

NUMERICAL MODELLING OF PROTECTION AIR SYSTEM IN FRONT WALL FIRED BOILER OP650

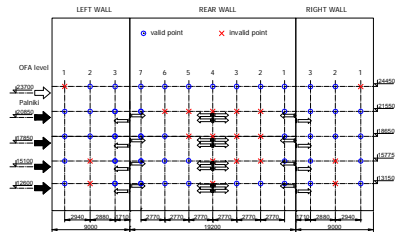
Bartłomiej HERNIK PhD student, Prof. Marek PRNOBIS, Robert WEJKOWSKI PhD,

Silesian University of Technology, Institute of Power Engineering and Turbomachinery, Gliwice, Poland

The aim of this study was numerical simulations, of protection air system in front wall fired boiler OP650 K5 in Rybnik Power Plant. Simulations of the furnace process with and without protection air system were done.

Measurement of boundary gas composition layer on left, rear and right wall in boiler for different cases of working boiler OP650 was done. Then numerical simulation of that different cases of working boiler was done to comparison measurement with simulations.

Schematic arrangement of points to probe boundary gas layer and protection air inlets (view from inside of the furnace)



Fuel for boiler OP650 was coal – characteristic parameters used: coal granulation as grain's share bigger than x, coal analysis as received state - lower heat value and elementary analysis.

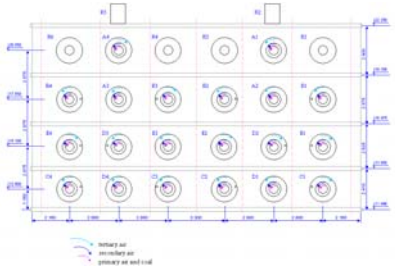
Coal granulation

| x | R |
|-----|--------|
| 0 | 33.07 |
| 10 | 27.074 |
| 20 | 20.890 |
| 50 | 17.917 |
| 200 | 5.46 |

coal analysis as received state

| | Q | A | V | C | H | S | O | N |
|--|------|------|-------|------|-----|-------|-------|-------|
| | 2124 | 21.2 | 12.51 | 56.4 | 3.2 | 0.200 | 1.800 | 0.450 |

Schematic arrangement of burners and OFA inlets on front wall of the boiler (view from inside of the furnace)

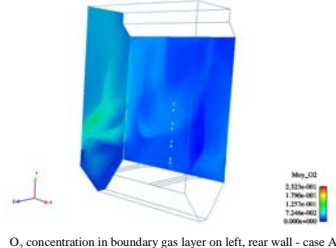


The four cases (A, B, C, D) of working boiler was implemented for numerical modelling. In this case boiler worked with 160MW and 215MW nominal output with various mills (burners) worked and with or without Protection Air System (PAS).

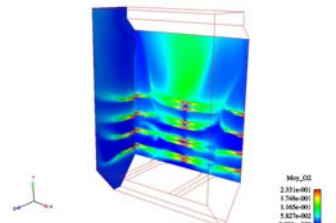
Data sheet of parameters for different boiler work cases

| Data | Unit | A | B | C | D |
|-----------------------|------------|------------|------------|------------|---------------|
| Working mills | A, B, C, E | A, C, D, E | B, C, D, E | B, C, D, E | A, B, C, D, E |
| Nominal output | MW | 160 | 160 | 215 | 215 |
| Primary air flow | kg/s | 15.10 | 16.02 | 17.27 | 17.18 |
| | kg/s | 17.06 | 18.59 | 17.58 | 17.33 |
| | kg/s | 16.36 | 18.98 | 18.45 | 17.74 |
| | kg/s | 15.89 | 19.2 | 17.73 | 17.86 |
| Coal flow | kg/s | 3.51 | 3.35 | 5.5 | 5.44 |
| | kg/s | 4.93 | 4.41 | 5.59 | 5.45 |
| | kg/s | 4.03 | 4.56 | 4.81 | 5.05 |
| | kg/s | 4.13 | 4.4 | 5.32 | 5.19 |
| Coal temperature | °C | 114 | 108 | 116 | 113 |
| Air temperature | °C | 257 | 250 | 268 | 267 |
| Opening of OFA inlets | % | 4.13 | 52.51 | 26.92 | 15.08 |
| B, 3, 4 | % | 28.65 | 48.51 | 51.81 | 40.29 |
| B, 5, 6 | % | 28.6 | 49.96 | 51.7 | 40.02 |
| OFA air flow | kg/s | 0.331 | 4.21 | 2.59 | 1.45 |
| | kg/s | 0.220 | 2.9 | 1.78 | 1.00 |
| B, 3 | kg/s | 2.300 | 5.49 | 4.99 | 3.88 |
| B, 4 | kg/s | 2.300 | 5.49 | 4.99 | 3.88 |
| B, 5 | kg/s | 1.577 | 2.75 | 3.42 | 2.65 |
| B, 6 | kg/s | 2.294 | 4.01 | 4.98 | 3.85 |
| Tertiary air flow | kg/s | 23.100 | 14.6 | 28.27 | 26.03 |
| | kg/s | 20.089 | 10.42 | 23.26 | 21.05 |
| | kg/s | 20.706 | 9.82 | 22.53 | 20.33 |
| | kg/s | 20.706 | 9.82 | 21.81 | 19.61 |
| Secondary air flow | kg/s | 21.55 | 21.55 | 25.86 | 25.86 |
| PAS air flow | kg/s | 0 | 16.33 | 0 | 15.8 |

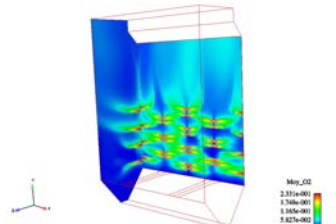
Additional simulation of new concept of Protection Air System for B and D cases of working boiler was done. That modelling is signed with "N" letter, for example NB means modelling the new protection air system for conditions of working boilers described in case B.



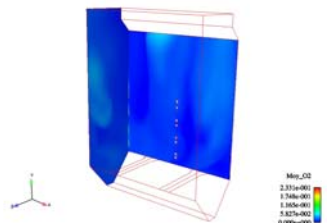
O₂ concentration in boundary gas layer on left, rear wall - case A



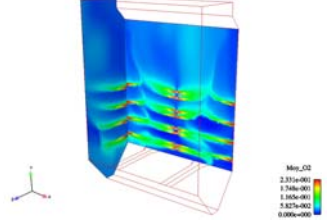
O₂ concentration in boundary gas layer on left, rear wall - case B



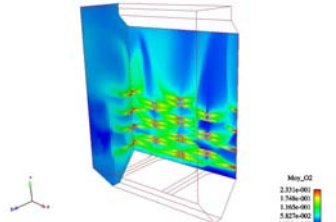
O₂ concentration in boundary gas layer on left, rear wall - case NB



O₂ concentration in boundary gas layer on left, rear wall - case C



O₂ concentration in boundary gas layer on left, rear wall - case D



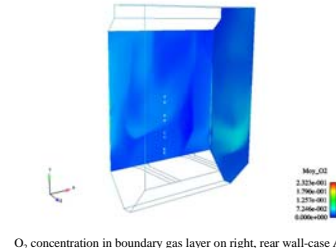
O₂ concentration in boundary gas layer on left, rear wall - case ND

Measured O₂ concentration in boundary gas layer - case A (view from inside of the furnace, grey layer- point's coordinates)

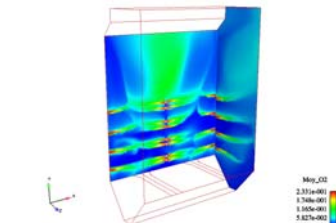
| Left Wall | 3 | 2 | 1 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 3 | 2 | 1 |
|-----------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 0.1 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 |
| 0.2 | 20.3 | 19.7 | 19.4 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 |
| 0.3 | 20.3 | 19.7 | 19.4 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 |
| 1000 | 4.06 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 |

Results of modelling O₂ concentration in boundary gas layer - case A (view from inside of the furnace, grey layer- point's coordinates)

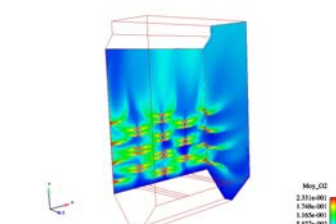
| Left Wall | 3 | 2 | 1 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 3 | 2 | 1 |
|-----------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 0.1 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 |
| 0.2 | 20.3 | 19.7 | 19.4 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 |
| 0.3 | 20.3 | 19.7 | 19.4 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 | 19.3 |
| 1000 | 4.06 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 | 1.19 |



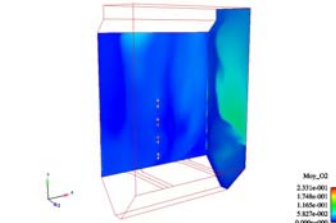
O₂ concentration in boundary gas layer on right, rear wall - case A



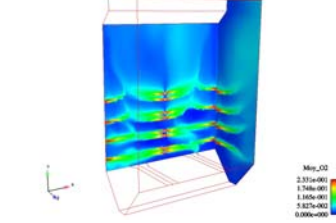
O₂ concentration in boundary gas layer on right, rear wall - case B



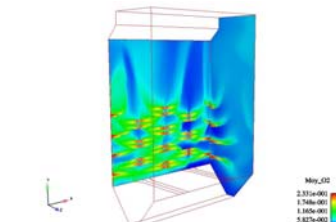
O₂ concentration in boundary gas layer on right, rear wall - case NB



O₂ concentration in boundary gas layer on right, rear wall - case C



O₂ concentration in boundary gas layer on right, rear wall - case D



O₂ concentration in boundary gas layer on right, rear wall - case ND