



Measurement of primary coolant flow rate from a pressure difference

Romain CAMY with the help of *Code.Saturne* team and Open CASCADE support - May 2019

EDF/DIPNN/TECHNICAL DIRECTION

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- Presentation of the integral effect test
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- Details on calculations setup
- Calculations results compared to experiment
- Conclusion and prospects

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Principle of primary flow rate measurement

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Balance of enthalpy

In a Pressurized Water Reactor (PWR), mass flow rate (\dot{m}_i) in each loop is derived from the **thermal power at the steam generator** (SG_i), the **temperatures in hot and cold legs** ($T_{HL,i}$ and $T_{CL,i}$) and the **electric power absorbed by the Reactor Coolant Pumps** (\dot{W}_{RCP}).

$$\dot{W}_{SG,i} = \dot{m}_i (h(T_{HL,i}) - h(T_{CL,i})) + \frac{\dot{W}_{PPump}}{4}$$

Only once at the beginning of a fuel cycle.

Possible impact

From [Lish 2017]:

Inaccurate flow monitoring can result in power downrating and unnecessary downtime.

Principle of primary flow rate measurement

Balance of enthalpy

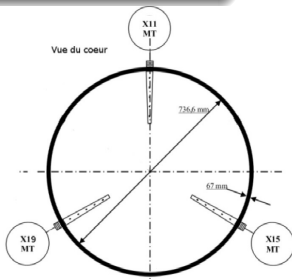
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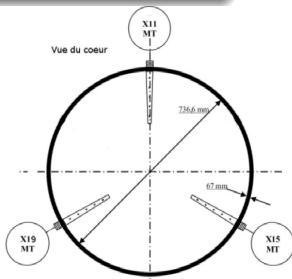
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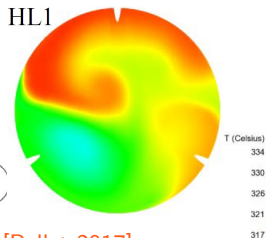
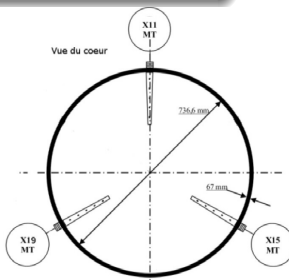
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Pressure difference

Use a **pressure difference** between both sides of the first elbow after steam generator ΔP_{elbow} to estimate the volumetric flow rate (\dot{V}_i) with

$$\dot{V}_i = KD^{3/2}Rc^{1/2}\sqrt{\frac{\Delta P_{elbow}}{\rho}}$$

- K a constant depending on the locations of the pressure probes,
- D tube diameter,
- Rc bending radius,
- ρ fluid density.

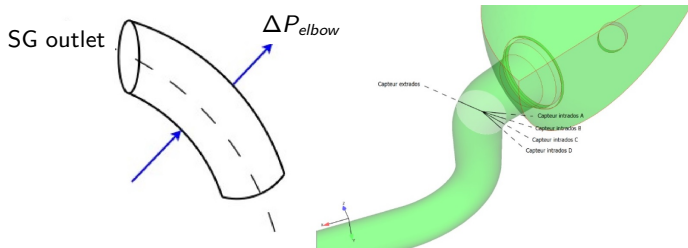
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Schematic view ΔP_{elbow} measure [Mercier 2015]

Presentation of the integral effect test

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EVEREST "SG water box - crossover leg"

- 1:4 scaled-down model of cold side SG water box loop 2 of Chooz B1 French PWR.
- Tests in 2000 and 2010.
- Experimental uncertainty quantification.
- In crossover leg $Re \in [8.3 \cdot 10^5, 2.6 \cdot 10^6]$
 $\rightarrow y^+ = 1 \Leftrightarrow \Delta y < 13 \mu m$
(full scale $Re \approx 8.0 \cdot 10^7$).

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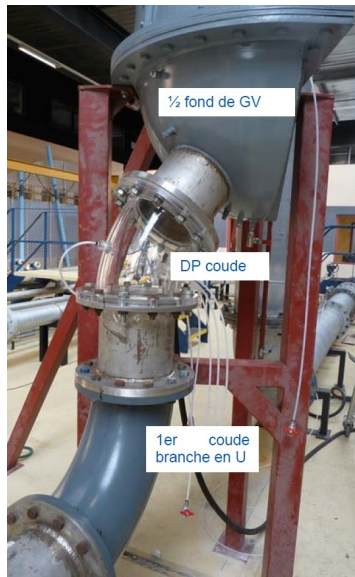
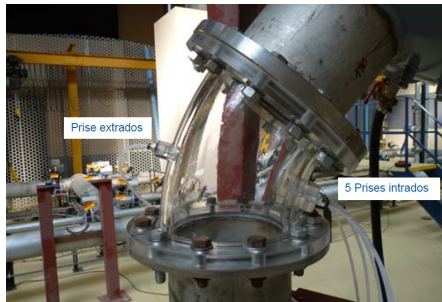
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Experimental setup in Chatou (France)

Zoom on the mesh generation

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What makes a mesh good ?

- **adapted to the physics** (boundary layer, alignment with streamlines, ...)
- **hexaedra** > other elements
- **conformal mesh**
- **good quality criteria**
- **good looking**

How to ?

No known algorithm able to mesh an arbitrary volume with conformal hexaedra (with the constraint to respect the initial volume) → **“blocking”**.

2 possible strategies:

- use assistance from **predefined patterns**,
- define the blocking in a **CAD program**.

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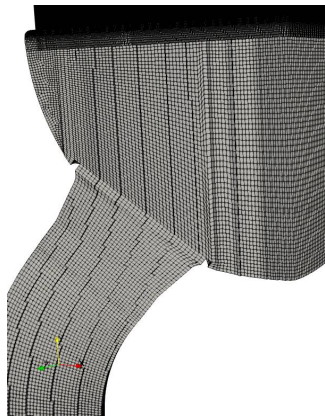
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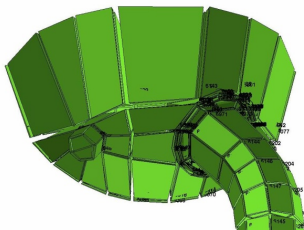
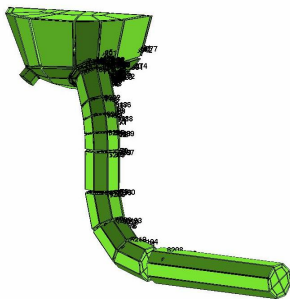
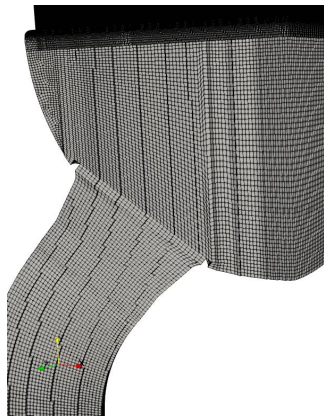
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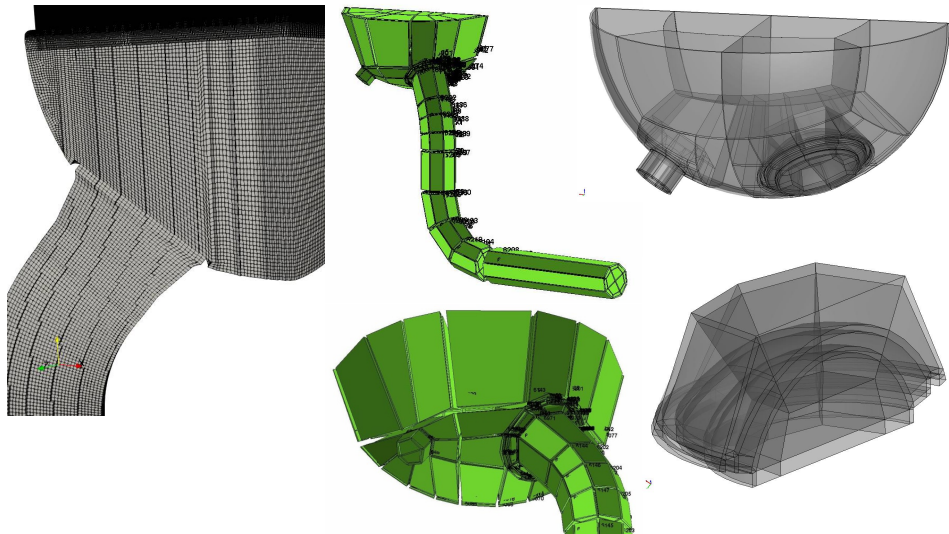
Recent realisations from 2 service providers and present work

Zoom on the mesh generation



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Used mesh technique in present work

Blocking made in 2 steps with **parallel joining** in *Code_Saturne* (conformal).

- → easier to setup and debug,
- → overcome the limitation of ≈ 200 M cells for a mesh in SMESH (and faster).

Large range of refinement levels: from 330 K (ref. 1) to 2.64 B cells (ref. 20)

0 bad cell but $> 0.05\%$ *"faces have a too large reconstruction distance"*

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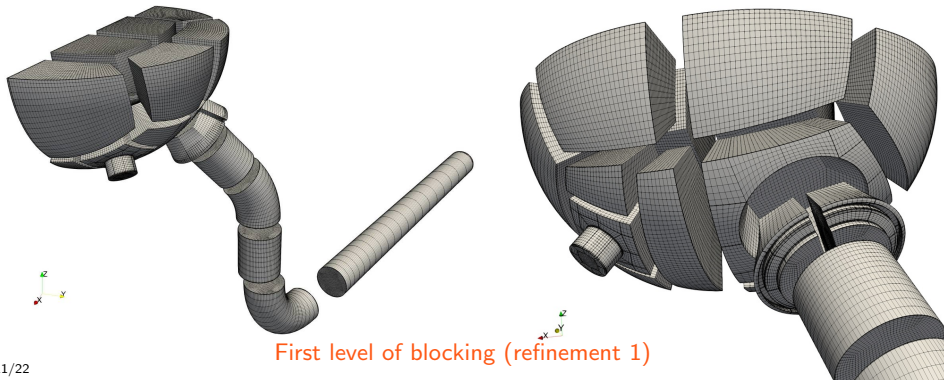
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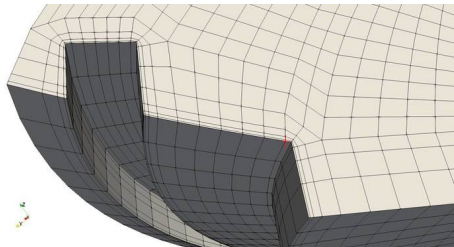
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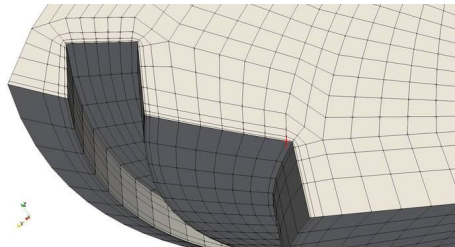
First level of blocking (refinement 1)

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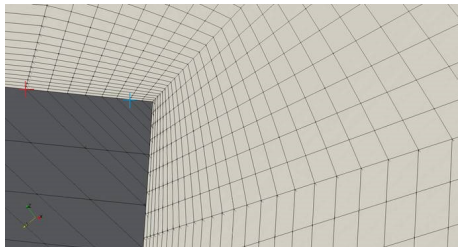


Ref. 1 (330 K cells)

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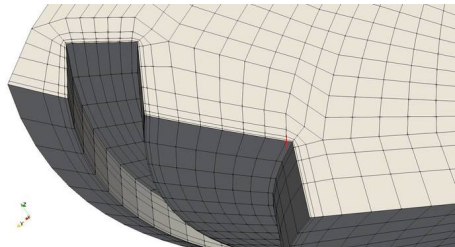
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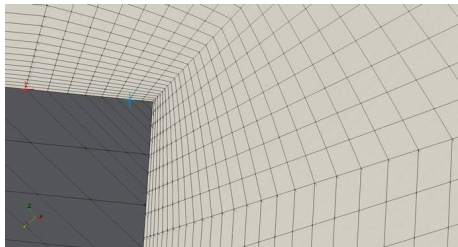
Ref. 8 (169 M cells)

Ref. 8: $y^+ \approx 2$, $z^+ \approx 70$, $x^+ \approx 186$ and $\bar{\nu}_t/\nu \approx 0.3$ with $\nu_{t,max}/\nu \approx 6$.

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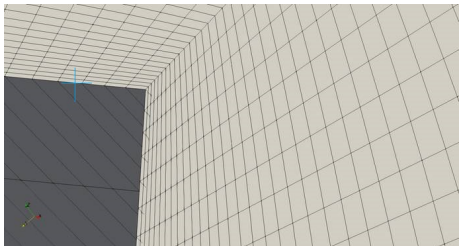


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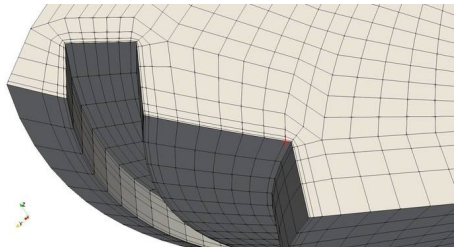
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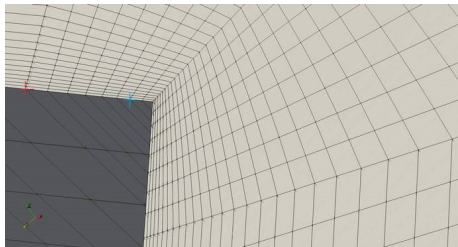


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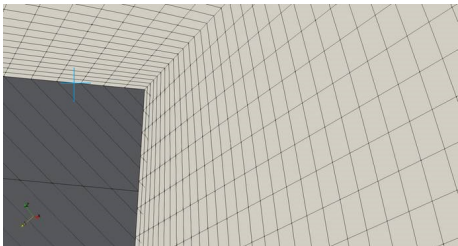


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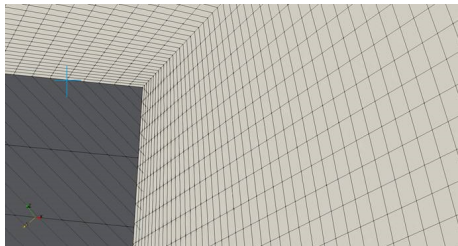


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Ref. 20 (2.64 B cells)

Details on calculations setup

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Models and numerical parameters

- **Unsteady** with constant time step,
 - in RANS: $CFL_{max} < 20$ and $CFL_{moy} \approx 0.05$,
 - in LES: $CFL_{max} < 10$ and $CFL_{moy} \approx 0.05$.
- In LES, **Smagorinsky model** and 2% upwind for momentum.
- In RANS, **wall resolved models**: $k - \omega$ & EB-RSM and pure central scheme.
- Inlet jets simulated with **non uniform inlet velocities**.

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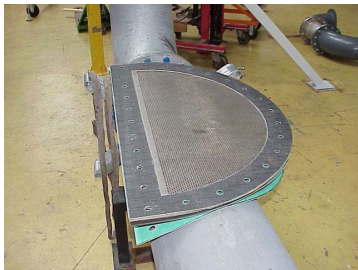
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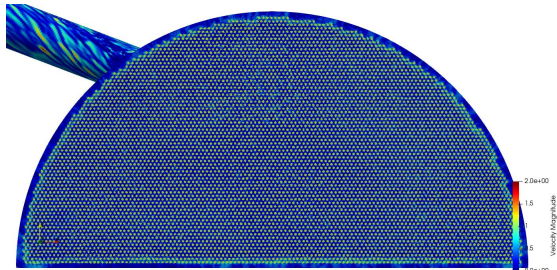
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Inlet slab



Inlet velocities (ref. 8 mesh)

Calculations results compared to experiment

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Different models tested on different meshes

The general shape of the streamlines are **consistent with each other**. More specifically:

- all calculations predict **Dean vortices** at the outlet of first elbow,
- all calculations excepting coarsest mesh predict a vortex between vertical wall in SG water box and inlet of crossover leg,
- $k - \omega$ steadier than EB-RSM steadier than LES.

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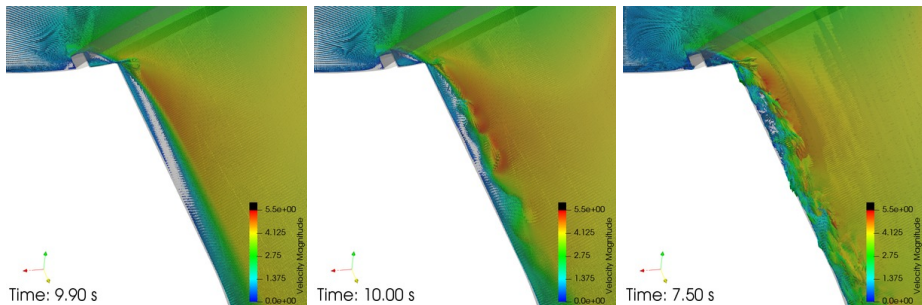
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- $k - \omega$ steadier than EB-RSM steadier than LES.

Calculations results compared to experiment

Different models tested on different meshes

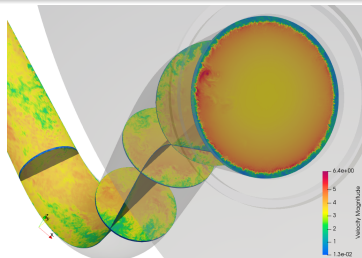
The general shape of the streamlines are **consistent with each other**. More specifically:

- all calculations predict **Dean vortices** at the outlet of first elbow,
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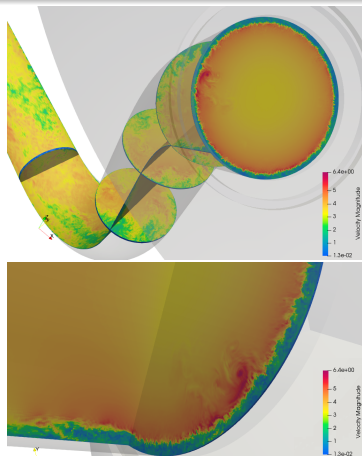
From left to right: ref. 5 $k - \omega$ & EB-RSM, ref. 8 LES

Calculations results compared to experiment



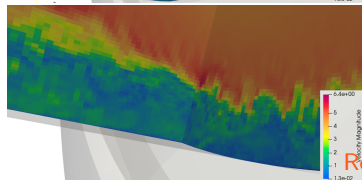
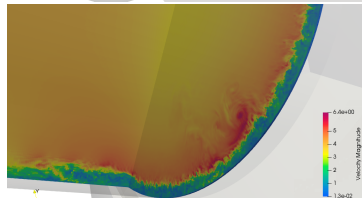
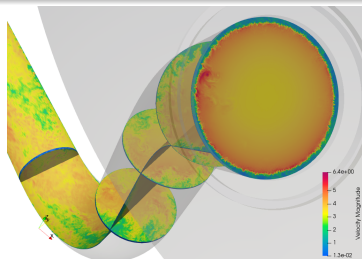
Ref. 13 LES (courtesy of Y. Fournier, E. Le Coupanec)

Calculations results compared to experiment



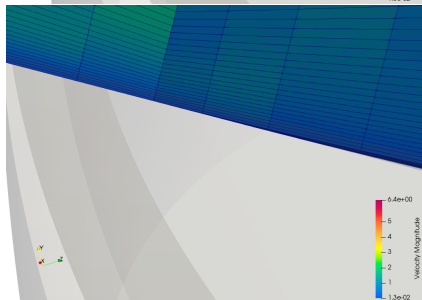
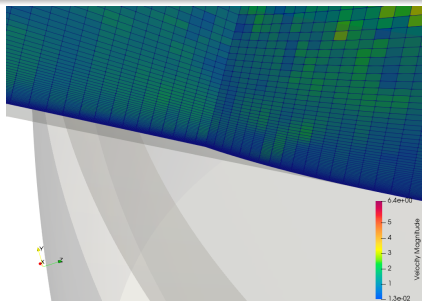
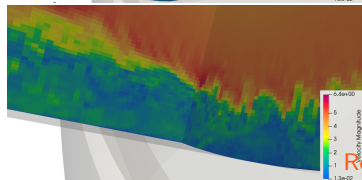
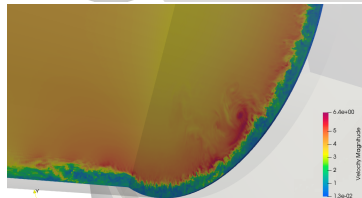
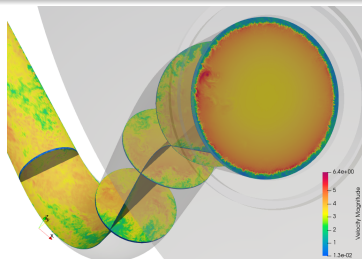
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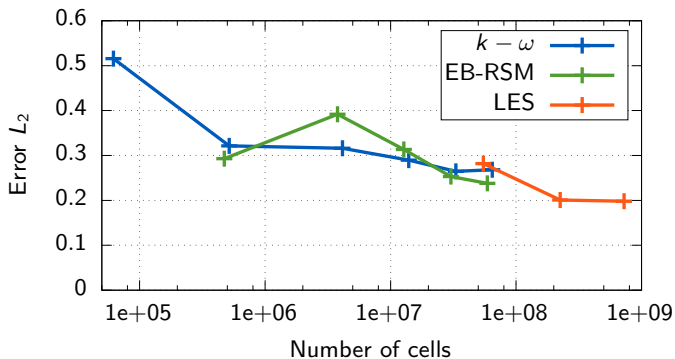
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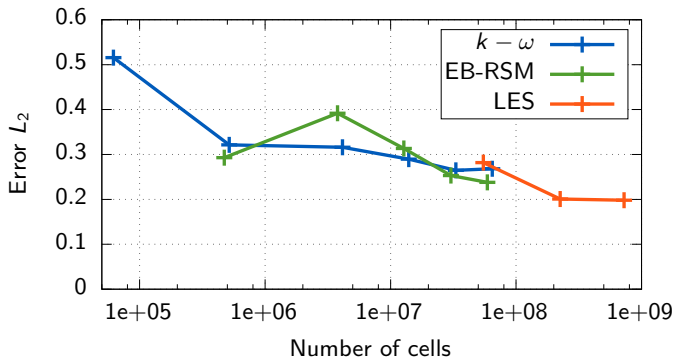
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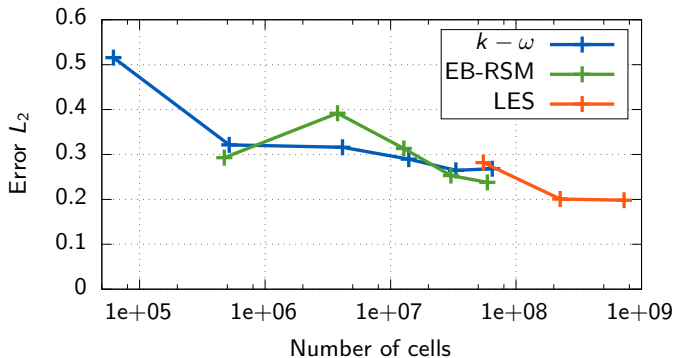
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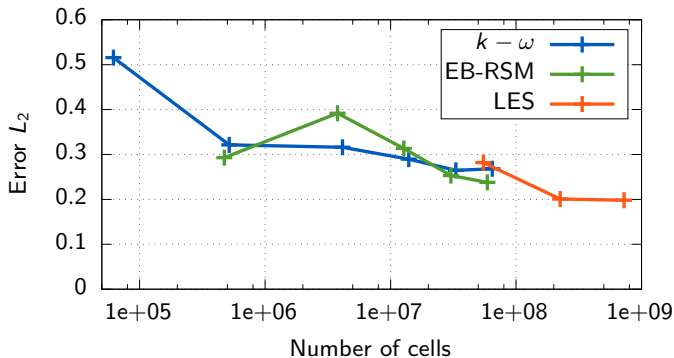
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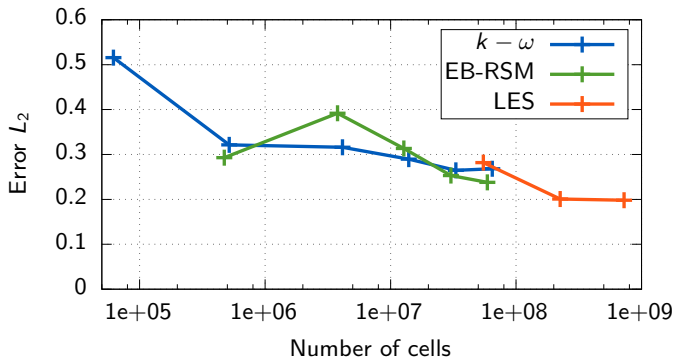
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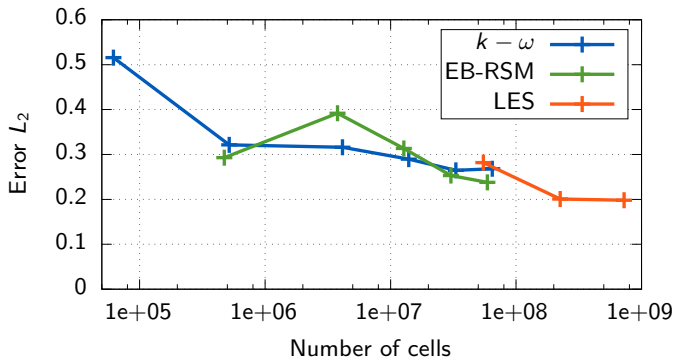
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- Numerical results **very consistent with each other**.
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 - Overlooked phenomenon?
 - Difference between actual experiment and the information used?
 - Common problem in all calculations?



Conclusion

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- For CFD the case is **still challenging**.
- In a foreseeable future **RANS models are unavoidable** on this application.
- To avoid error compensation the **new LES results should be used as reference** for future validation of RANS models on this case.

Future prospects

- Concerning industrial requirements, need for laws for **flowrate as a function of ΔP** with error bands using validation results.
- Concerning CFD use **more physical meshes**:
 - → evolutions of solver (CDO ?),
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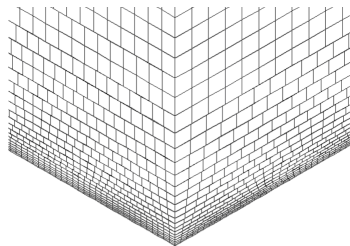
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Taylor scale based mesh
[Addad 2008]

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Thank you

Any questions ?



Turbulent luminance in impassioned van Gogh paintings. J. L. Aragón et al.