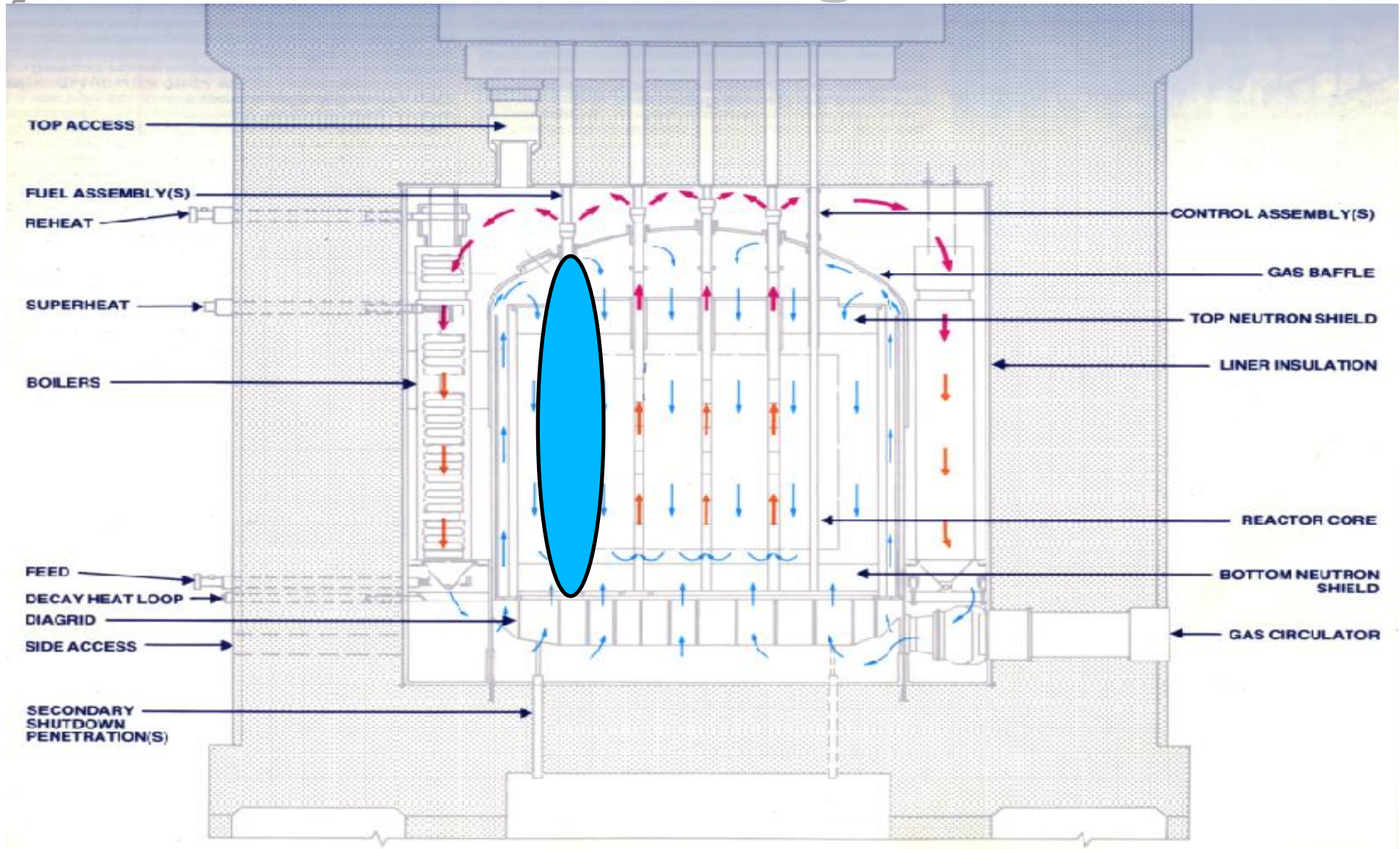
(KNOO Team: D. Laurence, M. Cotton, A. Keshmiri, S. Rolfo)

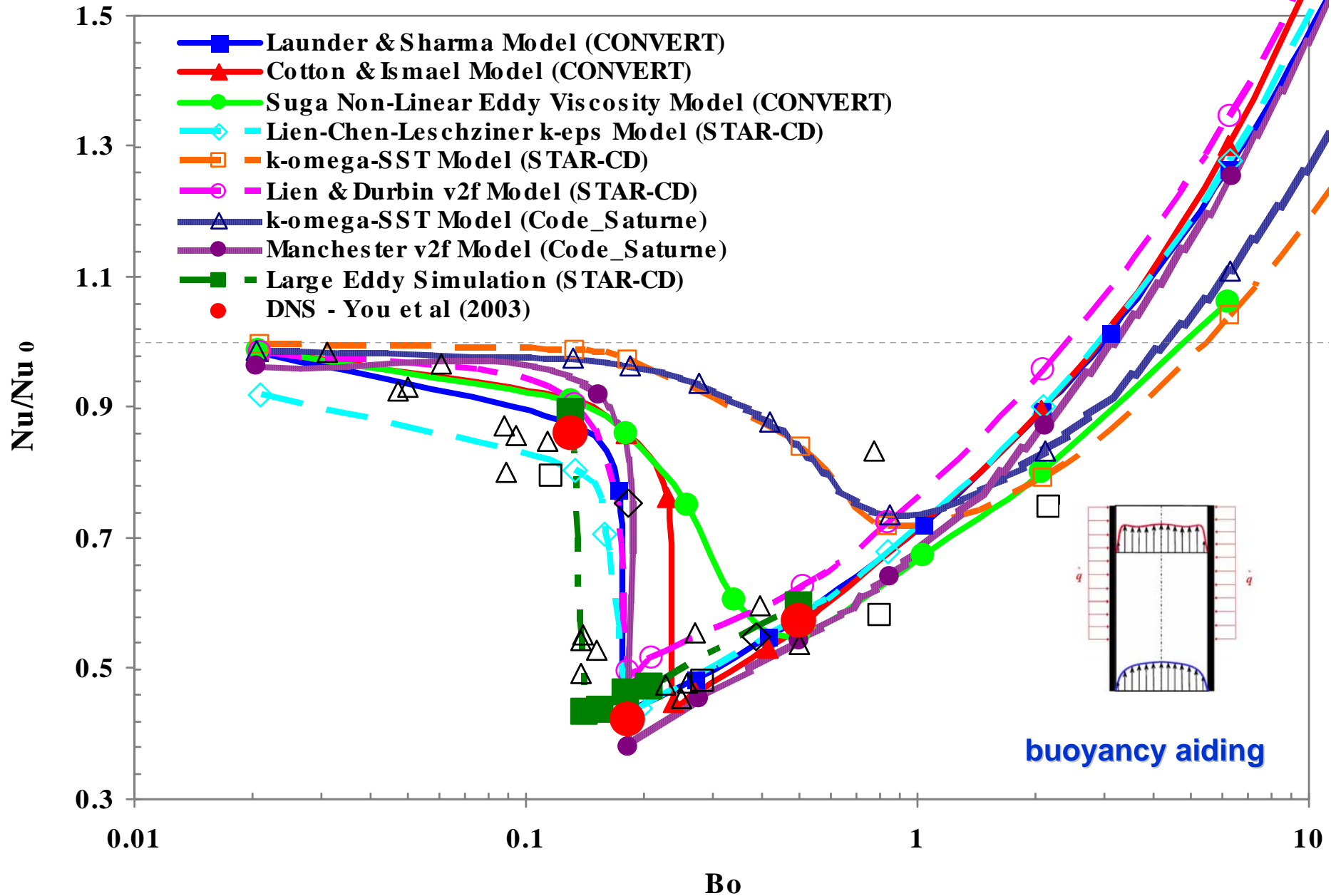
(Collaborators: S. Benhamadouche, R. Howard, F. di Mare)

School of Mechanical, Aerospace & Civil Engineering (MACE)

The University of Manchester

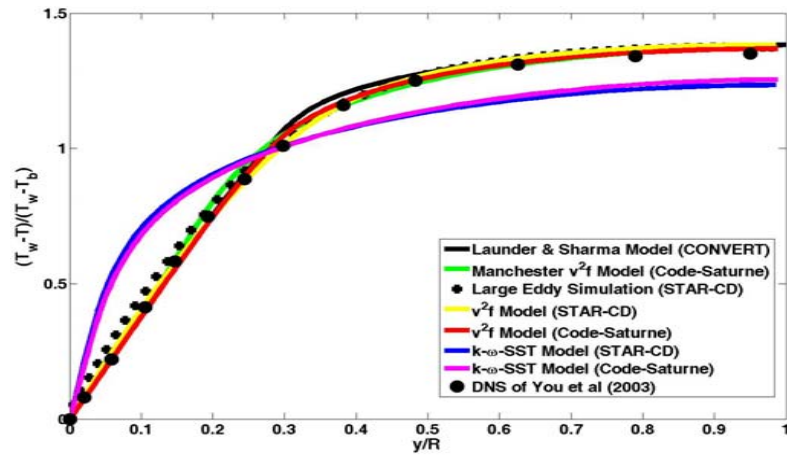
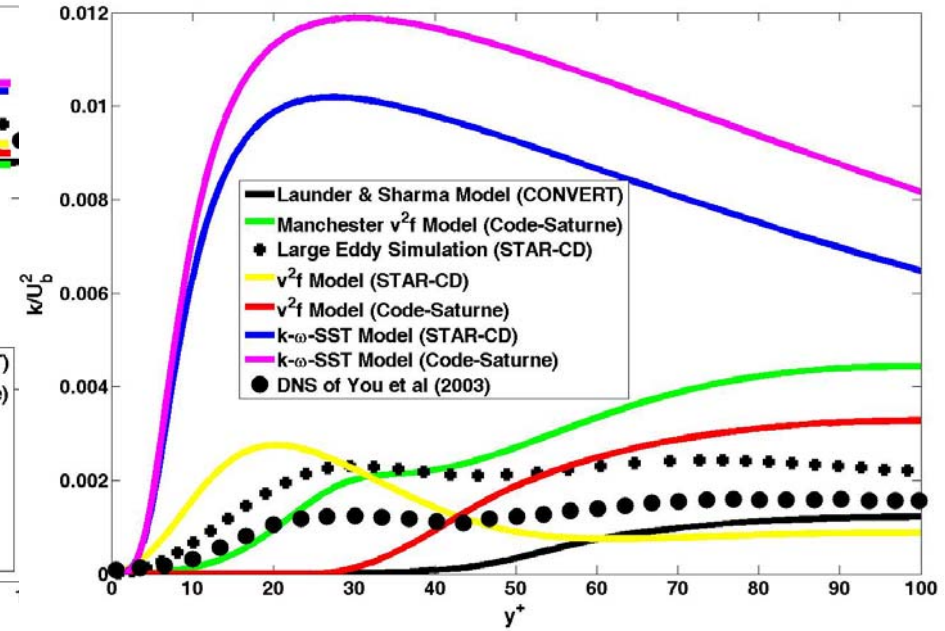
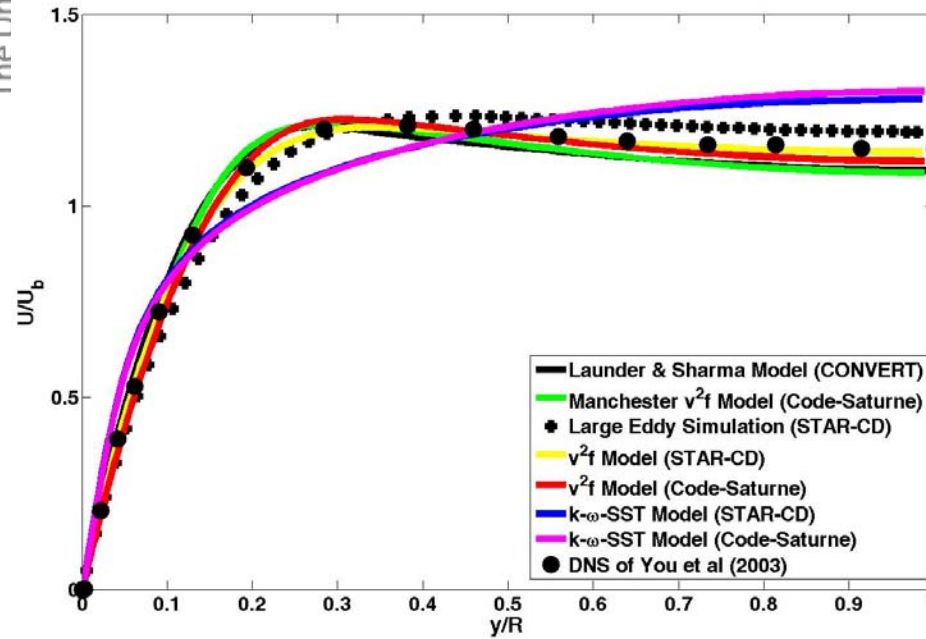
AGR working scheme





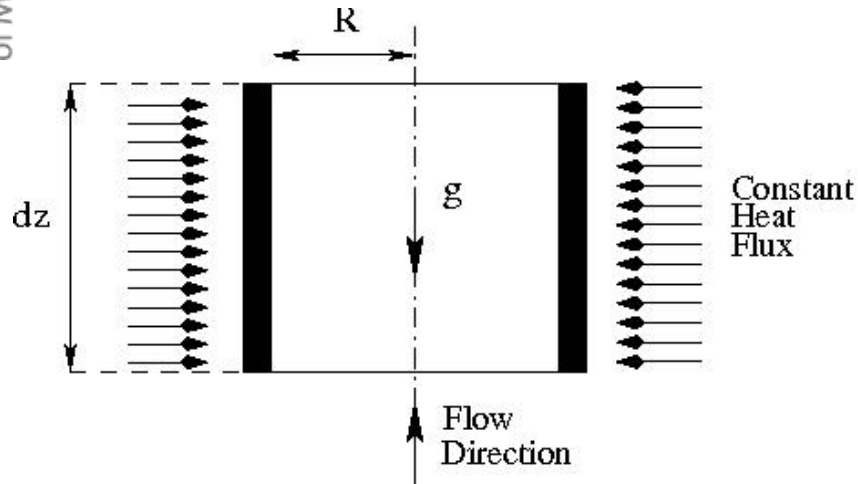
$Gr/Re^{**2} = 0.087$ (relaminarization)

The University of Manchester

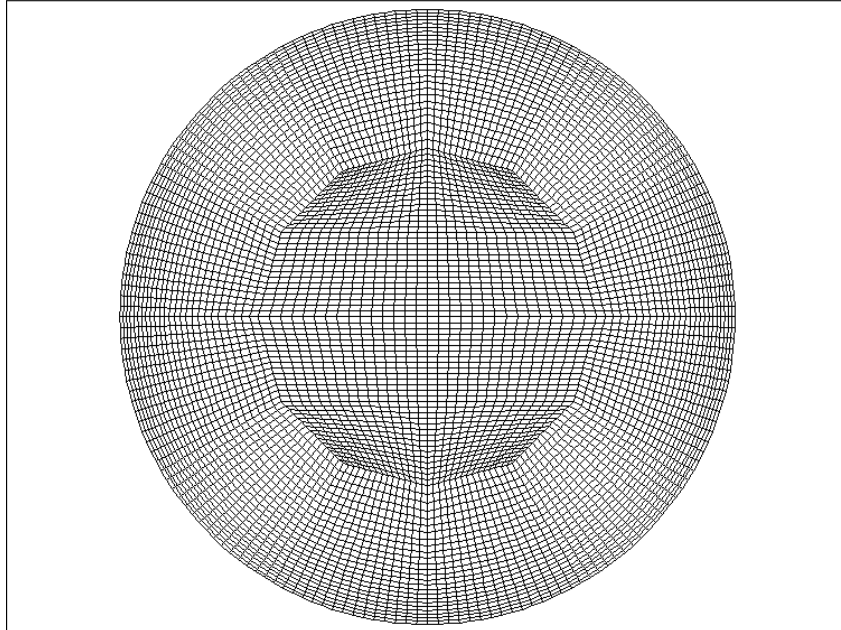


- Launder & Sharma Model (CONVERT)
- Manchester v^2f Model (Code-Saturne)
- Large Eddy Simulation (STAR-CD)
- v^2f Model (STAR-CD)
- v^2f Model (Code-Saturne)
- $k-\omega$ -SST Model (STAR-CD)
- $k-\omega$ -SST Model (Code-Saturne)
- DNS of You et al (2003)

Test Case Description

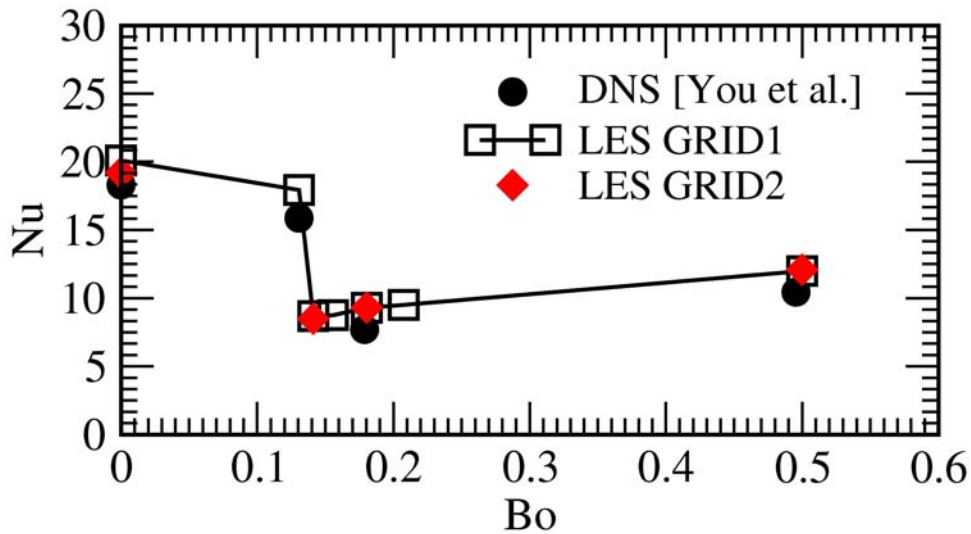
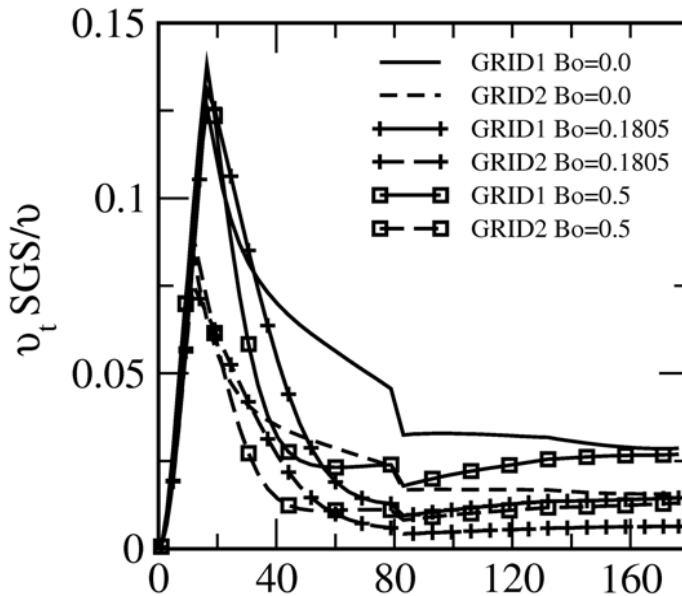


- **Re=180** based on R and u_τ .
- **Boussinesq** Approximation.
- Periodic Flow.
- $Lz=30R$

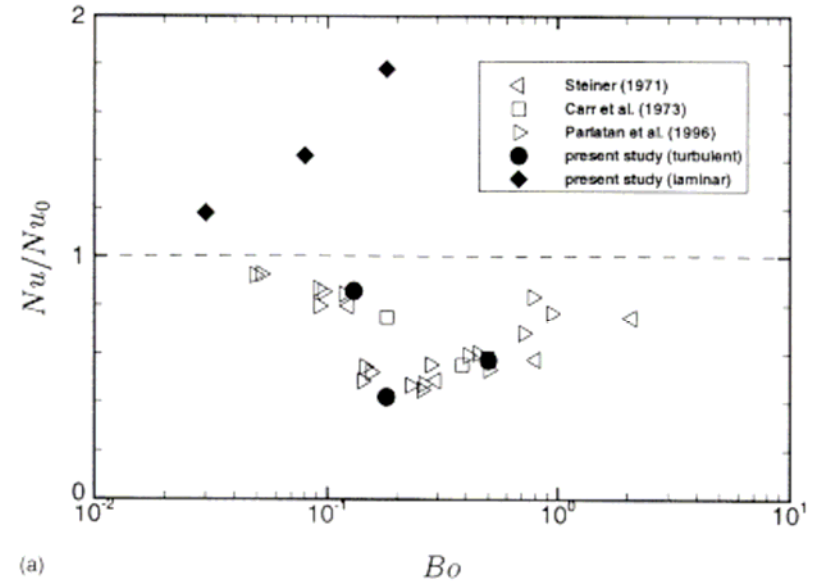


- **Grid1:** 1.61 million
- **Grid2:** 4.83 million
- Grid1 Resolution: $\Delta r^+_{\min}=1.0$, $\Delta\phi^+=6.28$, $\Delta z^+=18$.
- Grid2 Resolution: $\Delta r^+_{\min}=1.0$, $\Delta\phi^+=6.28$, $\Delta z^+=7.03$.

Ratio of SGS
to molecular
viscosity



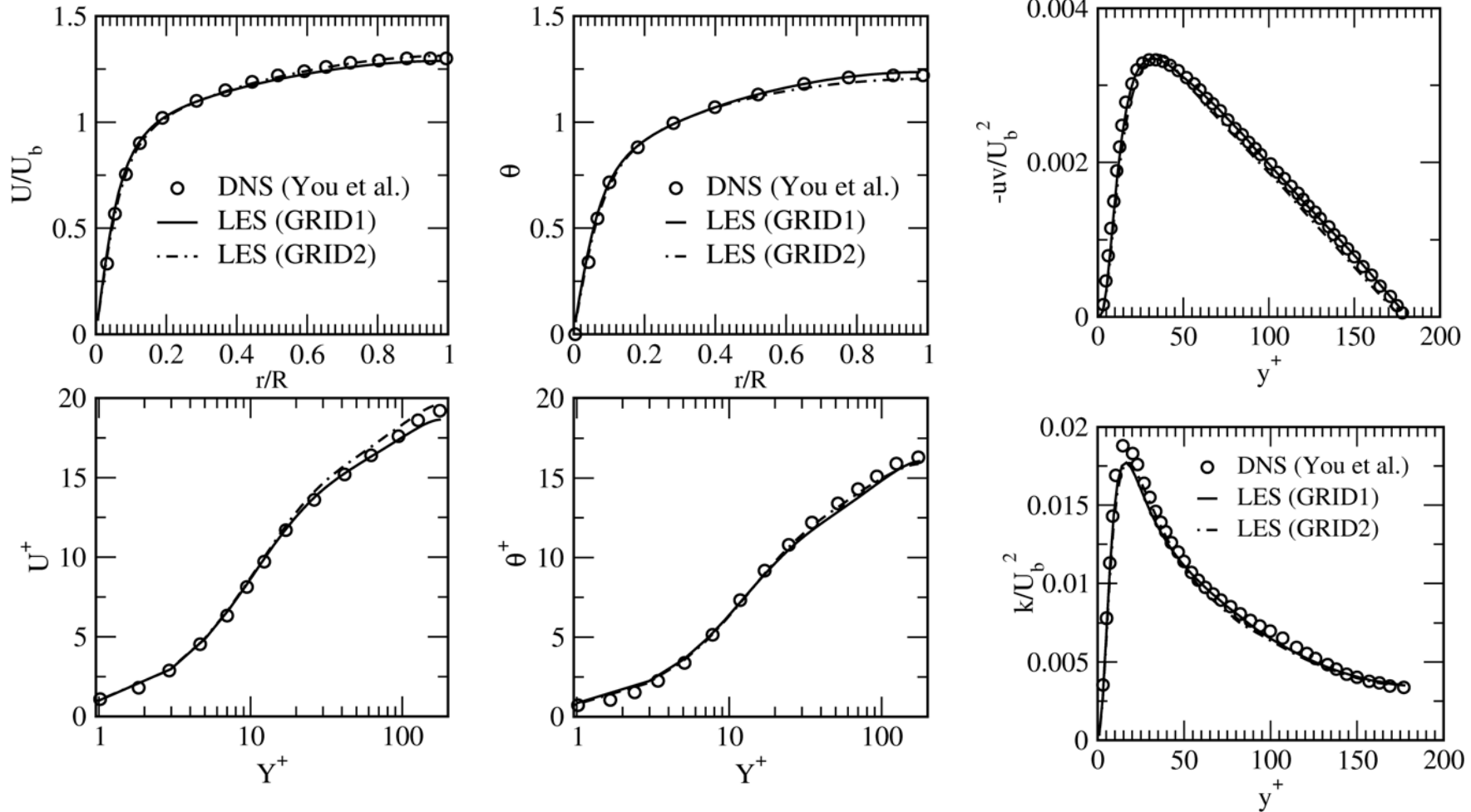
Nusselt number as a function of the buoyancy parameter



from You et al.

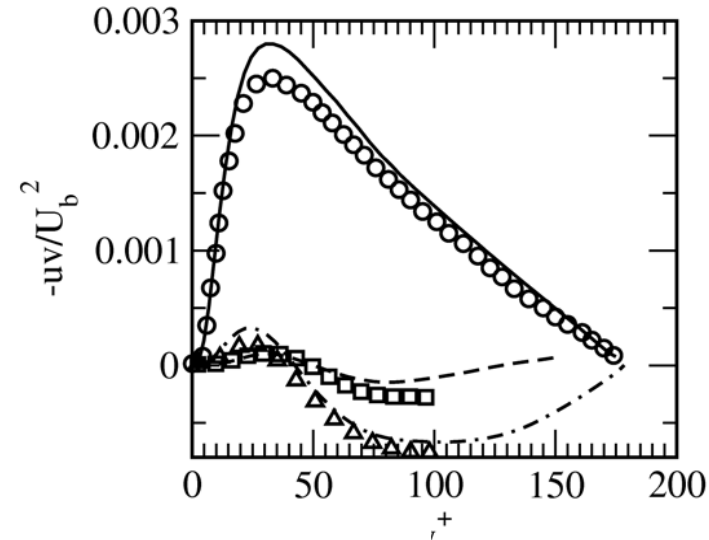
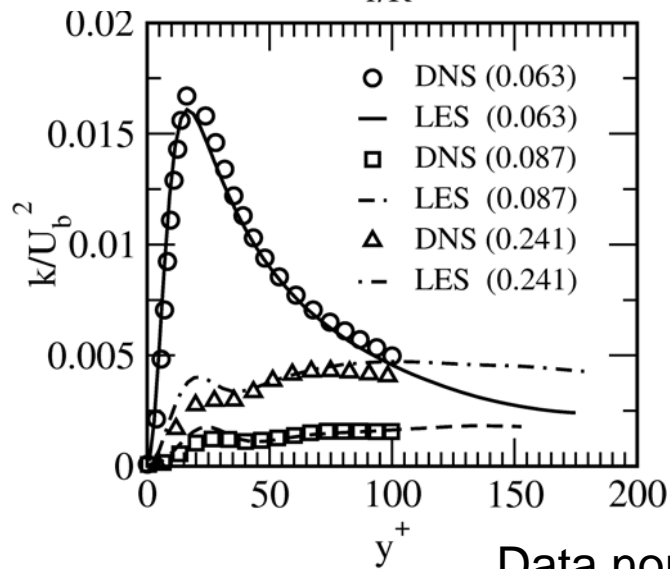
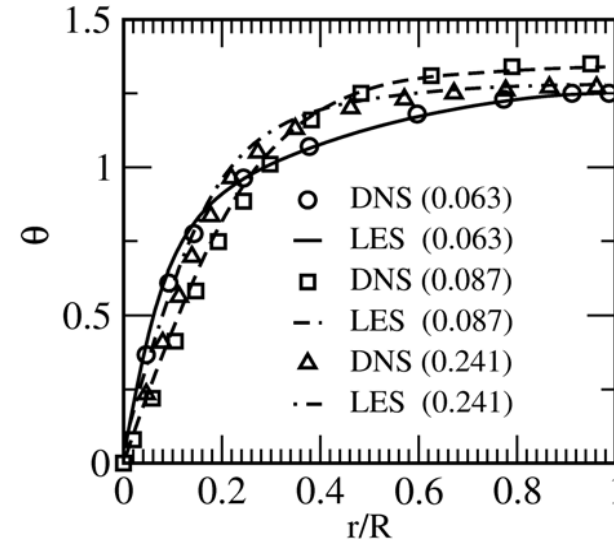
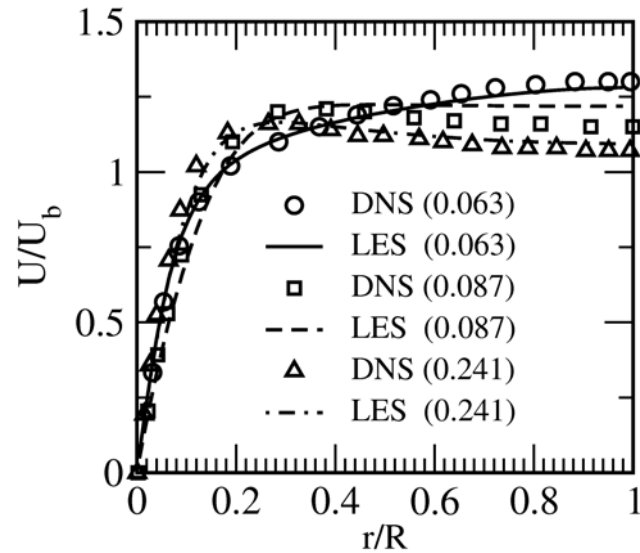
For RANS models predictions, see the paper by Amir Keshmiri et al.

Case1: Forced convection $Gr/Re^2=0.0$



Data normalized by the bulk velocity

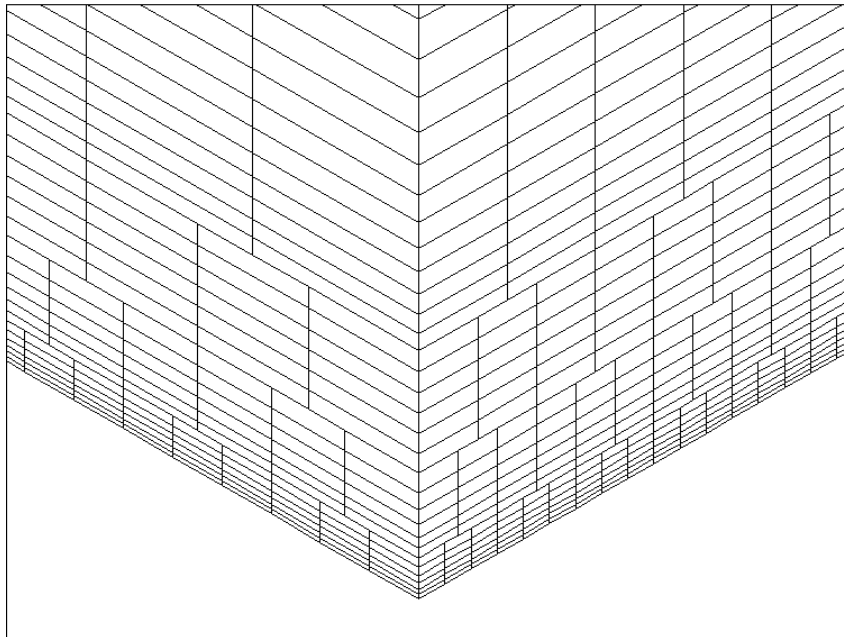
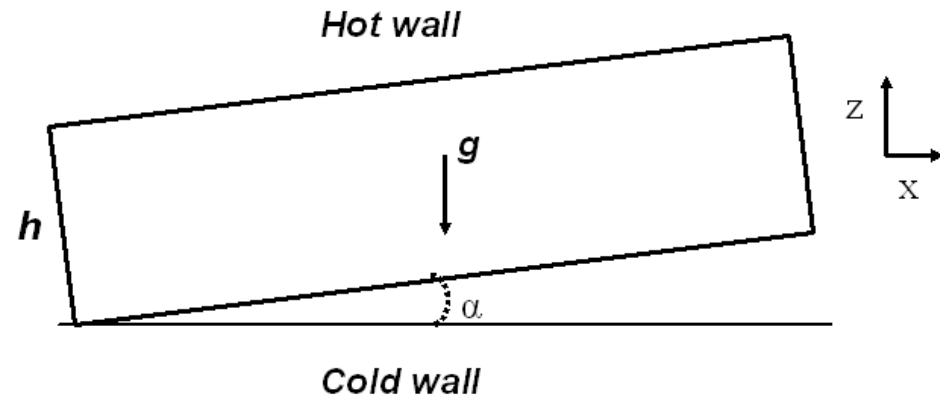
Cases from $Gr/Re^2=0.063$ to $Gr/Re^2=0.241$



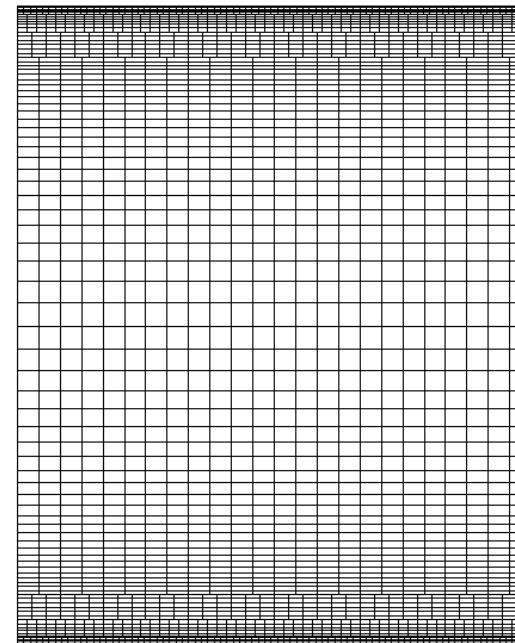
Data normalized by the bulk velocity

LES Grid (Case1)

- $Ra = 4.16 \times 10^8$
- NCELL = 3 million
- Boussinesq approximation
- $Pr = 0.71$ (Air)
- $\alpha = 5^\circ$



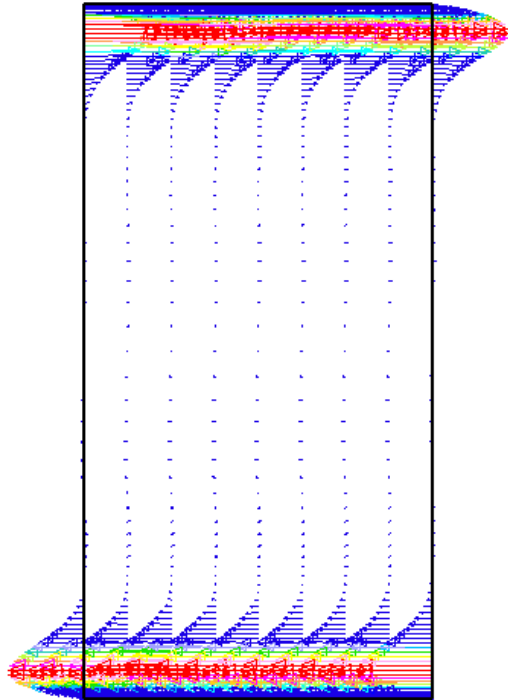
Plan Y-Z



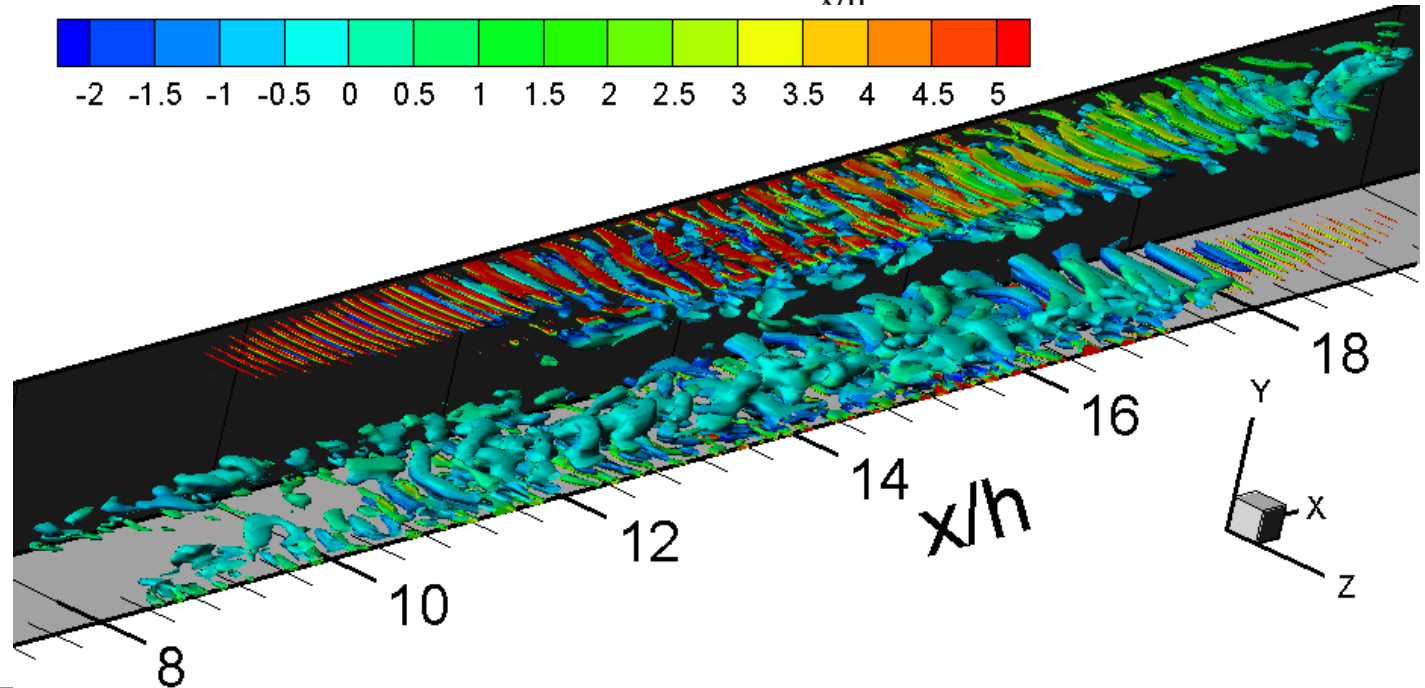
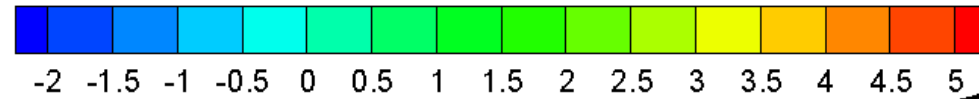
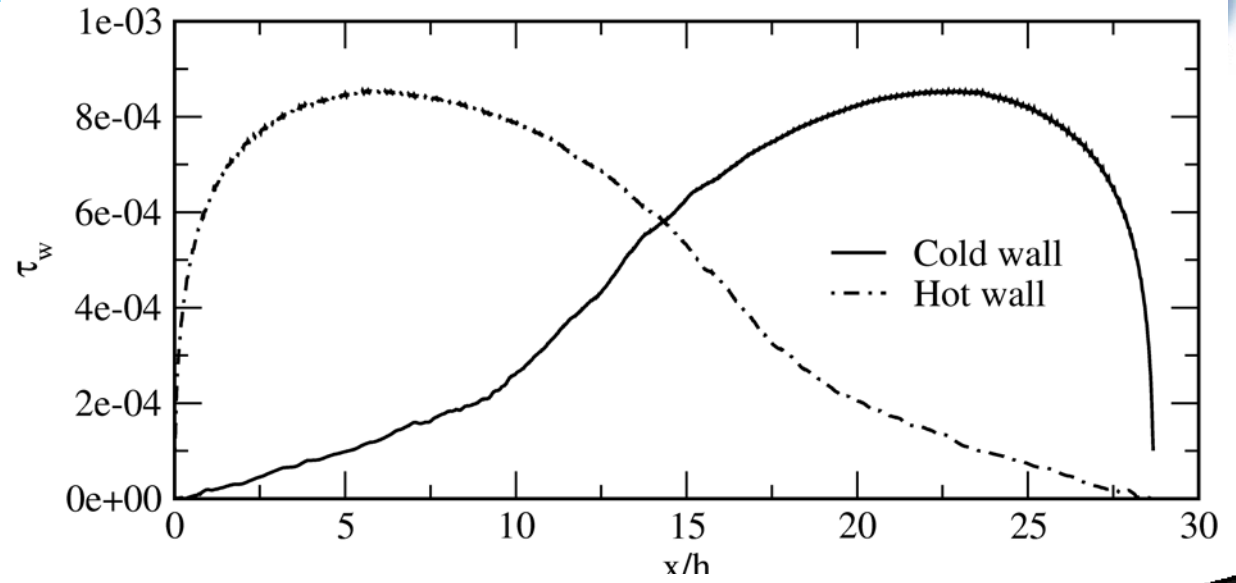
← 0.8h →

niversity
nchester

LES RESULTS



Q=0.05



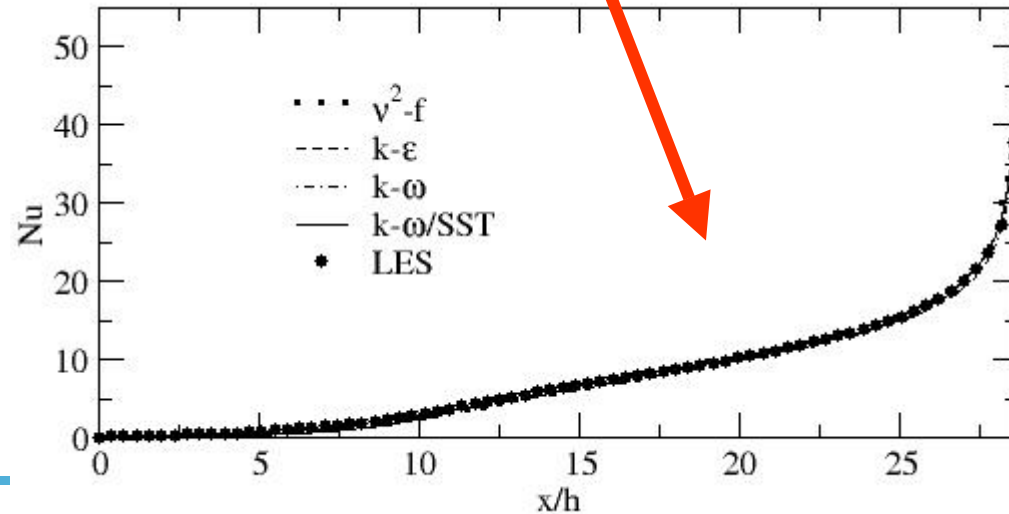
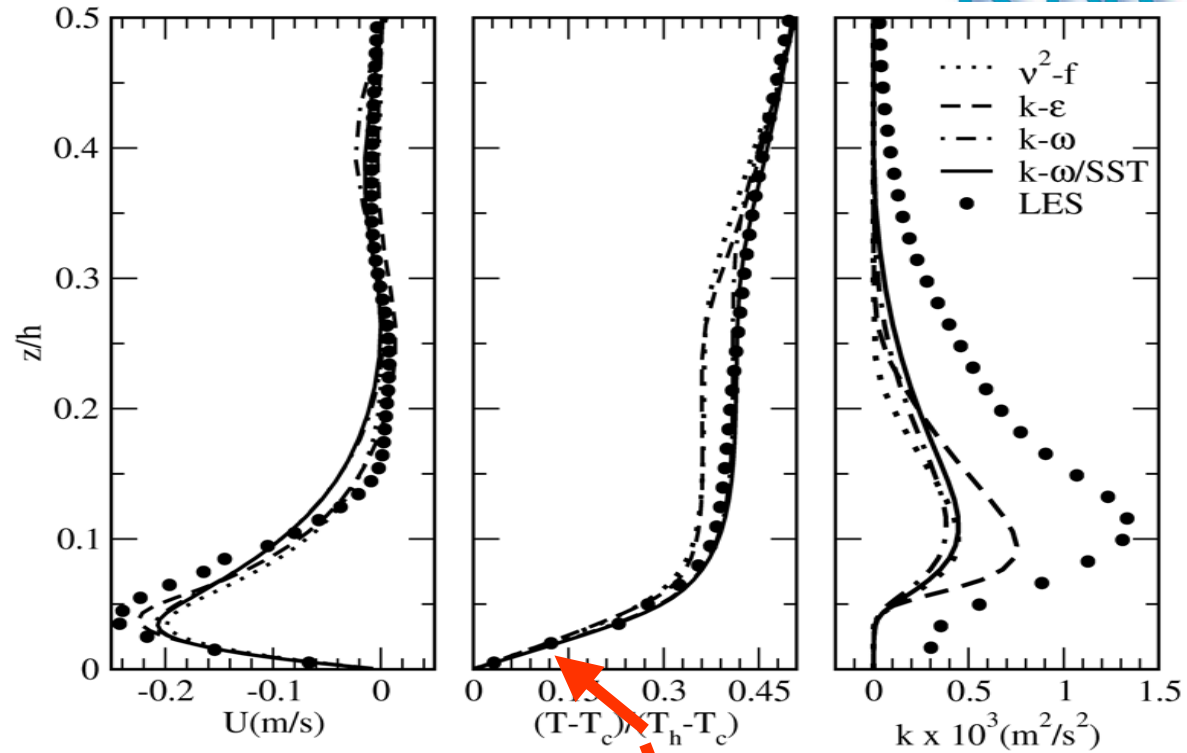
RANS RESULTS

Low-Re. models tested:

- k-ε Lien *et al.* (1996)
- k-ω Wilcox (1998)
- k-ω SST Menter (1993)
- v²-f Lien & Durbin (1996)

- Buoyancy term included in k-equation
- thermal fluxes

$$\overline{\rho u_j' h'} = -\frac{\mu_t}{\sigma_{h,t}} \frac{\partial h}{\partial x_j}$$



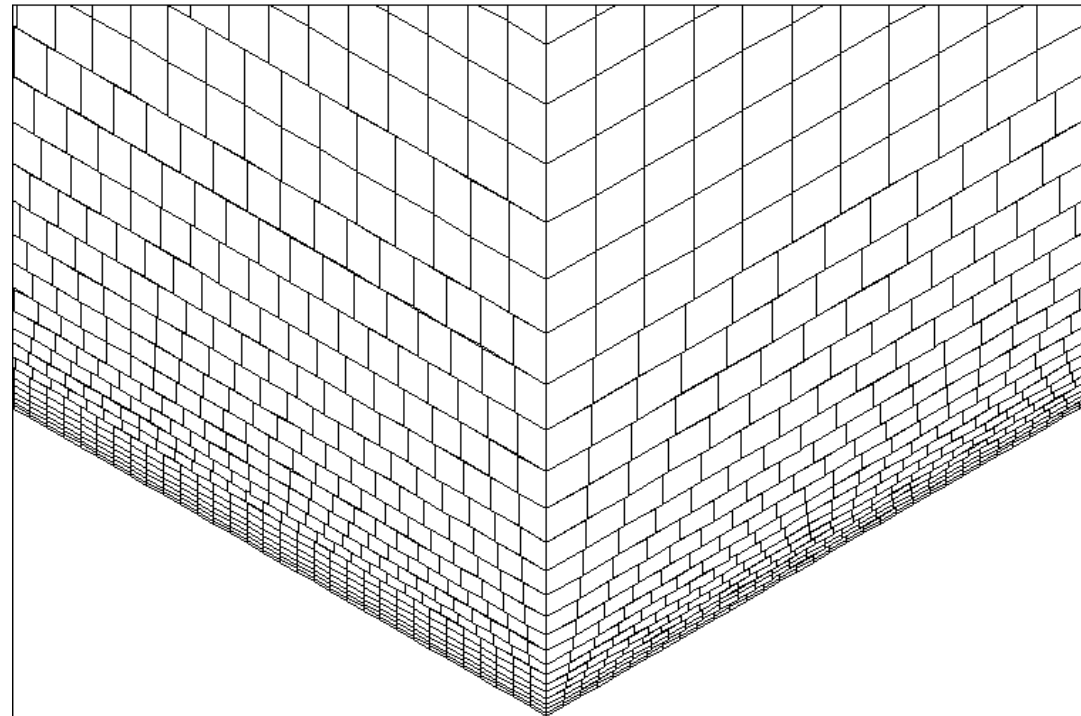
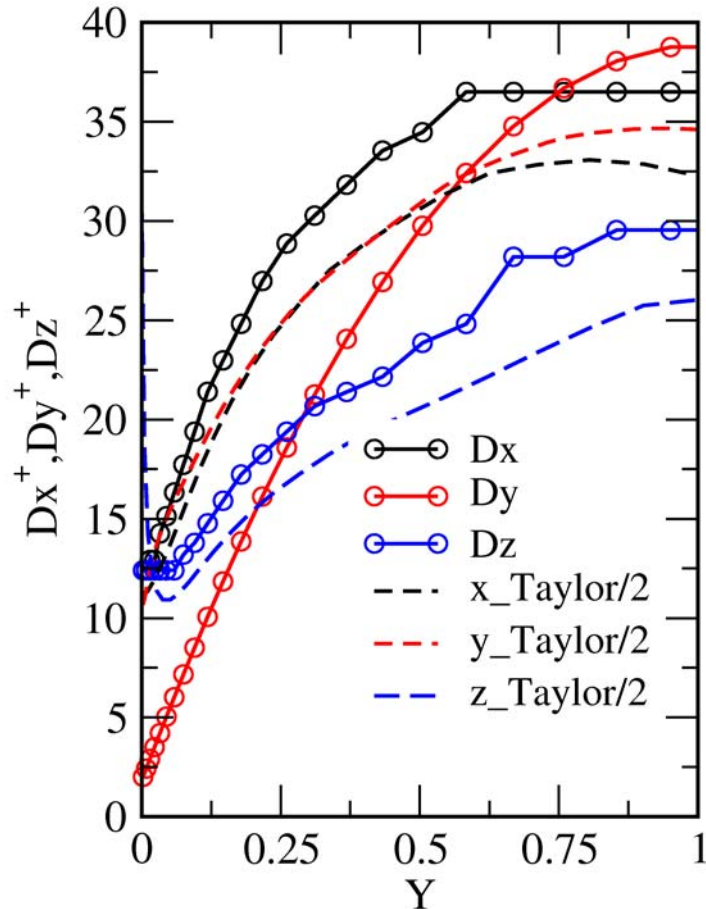
Code_Saturne:

- ❖ Unstructured (polyhedral).
- ❖ Collocated Finite Volume.
- ❖ SIMPLEC algorithm for the Vel/pres coupling.
- ❖ Time scheme: Crank-Nicolson. The mass flux non-linear term treated with Adams-Bashforth extrapolation.
- ❖ Spatial discretisation: Fully CD.
- ❖ Implicit Gradient reconstruction with Gauss method or least-squares.

Star-CD version 4.xx:

- ❖ Unstructured (polyhedral).
- ❖ Collocated Finite Volume.
- ❖ SIMPLE algorithm for the Vel/pres coupling.
- ❖ Time scheme: Three-time levels
- ❖ Spatial discretisation: CD (deferred correction → cross-diffusion term computed using explicit values).
- ❖ Gradient reconstruction with Gauss method for pressure and velocity.

- Re=395
- Domain $2\pi\delta \times 2\delta \times \pi\delta$
- LES Ncells= 443,272
- DNS Ncells = 9,486,336
(Ref: Moser et al. 1999)



Unstruct. "Taylor" mesh, $N_t=0.44$ M, $Re = 395$

	N x	Ny	Nz
LES	68 to 200	46	42 to 100
DNS	256	193	192

Time history at different points

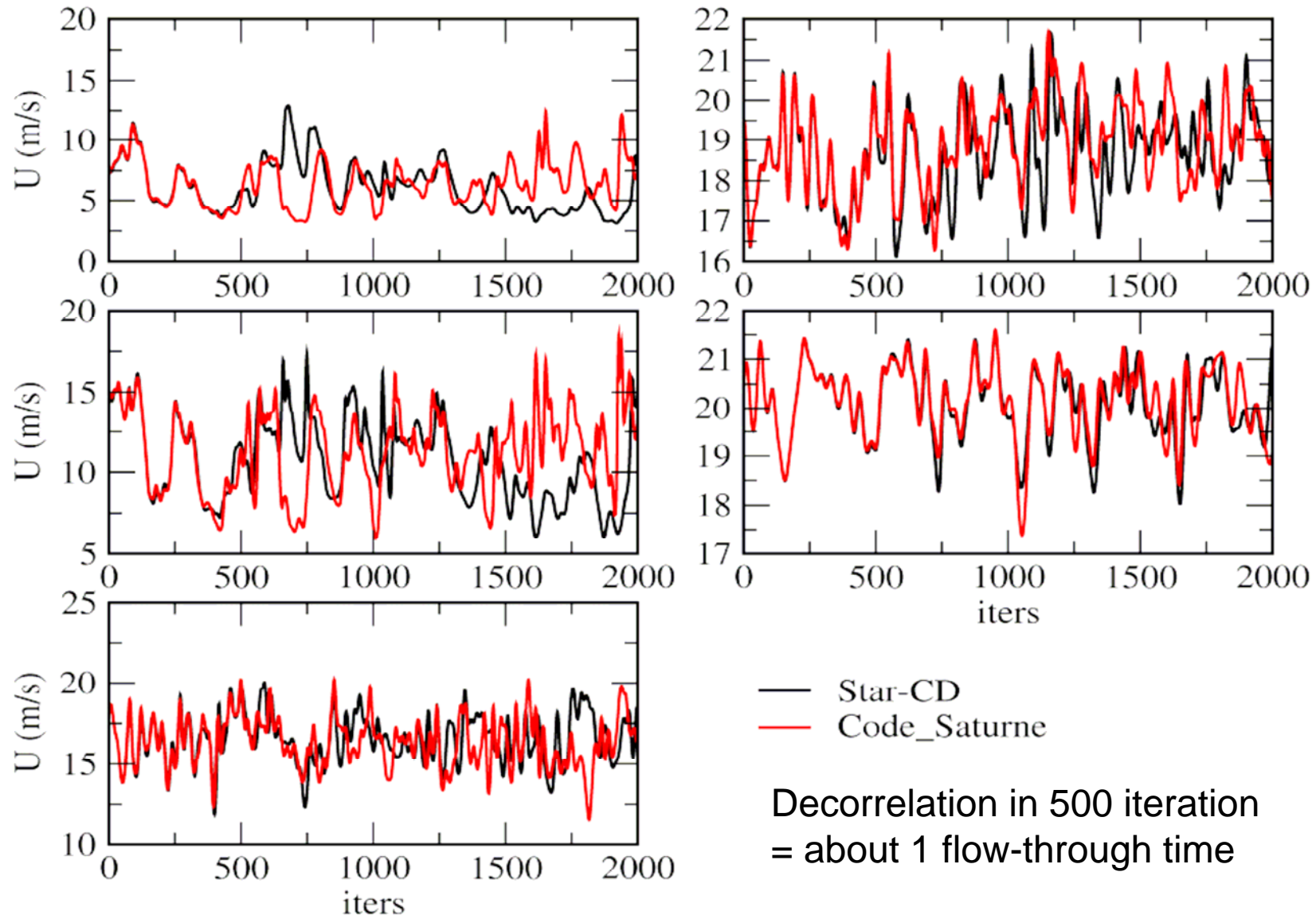
- History of the flow at 5 monitoring cells
- Number of iters. = 2000
- Time (T) = 2s
- Time for one Pass (T_{pass}) = 0.4432725 s

Probes	Y^+
1	5.88
2	12.95
3	70.67
4	199.43
5	375.61

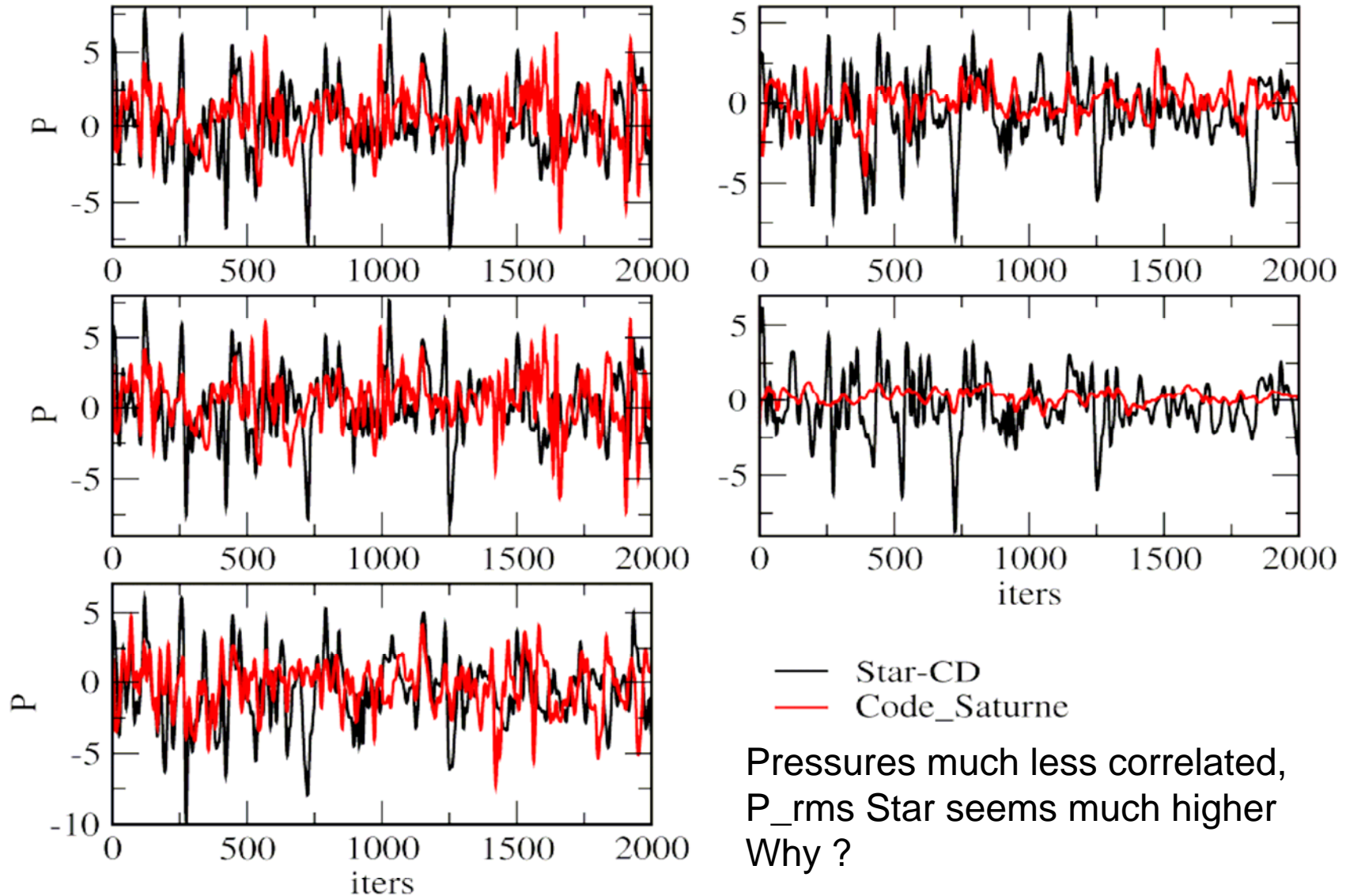
- $T/T_{pass} = 4.51$

	Star-CD	Saturne
Res Vel	1.00E-005	1.00E-004
Res P	1.00E-005	1.00E-003
Res Vel/P Coupling	1.00E-005	1.00E-003
Rec RHS	? (1 most probably)	Vel 10 P 5

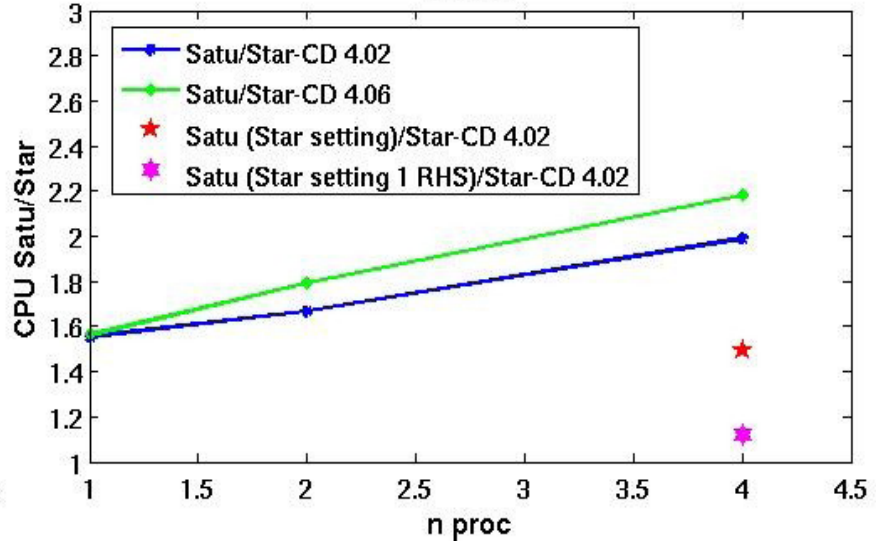
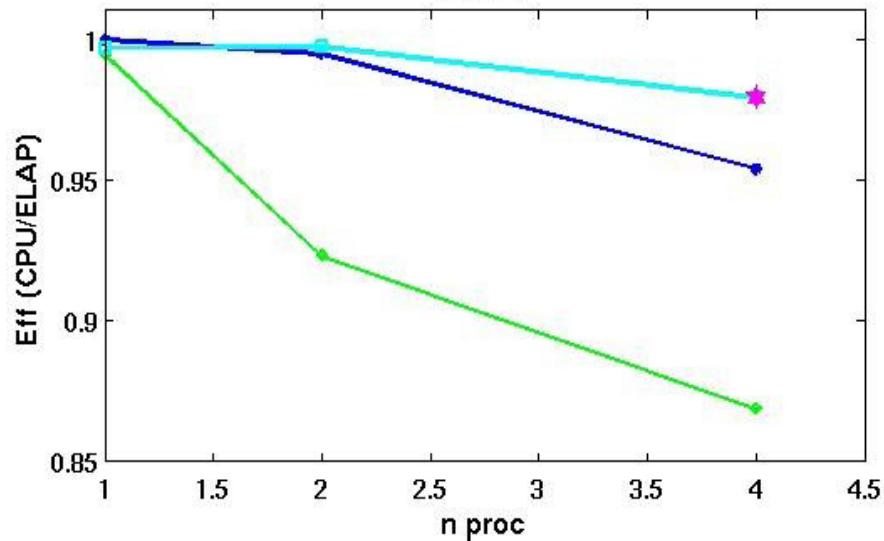
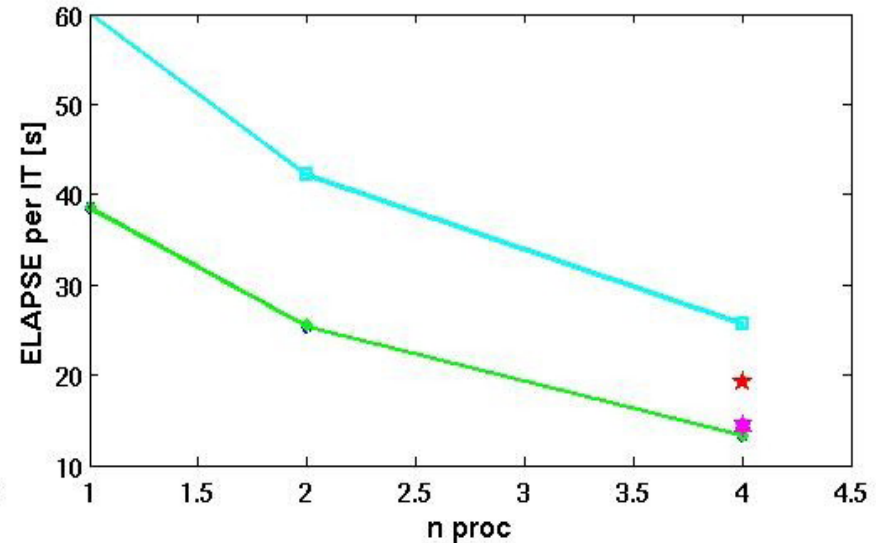
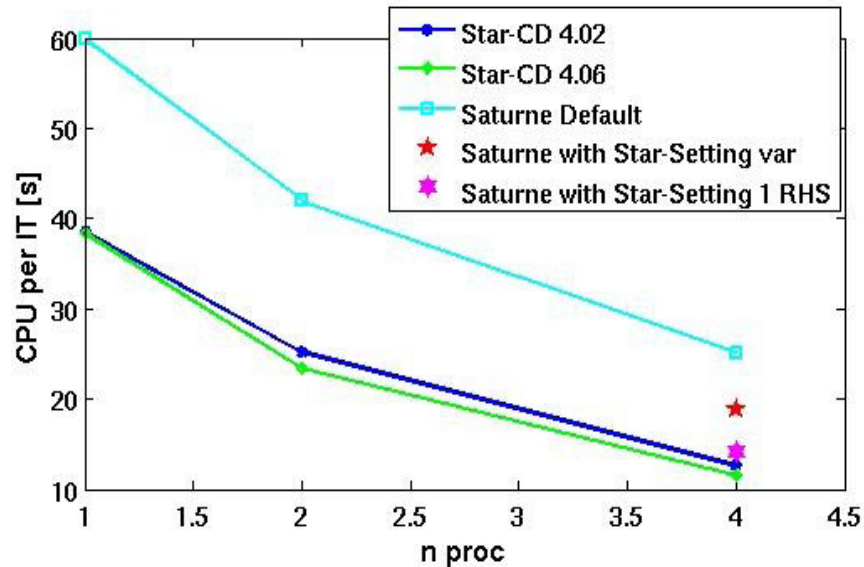
Time history at different points



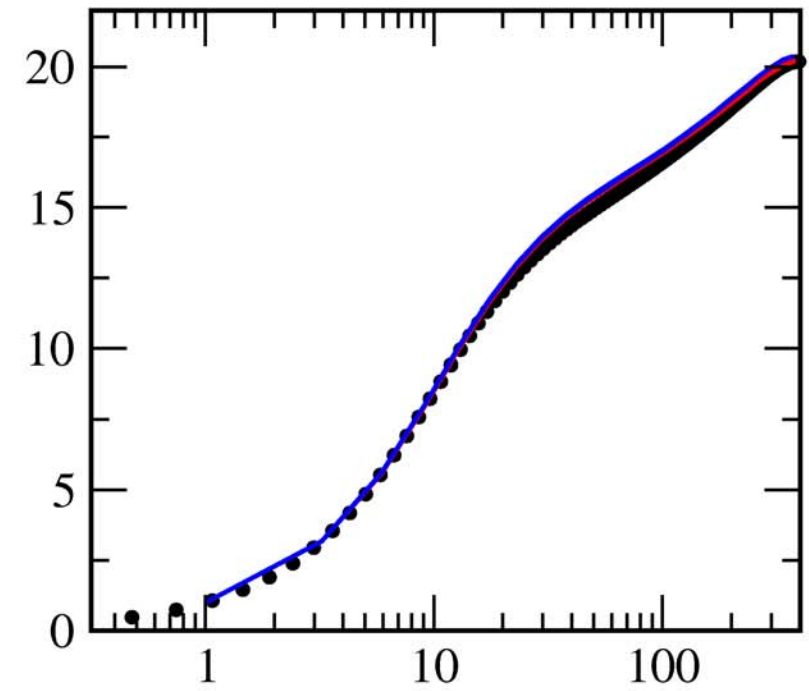
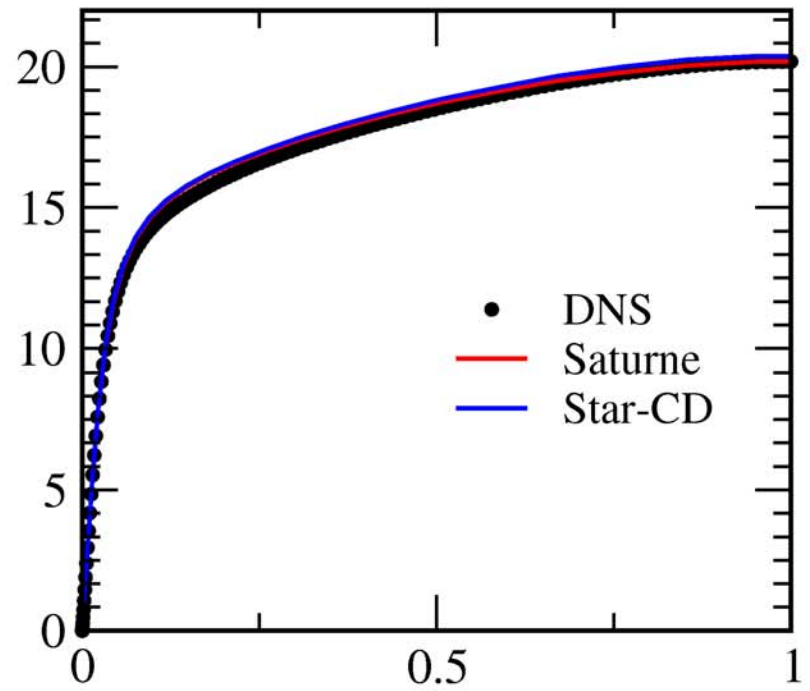
Time history at different points



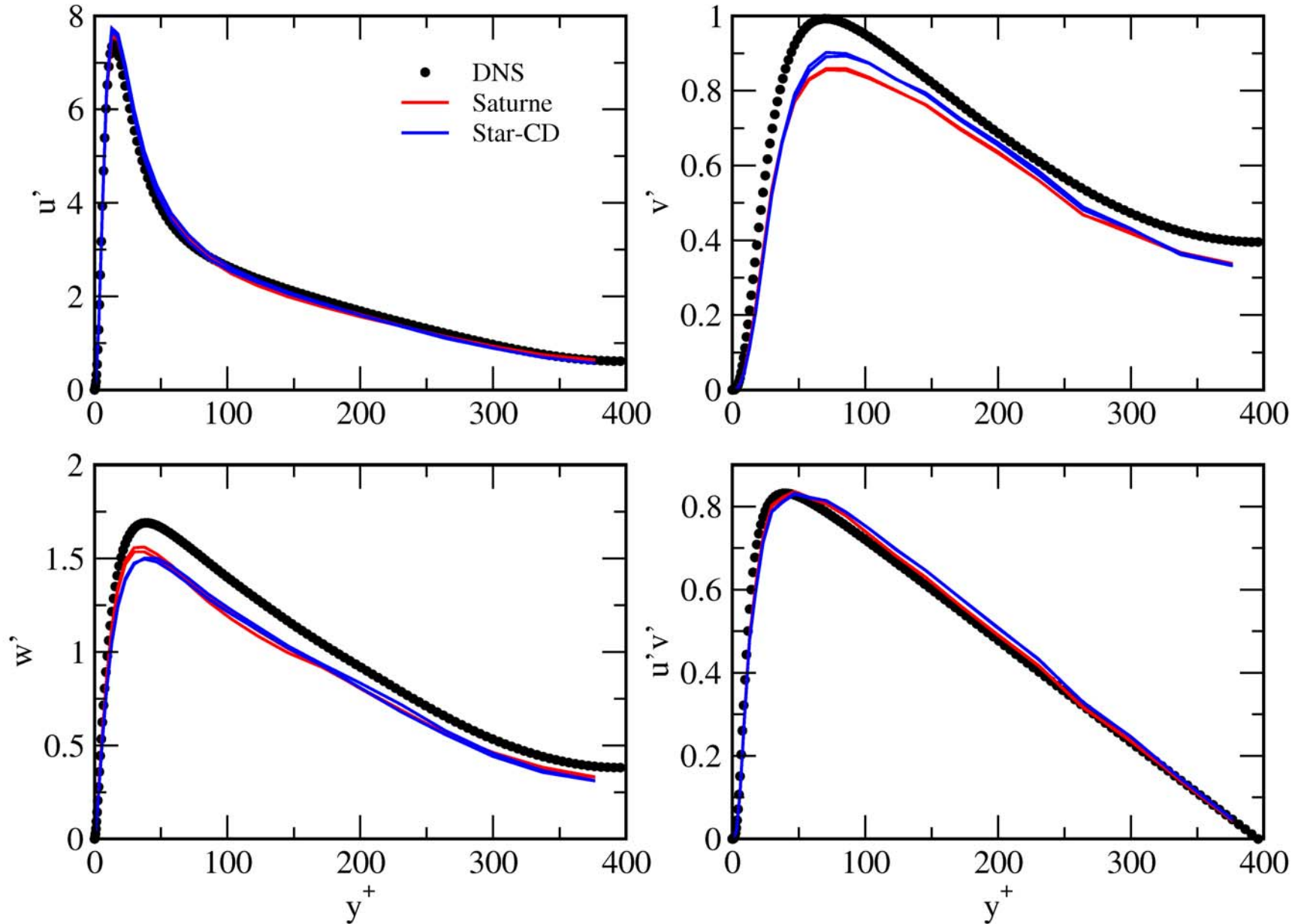
Unstruct. "Taylor" mesh on 1, 2, 3, 4 procs



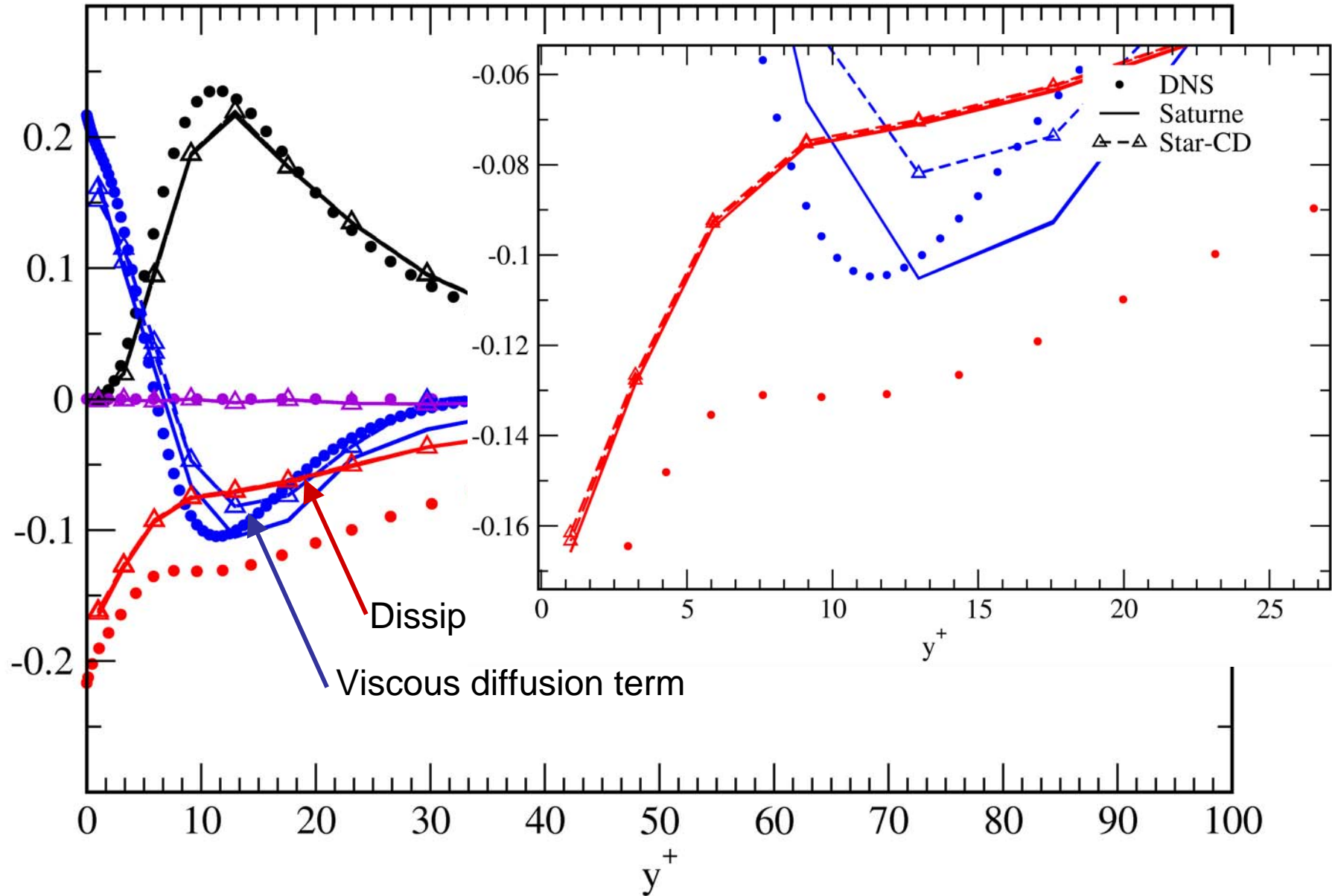
Channel flow test case: Mean Velocity predictions



Channel flow test case: Reynolds Stresses



Channel flow test case: Budget for k



Budgets of the Reynolds stress components

$$\underbrace{\langle \overline{U}_k \rangle \frac{\partial \langle u'_i u'_j \rangle}{\partial x_k}}_{C_{ij}} = - \underbrace{\left(\langle u'_k u'_i \rangle \frac{\partial \langle \overline{U}_j \rangle}{\partial x_k} + \langle u'_k u'_j \rangle \frac{\partial \langle \overline{U}_i \rangle}{\partial x_k} \right)}_{P_{ij}} + \underbrace{\left\langle \frac{p'}{\rho} \left(\frac{\partial u'_i}{\partial x_j} + \frac{\partial u'_j}{\partial x_i} \right) \right\rangle}_{\Phi_{ij}}$$

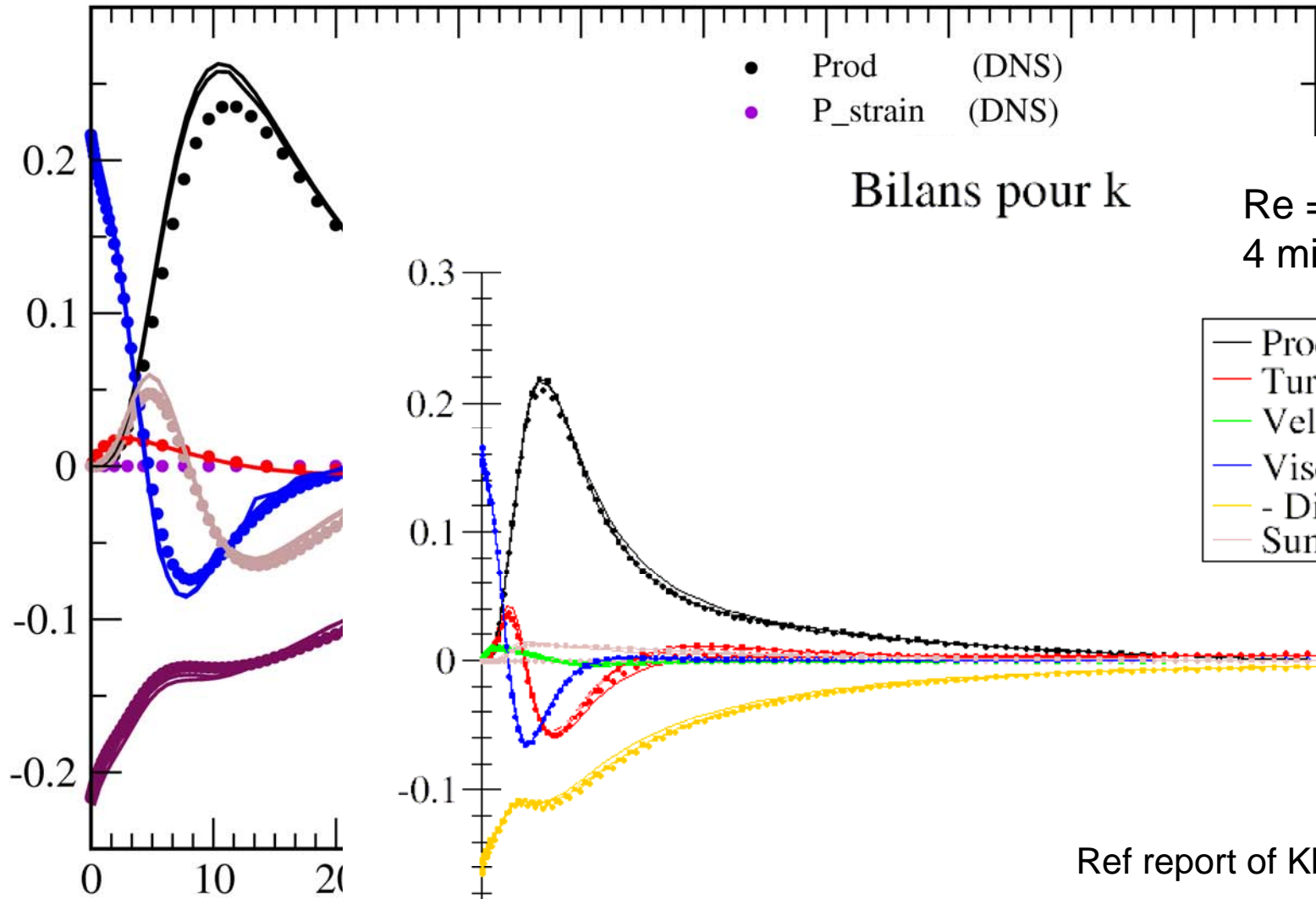
$$- \underbrace{\frac{\partial \langle u'_k u'_i u'_j \rangle}{\partial x_k}}_{D'_{ij}} - \underbrace{\frac{\partial}{\partial x_k} \left(\langle p' u'_i \rangle \delta_{jk} + \langle p' u'_j \rangle \delta_{ik} \right)}_{D''_{ij}} + \underbrace{\nu \frac{\partial^2 \langle u'_i u'_j \rangle}{\partial x_k^2}}_{D'''_{ij}} - \underbrace{2\nu \left\langle \frac{\partial u'_i}{\partial x_k} \frac{\partial u'_j}{\partial x_k} \right\rangle}_{\varepsilon_{ij}}$$

$$- \underbrace{\frac{\partial \langle u'_j \tau'_{ik} + u'_i \tau'_{jk} \rangle}{\partial x_k}}_{D^{SGS}_{ij}} + \underbrace{\left\langle \tau'_{ik} \frac{\partial u'_j}{\partial x_k} + \tau'_{jk} \frac{\partial u'_i}{\partial x_k} \right\rangle}_{\varepsilon^{SGS}_{ij}}$$

neglected

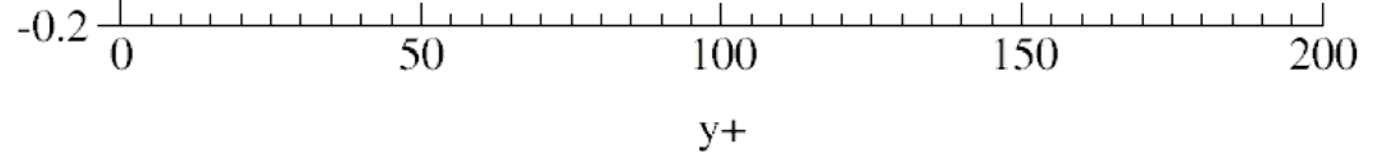
Ref: T. Omori et al. Int. J. Heat and fluid flow 2008

STAR: Grid (141x184x177) = 4.59 million
DNS : Grid (256x193x192)= 9.48 million

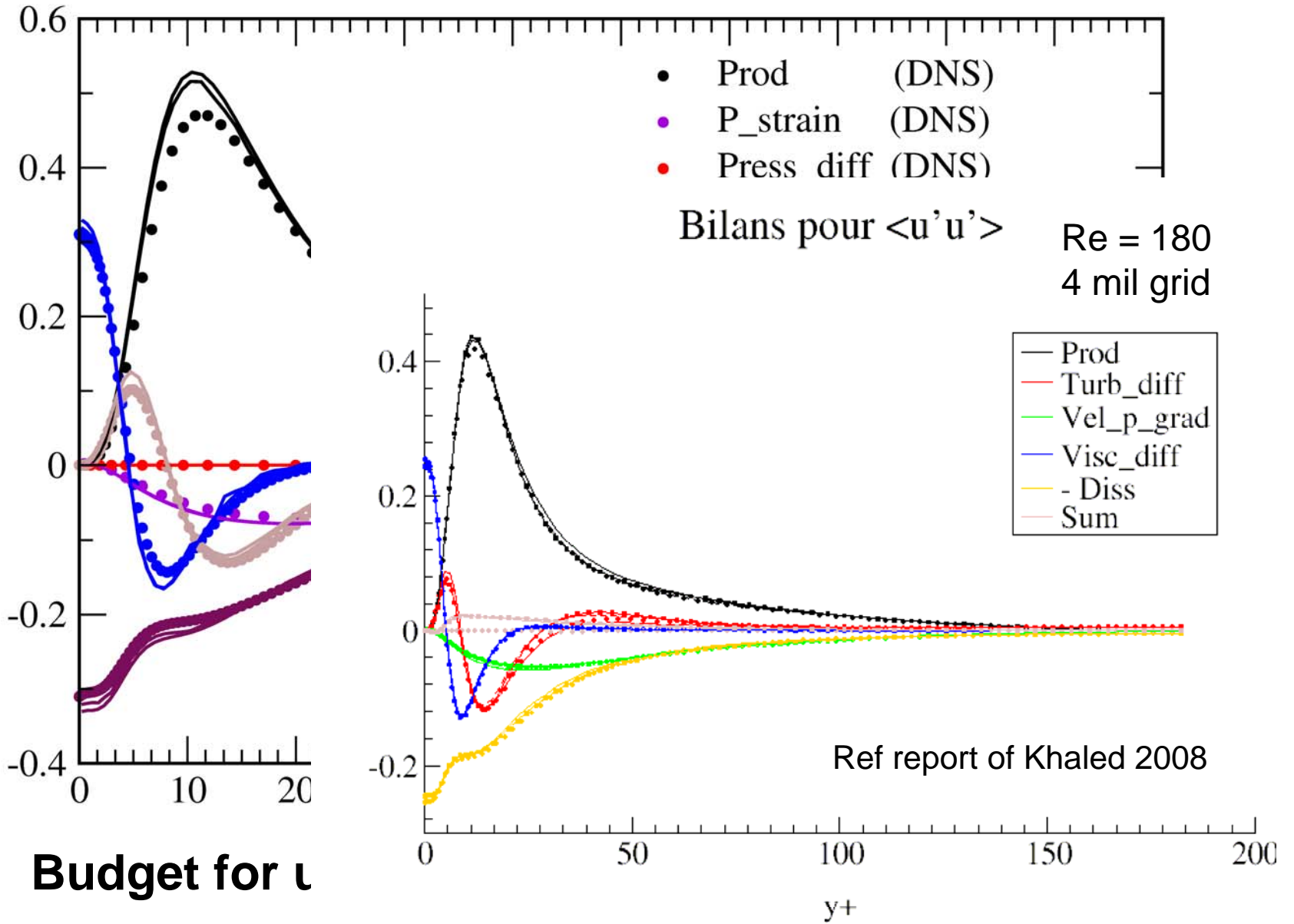


Ref report of Khaled 2008

Budget for k

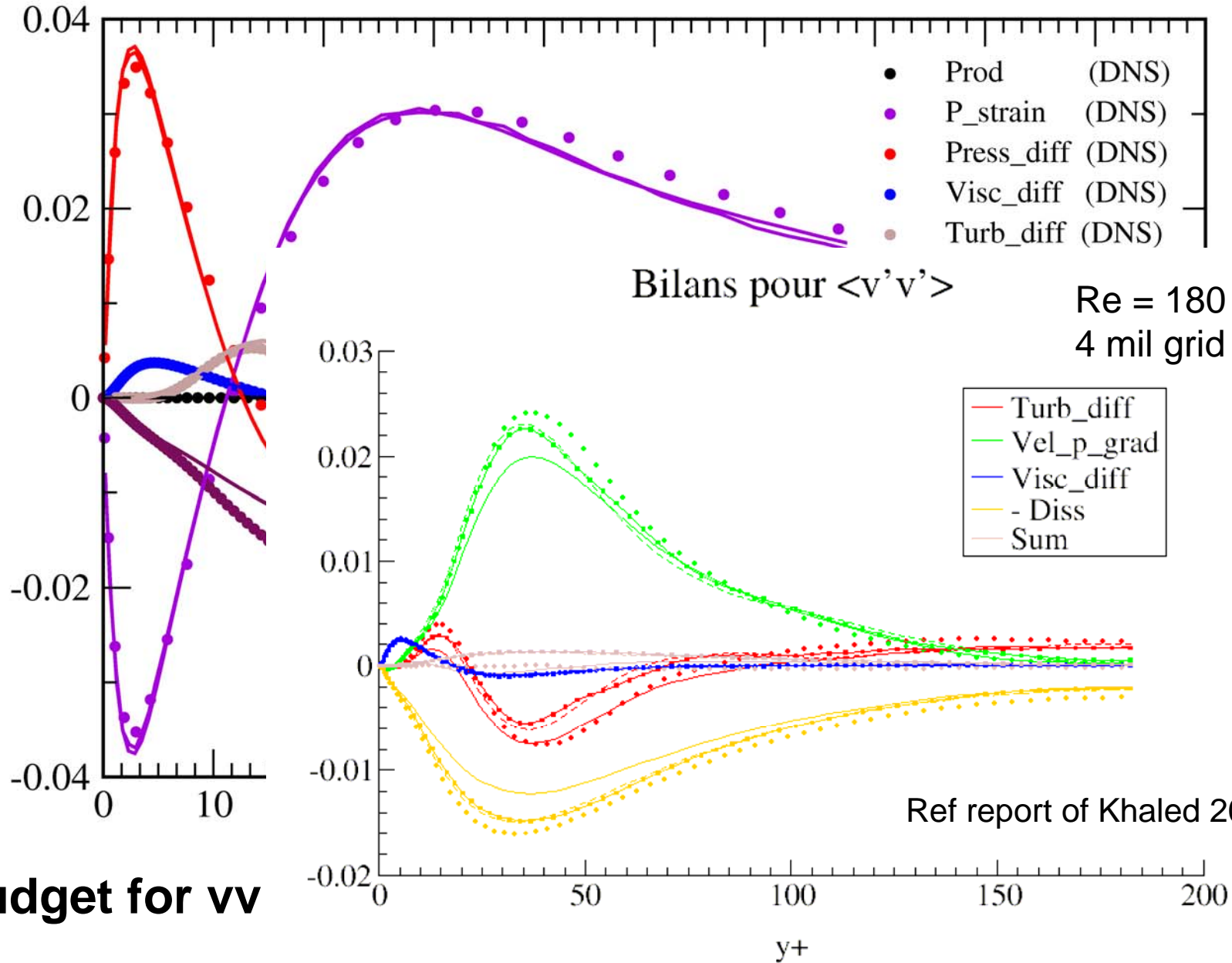


STAR: Grid (141x184x177) = 4.59 million
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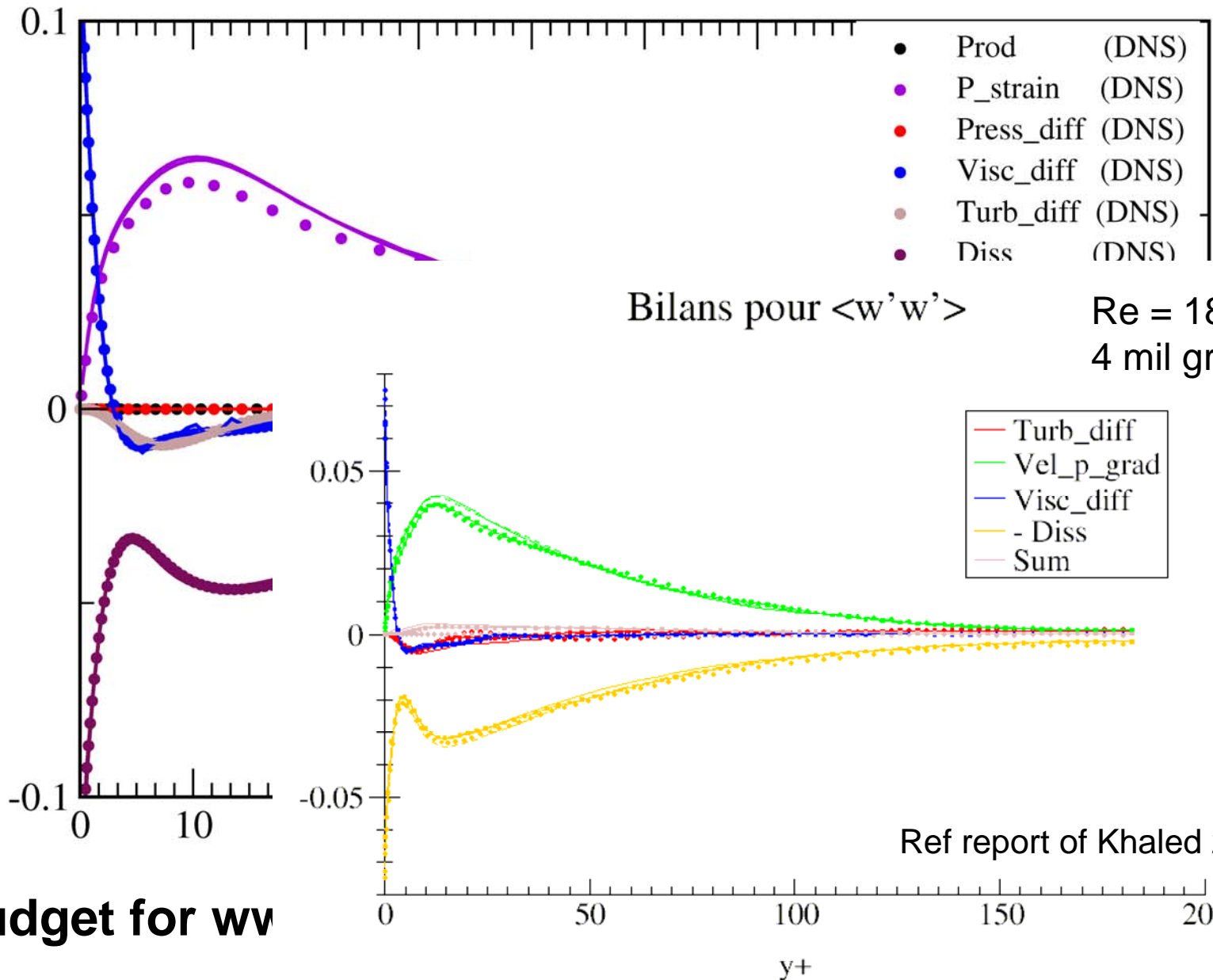
Budget for $\langle u'u' \rangle$

STAR: Grid (141x184x177) = 4.59 million
DNS : Grid (256x193x192)= 9.48 million



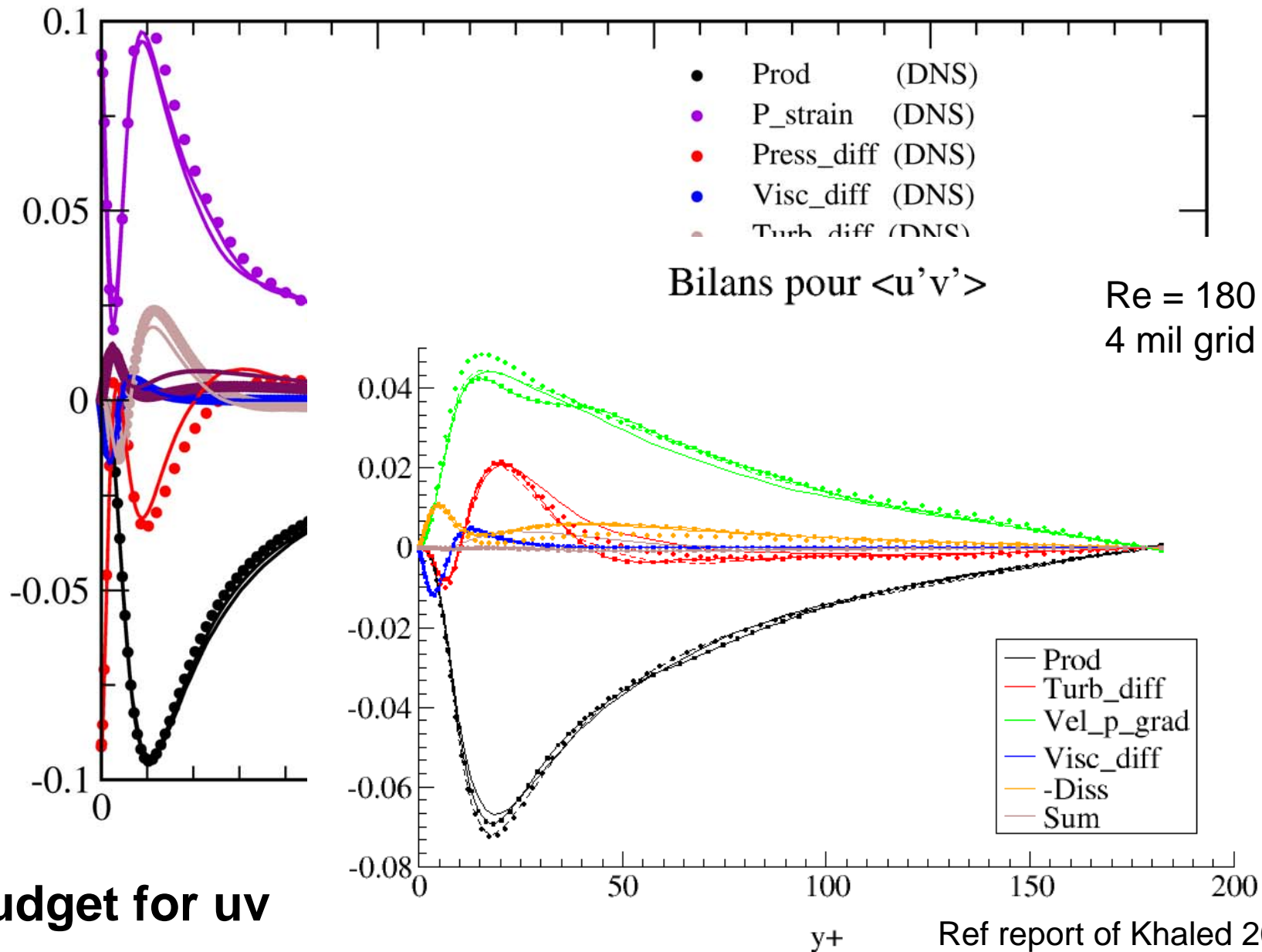
— Budget for vv

STAR: Grid (141x184x177) = 4.59 million
DNS : Grid (256x193x192)= 9.48 million



Budget for wv

STAR: Grid (141x184x177) = 4.59 million
DNS : Grid (256x193x192) = 9.48 million



- **Budget for uv**

Conclusions:

- DNS possible with only 2nd order FV (and true Central DS)
- NB: with C_S and S-C DNS not only limited to Channel Flows !
 - => whole range of PhD topics
(pipes, bends, particles, heat exchangers, thermal fatigue)
- Default precision parameters seem too severe in C_S (cost +50%)

Future work:

- Future tests on complex grids (polyhedral cells), and publish!
- Further investigation on quality criteria for LES is needed.
- Wider range of test cases relevant to the nuclear industry
(suggestions are more than welcome !)